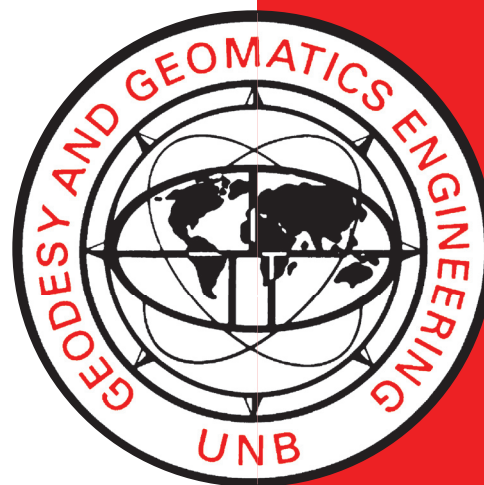


NAVSTAR PERFORMANCE ANALYSIS

DAVID WELLS
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November 1980



TECHNICAL REPORT
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PREFACE

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NAVSTAR PERFORMANCE ANALYSIS

by

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ABSTRACT

The two dimensional, real time navigational accuracy available from NAVSTAR/GPS is investigated, with emphasis on GPS performance during the partially implemented phase (1980 to 1987), and on the ocean areas surrounding Canada.

The mathematical models used in this study to compute NAVSTAR satellite positions, check for satellite visibility, and compute the covariance matrix of two dimensional position are described. The length of the semi major axis of the standard error ellipse represented by this covariance matrix is used as the GPS performance indicator. A computer program implementing these models is listed.

Results based on four error models are presented. These error models are P-code ranging only (with 4 metre range errors), C/A-code ranging only (16 metre range errors), P-code assisted by Loran-C and C/A-code assisted by Loran-C. For this analysis Loran-C ranges to Cape Race, Angissoq and Sandur were assumed to have standard deviations of 140 m. In all cases it was assumed that the user's clock could be kept synchronized to GPS time independently from the GPS measurements, to within 0.3 microseconds. Based on these assumptions, it was found that in the Davis Strait area, combined P-code GPS and Loran-C should provide 150 metre positioning about 11 hours per day, with the present (1980) orbital configuration of six GPS satellites.

GPS performance with only six satellites is also a function of both latitude and longitude. In general high latitudes (60° and above) have poorer performance. The performance at low and middle latitudes depends on the relationship between the observer's meridian and the meridians travelled by the GPS satellite subtracks. Plots of the variation in the length of the GPS error ellipse semi major axis over a 24 hour period are presented for 14 different locations. Complete output listings are presented for three locations and several error models.

A full GPS constellation of 24 satellites was simulated. The two dimensional, P-code positioning accuracy in Davis Strait, using all visible satellites was uniformly of the order of five metres.

It is concluded that it is feasible to use GPS in its present limited deployment as an operational survey positioning system in the eastern Canadian arctic, provided the requirements of the survey are met by 150 metres or better positioning for about 11 hours per day.

ACKNOWLEDGEMENT

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1. Introduction

The purpose of this study is to analyze the performance of the Navigation Satellite Timing and Ranging (NAVSTAR) system, also known as the Global Positioning System (GPS), for the purposes of positioning at sea, during the partially implemented phase of NAVSTAR development (the period 1980 to 1987). The combination of NAVSTAR and passive ranging Loran-C is also investigated.

1.1 NAVSTAR status

NAVSTAR/GPS is presently under development by the United States Department of Defense. Phase one (concept validation) of this development has been completed. Phase two (full scale development) began during 1979. Phase three (production/development) is scheduled for the period 1983 to 1987 (Eckhardt, 1980).

Six prototype NAVSTAR satellites are now in orbit. This constellation will be maintained until operational satellites are placed in orbit, using the Space Shuttle, during the period 1985 to 1987. Once the full constellation of 18 or 24 NAVSTAR satellites are in place, continuous coverage from four or more satellites will be available anywhere on earth. This permits an instantaneous solution for four parameters - normally a three dimensional (3D) position and a time synchronization. Until 1985 at least, however, the six prototype satellites will provide coverage at any location on earth varying from no satellites up to all six satellites. This coverage is a function of time, as well as position, with a main period of twelve hours (NAVSTAR satellite orbital period).

1.2 Passive ranging

NAVSTAR positioning depends on passive ranging measurements, also known as pseudo-ranging and as "rho-rho" measurements. Atomic clocks in each NAVSTAR satellite are kept accurately synchronized with each other. Timing signals (using the technique of pseudo-random-noise or PRN data modulation on a carrier) are thus transmitted "simultaneously" from all satellites. The user measures the time of arrival of these signals, as compared to his own clock. Since his own clock will not in general be synchronized to the NAVSTAR satellite clocks, this synchronization must somehow be determined. There are two possibilities. Either an extra NAVSTAR passive ranging measurement can be used (self synchronization), or else some external method of synchronization can be used. In the latter case, an atomic clock is required by the user.

Passive ranging has been in use for some time with the Loran-C radionavigation system (Grant, 1976). In this case as well, synchronization can be accomplished internally (using an extra Loran-C range), or externally (using position fixes from some other system to "calibrate" the clock).

1.3 Study outline.

There are five ways in which NAVSTAR ranges can be used:

- i) 3D fix with self-synchronization (requires four or more satellites).
- ii) 3D fix with external synchronization (requiring three or more satellites).
- iii) 2D fix with self-synchronization (requires three or more satellites).
- iv) 2D fix with external synchronization (requires two or more satellites).
- v) fix from combination of NAVSTAR with some other system (requires one or more satellites).

In this study we confine our interest to the last three possibilities.

In section 2 we develop the mathematical models required to compute a 2D error ellipse, given NAVSTAR satellite almanacs, user's position, and a passive ranging error model.

In section 3 we consider a selection of error models for passive ranging NAVSTAR, Loran-C, and user's clock synchronization.

In section 4 we present results of our analysis of NAVSTAR performance as a function of time, as a function of position (considering locations off Canada's east, north and west coasts, and in the north Atlantic), as a function of error model (isolating the effect of various factors in the error model), and in combination with Loran-C.

Details of these results, plotted and in tabular form, are contained in the appendices, as are the program listings used.

2. Mathematical models

2.1 NAVSTAR Satellite Positions.

The GPS user continuously receives navigation information from the GPS satellites in the form of data bits modulated on the received signals. This information includes the satellite's time, its clock correction and ephemeris parameters, almanacs and health for all GPS satellites (Van Dierendonck et al, 1978).

The satellite ephemeris presentation model is characterized by a set of parameters that is an extension of Keplerian elements plus secular drift terms and harmonic coefficients (ibid). The definitions of these parameters are given on Table 1. The mathematical models necessary for the determination of satellite positions into earth-fixed cartesian coordinates at specific transmission epochs are presented in a step by step fashion in Table 2.

2.2 Satellite Visibility Check

Because of the very high frequency of the GPS signals, visibility of GPS satellites is limited to the line of sight reception. To test for satellite visibility it is necessary to consider the coordinates of the satellite with respect to the observer's position on the surface of the earth.

The relative position of a satellite at $X_{S_i} = (x_{S_i}, y_{S_i}, z_{S_i})^T$ with respect to an observer given by $(\phi_{obs}, \lambda_{obs}, h_{obs})$ or by $X_{obs} = (x_{obs}, y_{obs}, z_{obs})^T$ is given by (Krakiwsky and Wells, 1971)

$$X_i^{AT} = X_{S_i}^{AT} - X_{obs}^{AT} \quad (1)$$

where the superscript AT denotes the Average Terrestrial Coordinate System. After transformation to the observer's topocentric (local geodetic) system we have

TABLE I.

GPS Ephemeris Representation Parameters

M_0	Mean Anomaly at reference time.
Δn	Mean Motion difference from computed value.
e	Eccentricity.
\sqrt{a}	Square root of semi-major axis.
Ω_0	Right Ascension at reference time.
i_0	Inclination Angle at reference time.
ω	Argument of the Perigee.
$\dot{\Omega}$	Rate of Right Ascension.
C_{uc}, C_{us}	Cosine and Sine harmonic correction terms to the argument of latitude.
C_{rc}, C_{rs}	Cosine and sine harmonic correction terms to the orbit radius.
C_{ic}, C_{is}	Cosine and sine harmonic correction terms to the inclination.
t_{oe}	Ephemeris reference time.

TABLE 2

GPS satellite positions computation from broadcast ephemeris

$\mu = 3.986008 \cdot 10^{14} \text{ m}^3/\text{sec}^2$	Universal Gravitational Constant (WGS 72)	
$\omega_e = 7.292115147 \cdot 10^{-5} \text{ rad/sec}$	Earth's rotation rate (WGS 72)	
$a = (\sqrt{a})^2$	Semi-major axis.	
$n_0 = \sqrt{\mu/a^3}$	Computed Mean Motion	
$t_k = t - t_{oe}$	Time from reference epoch	
$n = n_0 + \Delta n$	Corrected Mean Motion	
$M_k = M_0 + nt_k$	Mean Anomaly	
$M_k = E_k - e \sin E_k$	Kepler's equation for eccentric anomaly.	
$\left. \begin{aligned} \text{COSV}_k &= (\cos E_k - e)/(1 - e \cos E_k) \\ \text{SINV}_k &= \sqrt{1-e^2} \sin E_k / (1 - e \cos E_k) \end{aligned} \right\}$	True Anomaly	
$\phi_k = V_k + \omega$	Argument of latitude.	
$\delta u_k = C_{uc} \cos 2\phi_k + C_{us} \sin 2\phi_k$	Correction to the argument of latitude	} 2nd harmonic perturbations
$\delta r_k = C_{rc} \cos 2\phi_k + C_{rs} \sin 2\phi_k$	Correction to the orbit radius	
$\delta i_k = C_{ic} \cos 2\phi_k + C_{is} \sin 2\phi_k$	Correction to the inclination angle	
$u_k = \phi_k + \delta u_k$	Corrected argument of latitude	
$r_k = a(1 - e \cos E_k) + \delta r_k$	Corrected orbit radius	
$i_k = i_0 + \delta i_k$	Corrected inclination	
$\left. \begin{aligned} x_k &= r_k \cos u_k \\ y_k &= r_k \sin u_k \end{aligned} \right\}$	Position in orbital plane	
$\Omega_k = \Omega_0 + (\dot{\Omega} - \omega_e)t_k - \omega_e t_{oe}$	Corrected longitude of ascending node	
$\left. \begin{aligned} X_k &= x_k \cos \Omega_k - y_k \cos i_k \sin \Omega_k \\ Y_k &= x_k \sin \Omega_k + y_k \cos i_k \cos \Omega_k \\ Z_k &= y_k \sin i_k \end{aligned} \right\}$	Earth fixed coordinates	

$$X_i^{\text{Topo}} = P_2 R_2 (\phi_{\text{obs}} - 90^\circ) R_3 (\lambda_{\text{obs}} - 180^\circ) X_i^{\text{AT}} \quad (2)$$

where P_2 represents a reflection on the y -axis, and R_2, R_3 represent rotations about the y and z axes respectively.

Once the position vector X_i^{Topo} is computed, visibility is only possible if

$$z_i^{\text{Topo}} \geq 0 \quad (3)$$

The azimuth of a visible satellite is then given by

$$A = \tan^{-1} \frac{y}{x} \quad (4)$$

and its elevation angle is given by

$$E = \tan^{-1} \frac{z}{(x^2 + y^2)^{\frac{1}{2}}} \quad (5)$$

2.3 Positioning Design Matrix

As already stated earlier NAVSTAR positioning depends on passive ranging measurements, also known as pseudo-range measurements. These are defined as the transit times of the satellite generated signals as observed by the user and scaled by the speed of light c . For a given observation, the true slant range R is represented by the equation

$$R = C(t_R - t_T) + e \quad (6)$$

Where t_R is the GPS received time, t_T is the GPS transmission time and e is the measurement error due to atmospheric delay, measurement noise and other user errors. The corresponding pseudo-range measurement is described as

$$\tilde{R} = R + C(\Delta t_u - \Delta t_s) + e \quad (7)$$

where Δt_s and Δt_u are the satellite's and user's clock offsets from the GPS reference time. The range R may be expressed in terms of the navigator's coordinates and the satellite position, so that the equation

$$F(X,L) \equiv \sqrt{(X_s - X_{OBS})^2 + (Y_s - Y_{OBS})^2 + (Z_s - Z_{OBS})^2} + c\Delta t_u - c\Delta t_{s_i} + e_i - \tilde{R}_i, \quad i = 1, 2, \dots, n \quad (8)$$

summarizes the information from n satellites which is required for the computation of user position and user clock bias. The n equations represented by eqn. (8) can be linearized on the usual way using a first order Taylor series expansion about an approximate user position and clock bias X^o . The linearized equations can then be written in expanded matrix form as

$$A\delta + BV + W = 0 \quad (9)$$

where δ is a vector of corrections to the user's position and clock bias, V is the vector of residuals, W is the misclosure vector and A and B are design matrices with

$$B \equiv I \quad (10a)$$

and

$$A = \left. \frac{\partial F}{\partial X} \right|_{X^o} \quad (10b)$$

In the 2-D case we consider here the design matrix A has rows having three elements such that

$$A_t = \left[\frac{\partial F}{\partial \phi} \quad \frac{\partial F}{\partial \lambda} \quad \frac{\partial F}{\partial \Delta t_u} \right]_t \quad (11)$$

where t denotes time epoch and

$$\frac{\partial F}{\partial \phi} = \left[\frac{\partial F}{\partial x_t^o} \quad \frac{\partial F}{\partial y_t^o} \quad \frac{\partial F}{\partial z_t^o} \right] \frac{\partial}{\partial \phi} \begin{bmatrix} x_t^o \\ y_t^o \\ z_t^o \end{bmatrix} \quad (12a)$$

$$\frac{\partial F}{\partial \lambda} = \left[\frac{\partial F}{\partial x_t^o} \quad \frac{\partial F}{\partial y_t^o} \quad \frac{\partial F}{\partial z_t^o} \right] \frac{\partial}{\partial \lambda} \begin{bmatrix} x_t^o \\ y_t^o \\ z_t^o \end{bmatrix} \quad (12b)$$

$$\frac{\partial F}{\partial \Delta t_u} = c \quad (12c)$$

where the partial derivatives involved are given in Krakiwsky and Wells (1971) and McCaskill et al (1978) as

$$\frac{\partial F}{\partial X} = - \frac{X_s - X_{obs}^o}{R^o} \quad (13a)$$

$$\frac{\partial F}{\partial Y} = - \frac{Y_s - Y_{obs}^o}{R^o} \quad (13b)$$

$$\frac{\partial F}{\partial Z} = - \frac{Z_s - Z_{obs}^o}{R^o} \quad (13c)$$

$$\frac{\partial x}{\partial \phi} = \left[\frac{a}{(1-e^2 \sin^2 \phi)^{1/2}} + h \right] \sin \phi \cos \lambda + \frac{ae^2 \sin \phi \cos^2 \phi \cos \lambda}{(1-e^2 \sin^2 \phi)^{3/2}} \quad (14a)$$

$$\frac{\partial y^o}{\partial \phi} = - \left[\frac{a}{(1-e^2 \sin^2 \phi)^{1/2}} + h \right] \sin \phi \sin \lambda + \frac{ae^2 \sin \phi \cos^2 \phi \sin \lambda}{(1-e^2 \sin^2 \phi)^{3/2}} \quad (14b)$$

$$\frac{\partial z_t^o}{\partial \phi} = \left[\frac{a}{(1-e^2 \sin^2 \phi)^{1/2}} + h - \frac{ae^2}{(1-e^2 \sin^2 \phi)^{1/2}} \right] \cos \phi + \frac{ae^2 (1-e^2) \sin^2 \phi \cos \phi}{(1-e^2 \sin^2 \phi)^{3/2}} \quad (14c)$$

$$\frac{\partial x_t^o}{\partial \lambda} = \left[\frac{a}{(1-e^2 \sin^2 \phi)^{1/2}} + h \right] \cos \phi \sin \lambda \quad (14d)$$

$$\frac{\partial Y_t^o}{\partial \lambda} = \left[\frac{a}{(1-e^2 \sin^2 \phi)^{\frac{3}{2}}} + h \right] \cos \phi \cos \lambda \quad (14e)$$

$$\frac{\partial Z_t^o}{\partial \lambda} = 0 \quad (14f)$$

2.4 Covariance Matrix of Position

Assuming that a weight matrix P is given for the errors corresponding to the n simultaneous (or near simultaneous) pseudo-range measurements to the n satellites, the estimate of δ is given by

$$\hat{\delta} = (A^T P A)^{-1} A^T P W \quad (15)$$

and the covariance of the corresponding error in the estimate of δ is given by

$$C_{\hat{\delta}} = (A^T P A)^{-1} \quad (16)$$

which is also the covariance of the adjusted solution vector

$$\hat{X} = X^o + \hat{\delta}$$

Once the covariance matrix of position matrix of position has been computed from eqn.(16) corresponding error ellipses can be computed in the usual manner whereby the semi-major (α) and semi-minor (β) axes are given by

$$\alpha = \left[\frac{\sigma_{\phi} + \sigma_{\lambda}}{2} + \sqrt{\frac{(\sigma_{\lambda} - \sigma_{\phi})^2}{4} + \sigma_{\phi\lambda}^2} \right]$$

$$\beta = \left[\frac{\sigma_{\phi} + \sigma_{\lambda}}{2} - \sqrt{\left(\frac{\sigma_{\lambda} - \sigma_{\phi}}{4} \right)^2 + \sigma_{\phi\lambda}^2} \right]$$

and the orientation of the error ellipse is given by

$$\theta = \frac{1}{2} \tan^{-1} \frac{2\sigma_{\phi\lambda}}{\sigma_{\lambda} - \sigma_{\phi}}$$

3. Error models

3.1 NAVSTAR Error Models

The level of navigation performance with the GPS is a direct result of the waveform characteristics of the GPS satellite signals. Operation with either the P or C/A code to a large extent establishes the navigation accuracy level which can be achieved by the user. The environmental medium and propagation link in which the signals are transmitted and received are also significant performance constraints on GPS. The basic NAVSTAR error models and the term which may be employed in a performance analysis have been discussed by Martin (1978), and also by Gilbert (1979). A summary of this error budget, which was also used for the present analysis, is given in table 3.

3.2 LORAN-C Error Models

Examining the combined performance of GPS with LORAN-C associated standard deviations for the LORAN ranges were computed using the empirical relationship (pers.comm. Grant)

$$\sigma_L = 100 / \sqrt{\text{SNR}} \quad (\text{m})$$

where SNR is the signal-to-noise ratio of the measured ranges which can typically be 0.5 for a weak signal or 10.0 for a strong signal. From recent operations on Davis Strait the accuracy of LORAN ranging to Saglek, Cape Race and Angissoq was of the order of 100 to 280 m, from table 4. For the present analysis LORAN ranging to Cape Race, Angissoq and Sandur was assumed with obtainable accuracies of ~ 140 m, i.e. SNR = 0.5

TABLE 3.

GPS Error Budget expressed as
uncorrelated equivalent range errors (m)

	P-Code	C/A-Code
Satellite Ephemeris	1.5	1.5
Satellite Clock Delay	0.9	0.9
Pseudorange Noise	1.0	10.0
Range Quantization	0.3	0.3
Mechanization	1.0	10.0
Ionospheric Dual Frequency Compensation	3.0	
Uncompensated ionospheric delay		
Daytime		5.0 to 15.0
Nighttime		0.5 to 1.5
Tropospheric Delay	1.0	1.0
Multipath	1.2	5.0
Rms	4.0 m	16 to 21 m

TABLE 4

Loran Measurements in Davis Strait*
($\phi = 66^\circ 45'$)

To	Noise N	S/N = 128/N	$\sigma_L = 100/\sqrt{S/N}$
Saglek	1000	0.13	280 m
Cape Race	377	0.34	170 m
Angissoq	135	0.95	100 m

* After Grant (October 1980, personnel communication).

3.3 Clock synchronization Error

To further enhance the analysis of the NAVSTAR navigation performance it was assumed that clock synchronization can be retained within 0.3 μsec (~ 100 m in equivalent range) and that the navigator knows his position within 10° in ϕ and λ .

This information was incorporated into the model by treating ϕ , λ and Δt_u as "pseudo-observables" with weight matrix P_x , and rewriting equation (16) as

$$\hat{C}_\delta = (A^T P A + P_x)^{-1}$$

4. Results

Some aspects of the nature of GPS orbits and the combination of their lines of position are discussed in section 4.1.

For the purposes of this report, GPS performance was measured by the length of the semi-major axis of the error ellipse computed as described in section 2.4. This performance was evaluated as a function of time, as a function of position, and as a function of error model, both alone and in combination with LORAN-C. Results are given in Sections 4.2, 4.3 and 4.4.

For the purposes of this report, LORAN-C transmitters were treated as "stationary" GPS satellites, located on the surface of the earth. That is rho-rho LORAN-C was treated as measuring chord distances through the earth, rather than geodesic distances over the surface of the earth. This introduces a spurious dip of up to 10° below the horizon for the range vector, but this will propagate only weakly into the determination of the two-dimensional horizontal design matrix in equation 16.

4.1 GPS orbit geometry

Because of their high altitude (20,000 km) GPS spacecraft are visible at spherical distances of up to 76° .

Due to their twelve hour orbital period and the small precession of their orbit planes, GPS satellites ground tracks repeat from day to day nearly exactly.

Due to their 63° orbit plane inclination and twelve hour period, the GPS ground tracks plot almost like a square wave on a mercator plot. In contrast to Transit satellite ground tracks, GPS ground tracks move from west to east. Figures 1 and 2 show GPS ground tracks plotted on a polar

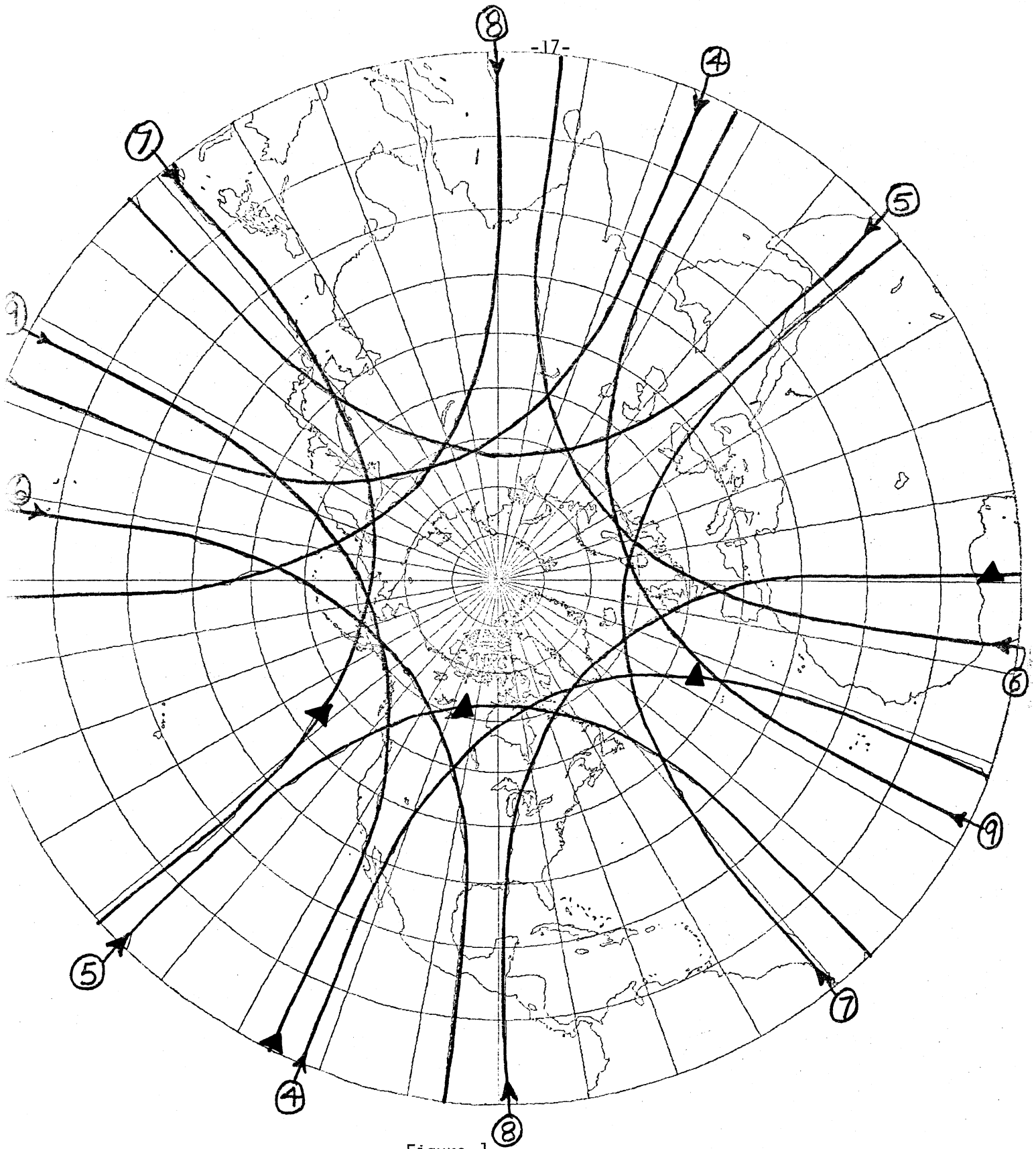


Figure 1.
 SUBTRACKS OF SIX GPS
 SPACE VEHICLES IN ORBIT
 AS OF 1 OCTOBER 1980.
 SHOWING VISIBLE SVS FROM
 65°N, 60°W, AS OF 00:19 UT

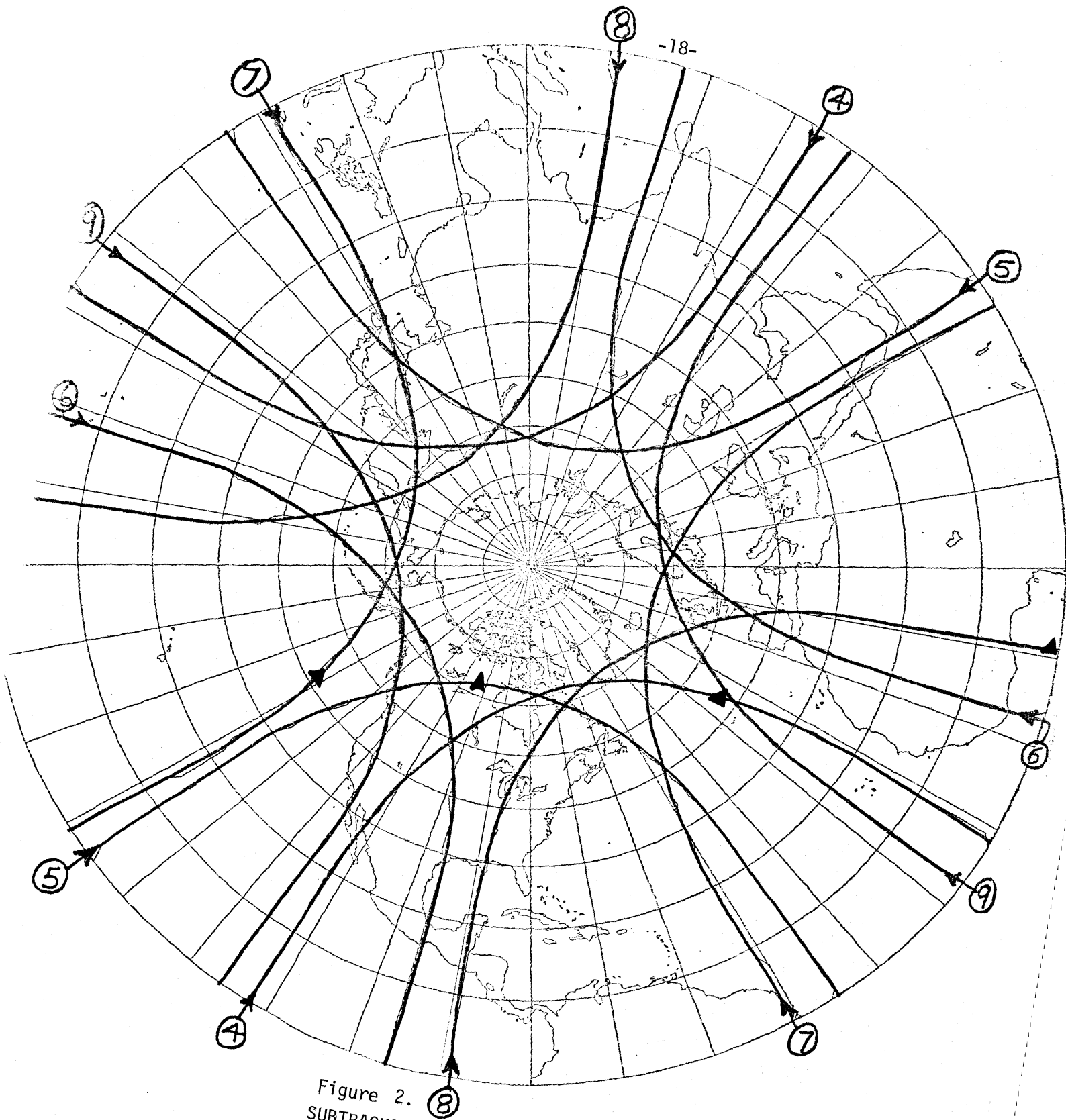


Figure 2. SUBTRACKS OF SIX GPS SPACE VEHICLES IN ORBIT AS OF 1 OCTOBER, 1980. SHOWING VISIBLE SVS FROM 65°N, 60°W, AS OF 0024 UT

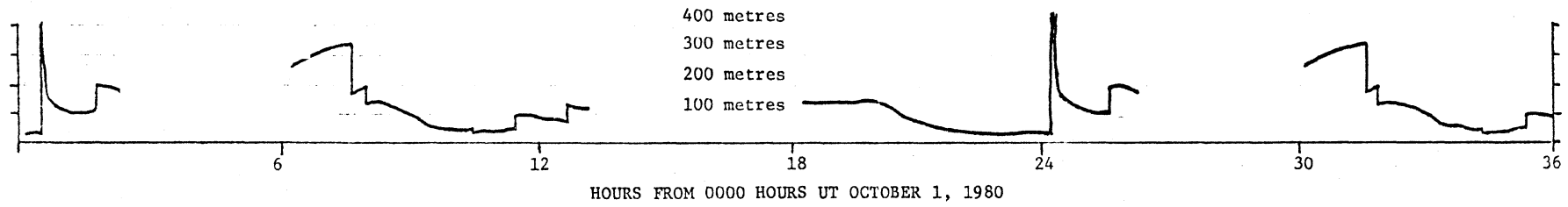
stereographic projection.

The combination of lines of position from GPS satellites at a given tracking station changes with time as satellites rise and set over the horizon, and change position relative to each other and to the tracking station. In particular, if a satellite providing a particularly strong geometry sets, the combined positional accuracy may change dramatically. Figures 1 and 2 illustrate an example of this. Figure 1 shows the five GPS satellites visible from Davis Strait (65°N , 60°W) as of 0019 hours on 1 October 1980. Note that satellites 7,5,4 and 8 are almost collinear with Davis Strait, but satellite 9 is not. Figure 2 shows the situation five minutes later. Satellite 9 has set and the remaining satellites are even more collinear with Davis Strait. The error ellipse semi major axes at Davis Strait corresponding to Figures 1 and 2 respectively are 31 and 414 metres.

Figure 3 shows a 36 hour record of this semi major axis at Davis Strait. Each of the discontinuities corresponds to the rise or set of a satellite which significantly changes the strength of the geometry.

FIGURE 3.

SEMI-MAJOR AXIS OF ERROR ELLIPSE USING GPS ALONE (IF MORE THAN 3 SATELLITES) AND IN COMBINATION WITH LORAN-C (IF FEWER)
FOR DAVIS STRAIT (65°N, 60°W) USING P-CODE



4.2 GPS performance as a function of time

There are three aspects to this analysis. Most important is the variation in GPS performance during a 24 hour cycle. Second is the variation from day to day, and third is the variation from year to year.

The present constellation of six satellites was assumed throughout. The performance during a 24 hour cycle is characterized by periods of no satellites, periods of excellent multisatellite geometry, and periods in between these extremes. Performance characteristics were computed at five minute intervals for 24 hour time spans. Appendix C contains the results. The performance characteristics used are the combined error ellipse semi-major axis, semi-minor axis, and orientation; the number of satellites visible; and the elevation, azimuth, and subtrack latitude and longitude for each visible satellite.

A typical plot of the error ellipse semi-major axis is shown in figure 3. A full set of plots is contained in Appendix B.

Plots of the portion of each day for which GPS provides a specified accuracy (as measured by the error ellipse semi-major axis) are shown in figures 4,5,6 and 7, 8 and 9.

Analysis of the variation from day to day and year to year is limited by the fact that only one set of GPS almanacs was available, and these almanacs accurately represent actual GPS orbits only at the time of transmission. According to van Dierendonk (1978) the almanac error is 1 km after 1 day and 20 km after 5 weeks. A time series of almanacs would be required for a more detailed analysis.

From the 36 hour results listed in Appendix B, it can be seen that the orbit periods differ by a few minutes from exactly 24 hours. This is equivalent to an along track precession of several hundred kilometers (at

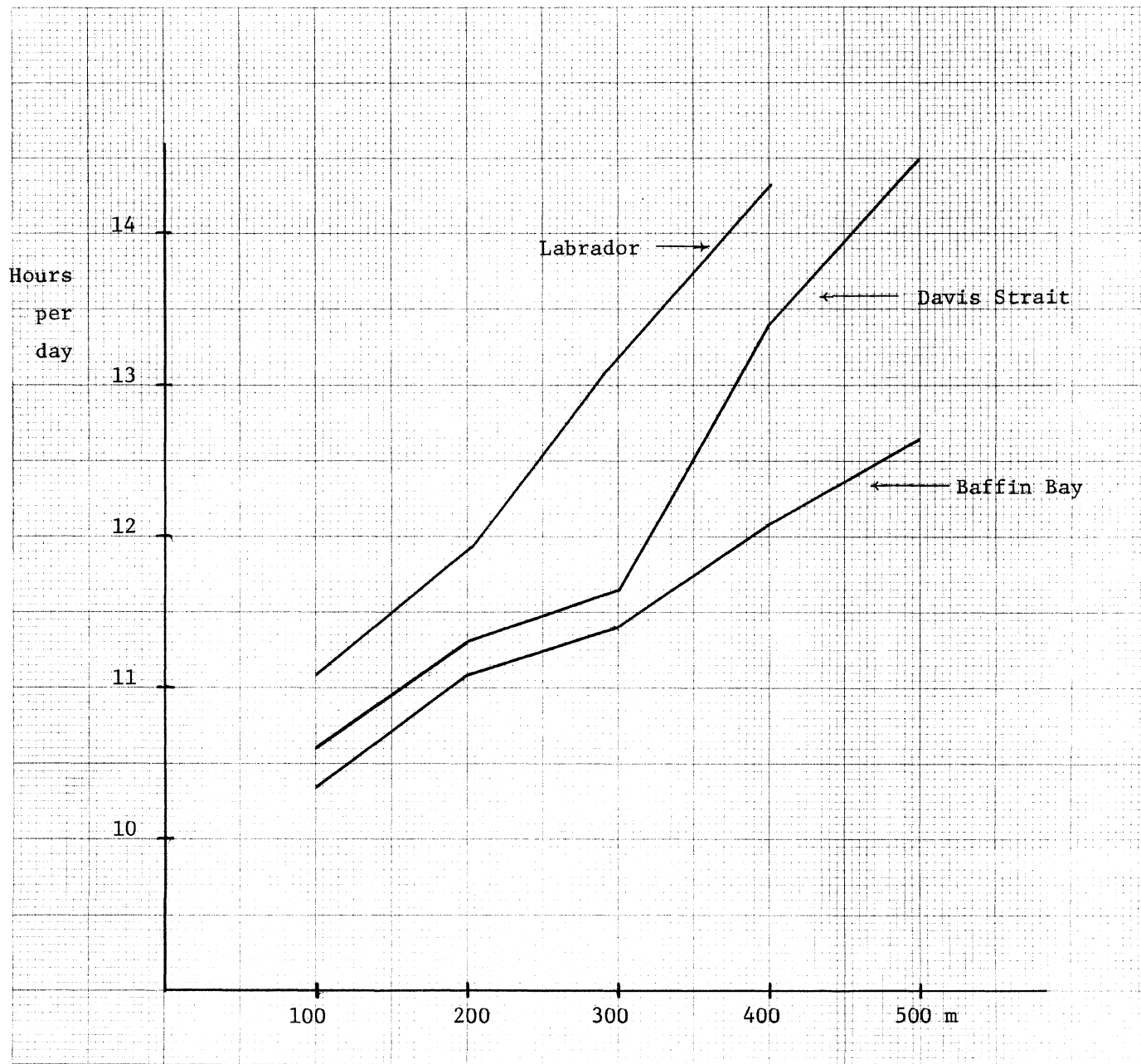


Figure 4

GPS performance as a function of position

Hours per day for which the GPS P-code ranging error ellipse semi-major axis is below a specified value.

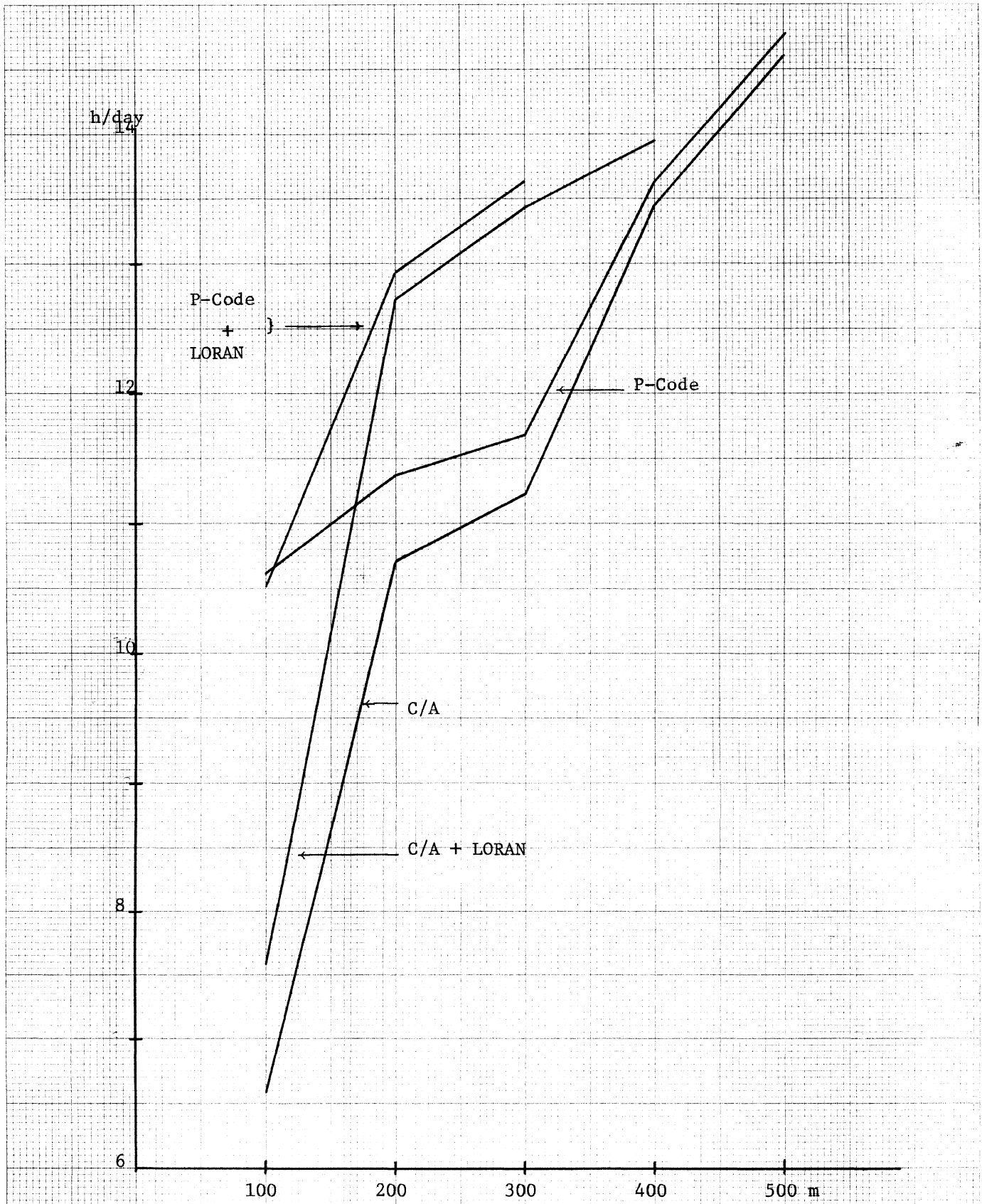


Figure 5.

GPS performance as a function of error model for Davis Strait. Hours per day for which the GPS/loran error ellipse semi-major axis is below a specified value.

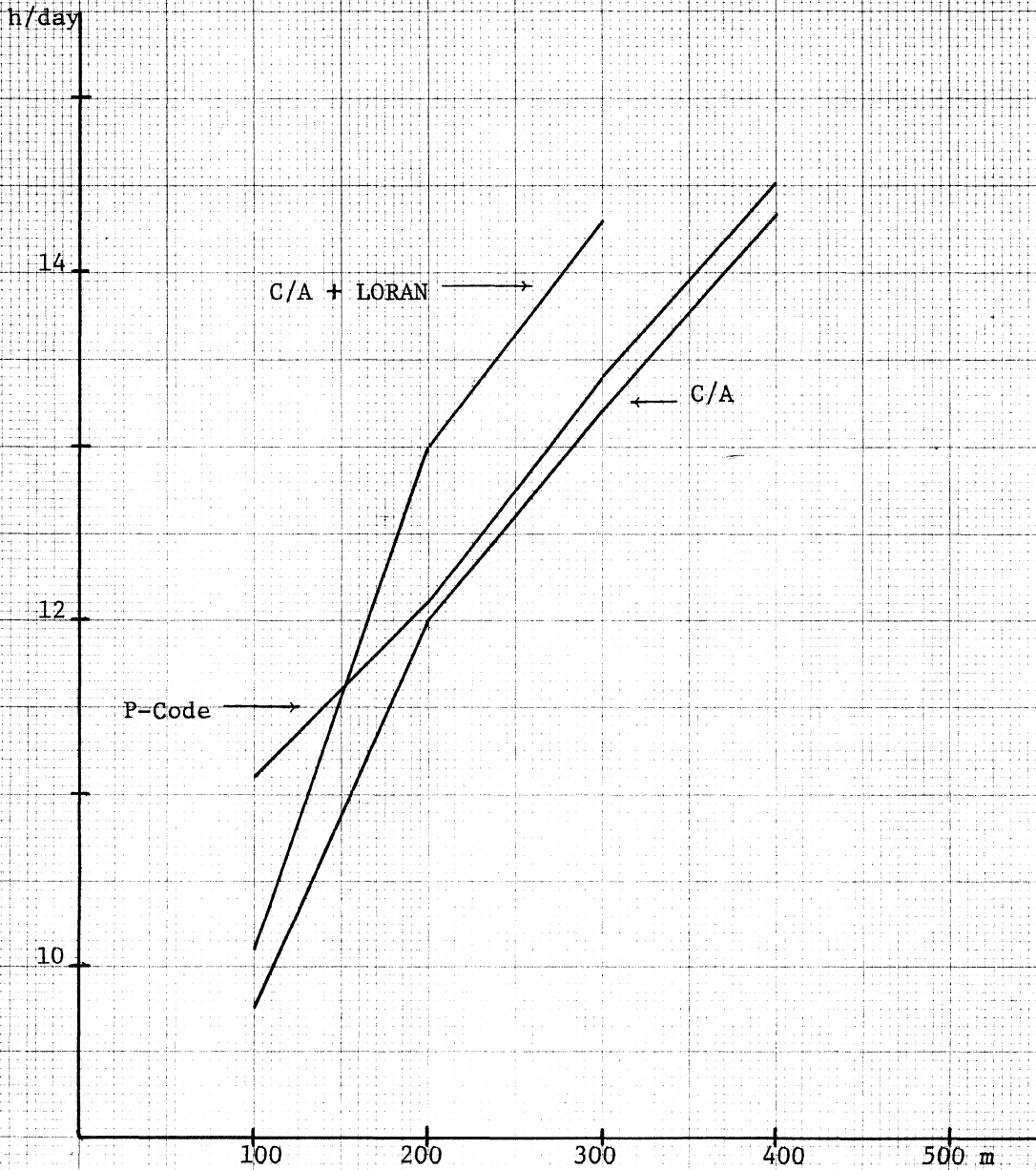


Figure 6.
GPS performance as a function of error model for Labrador sea. Hours per day for which GPS/LORAN error ellipse semi-major axis is below a specified value.

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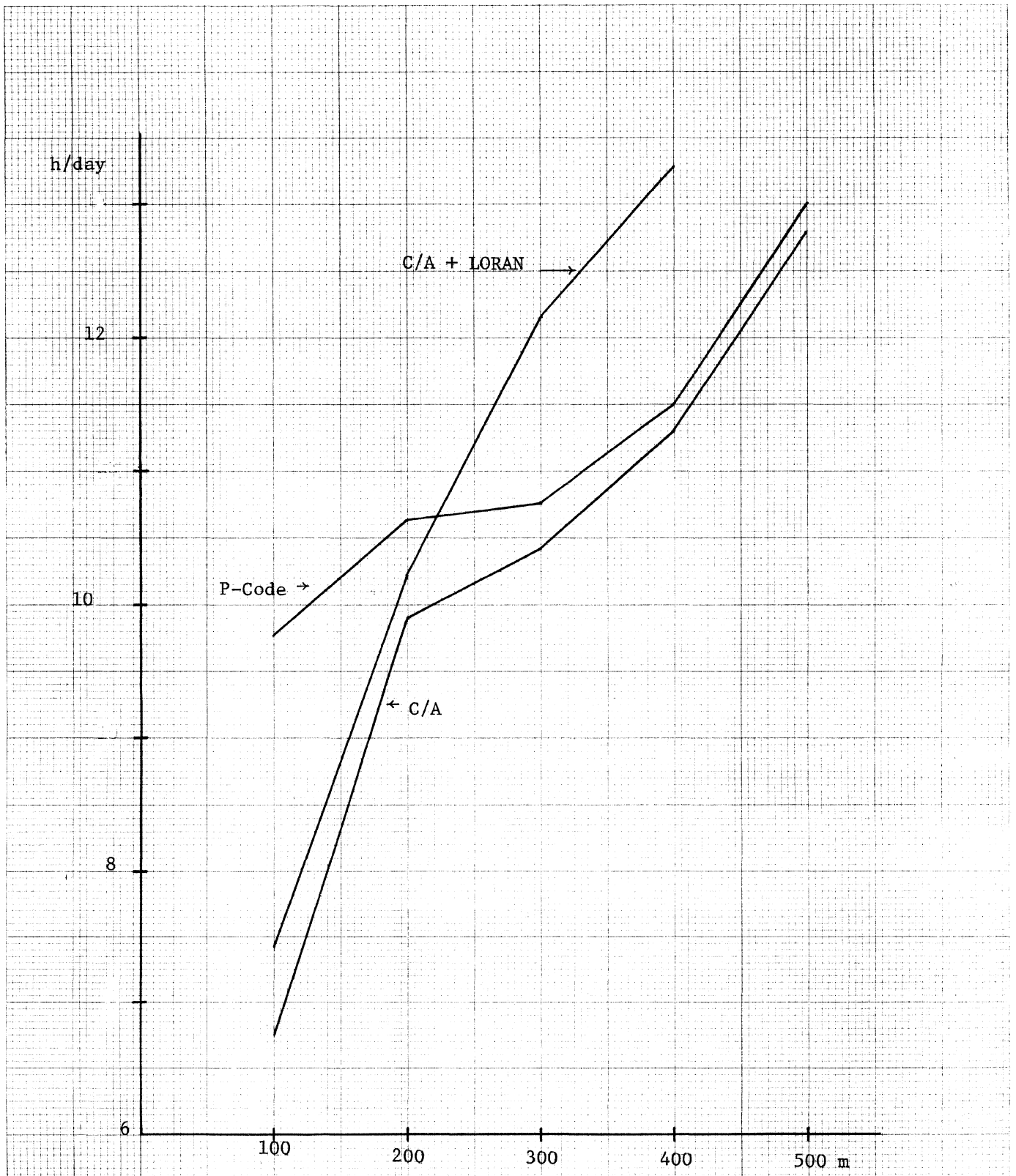


Figure 7
 GPS Performance as a function of error model for Baffin Bay. Hours per day for which GPS/LORAN error ellipse semi-major axis is below a specified value.

KEYSTONE

NO. 2 GRAPH SHEET B¹/₂ X 11 20 DIVISIONS TO INCH

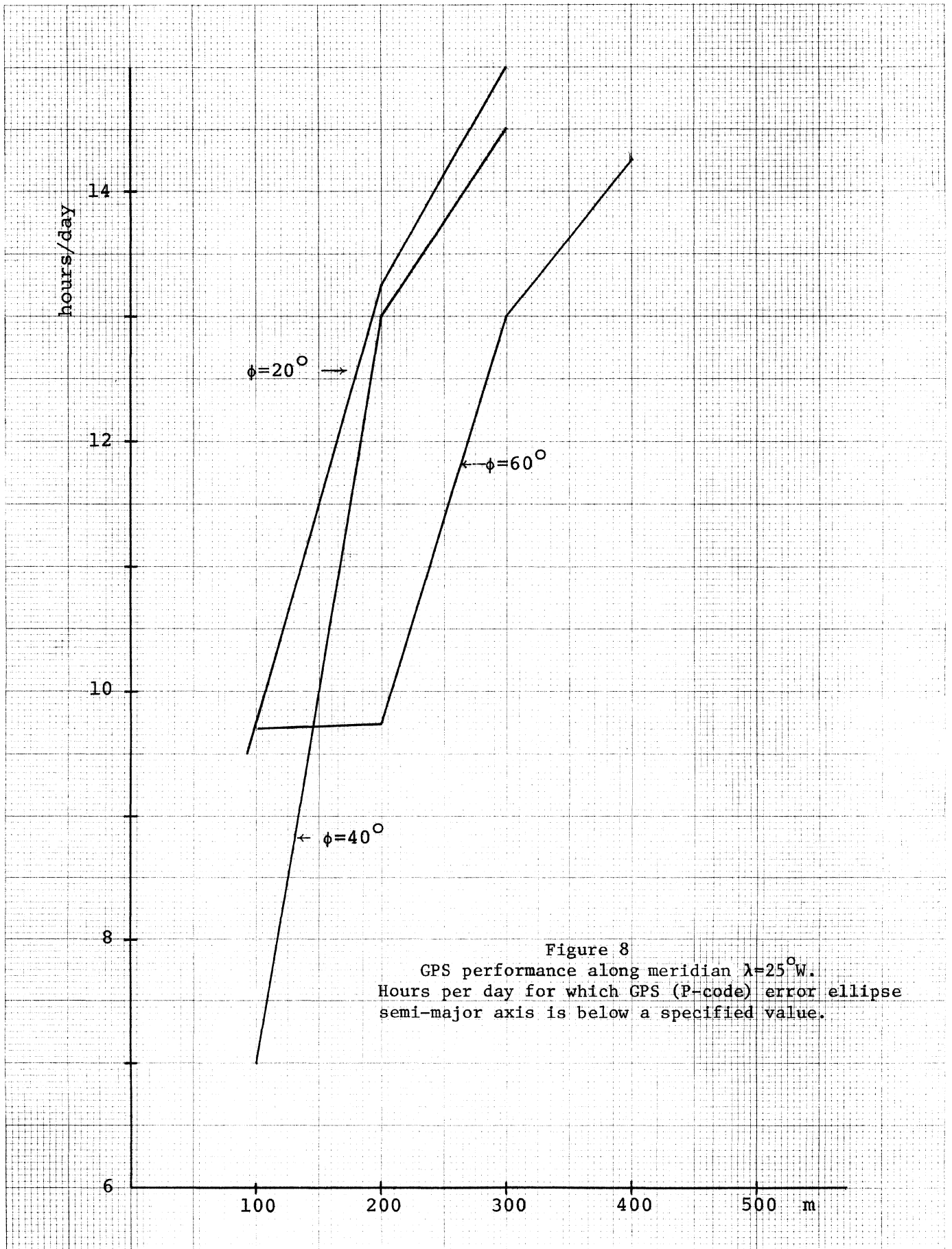


Figure 8
 GPS performance along meridian $\lambda=25^\circ W$.
 Hours per day for which GPS (P-code) error ellipse
 semi-major axis is below a specified value.

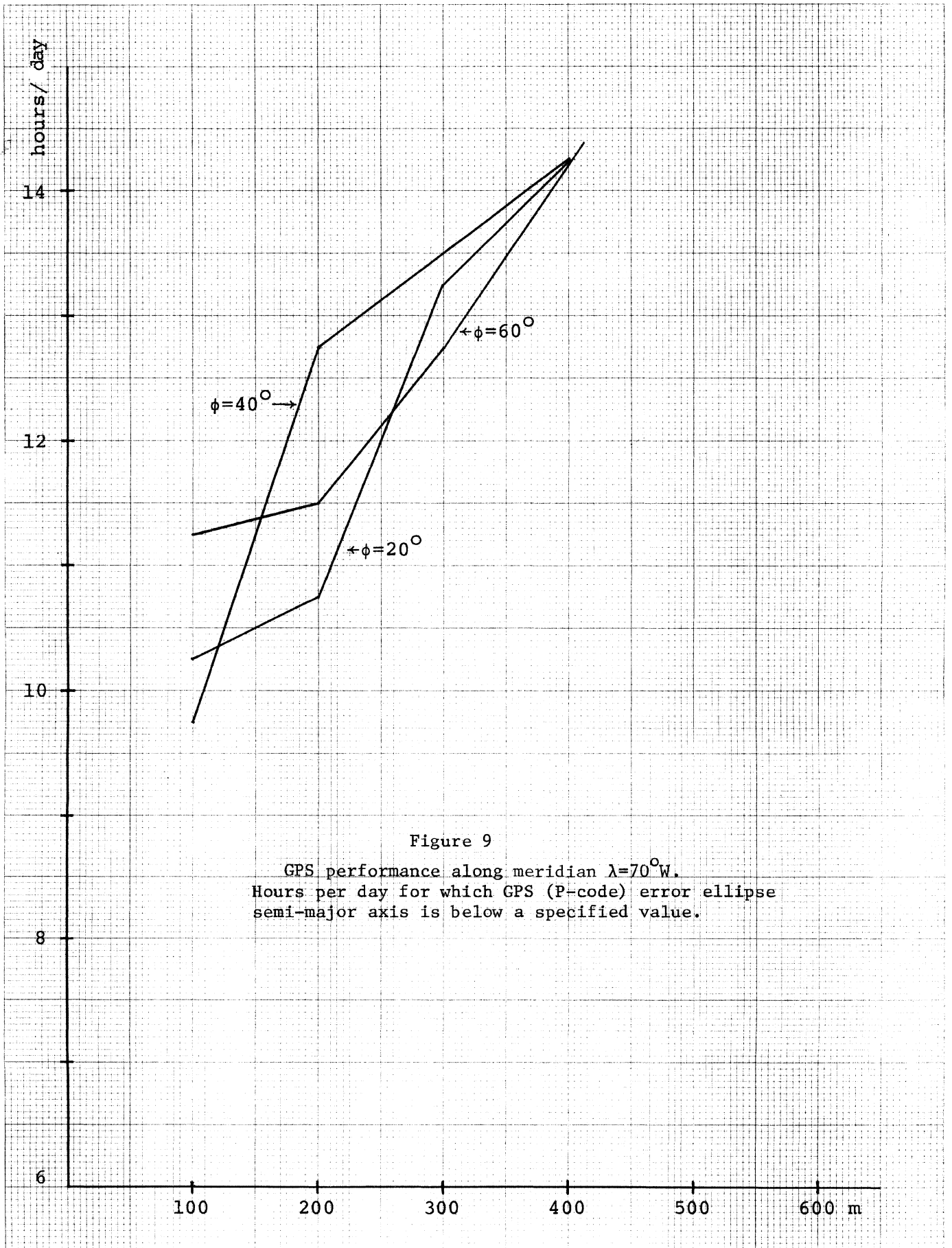


Figure 9
 GPS performance along meridian $\lambda=70^\circ W$.
 Hours per day for which GPS (P-code) error ellipse
 semi-major axis is below a specified value.

orbit altitude) per day. This appears to be outside the error of the almanacs, and hence probably represents a real (but slight) change in the orbit configurations from day to day.

A special run was made, using the same almanacs, for 1 October, 1981, and compared with the 1980 results. This indicated that the orbit planes precess by a few degrees per year. This is likely within the error of the almanacs, and no firm conclusion should be drawn.

4.3 GPS performance as a function of position

Three tracking station positions were selected for analysis. They are Labrador (55°N, 65°W), Davis Strait (65°N, 60°W) and Baffin Bay (70°N, 68°W). The results are contained in Appendix B.

Figure 4 compares GPS performance at each of these three positions, expressed in terms of the number of hours per day that GPS accuracy measured by the error ellipse semi-major axis) was below a specified value. For example, from this preliminary analysis GPS accuracy is predicted to be 150 metres or better for 11.5, 11.0 and 10.75 hours per day at Labrador, Davis Strait and Baffin Bay respectively.

4.4 GPS performance as a function of error model

Two simple error models were chosen for GPS ranges, using the data of Table 3. P-code ranging was assumed to have a standard deviation of 4 metres, and C/A-code ranging standard deviation to be 16 metres.

Rho-Rho LORAN-C ranging from Angissoq and Cape Race were both assumed to have standard deviations of 140 metres at all tracking stations. According to the data of Table 4 this was probably a reasonable choice for Davis Strait. It is probably too pessimistic for Labrador. Baffin Bay is probably beyond the groundwave range for Angissoq and Cape Race.

A priori standard deviations of 10° in latitude and longitude were assigned to the tracking station coordinates. An a priori standard deviation of the tracking station clock synchronization, expressed in terms of equivalent range, of 100 metres was assumed.

In the absence of these a priori standard deviations (weighted constants) the C/A code error ellipses are exactly four times the size of the P-code error ellipses. However when the weighted constraints are included this is no longer true.

The algorithm chosen for the combination of GPS and LORAN-C was; a) if four or more GPS satellites were visible, a GPS-only error ellipse was computed; b) if one to three GPS satellites were visible a combined GPS-LORAN error ellipse was computed; c) if no GPS satellites were visible, no error ellipse was computed.

Runs were made at each of the three tracking stations for each of three conditions:

- a) P-code ranging without LORAN
- b) C/A-code ranging without LORAN
- c) C/A-code ranging with LORAN

The results are summarized in Figures 5,6 and 7. Figure 5 alone shows results from P-code ranging with LORAN. Figure 5 indicates that 150 metre or better positioning is predicted for 8.5, 10.0, 11.0 and 11.75 hours per day at Davis Strait, using C/A only, C/A + LORAN, P only and P with LORAN respectively.

The weighted constraint of 100 metres equivalent range (or 0.33 microseconds) on the clock synchronization implies the use of an atomic frequency standard, and of some external method of maintaining synchronization (for example Transit fixes to check GPS range measurements). However, as long as there are three or more GPS satellites with good geometry, the GPS-only solution for synchronization overwhelms the influence of this weighted constraint. From two special runs at Davis Strait with this constraint removed, 150 metre or better positioning is predicted for 11.0 and 11.3 hours per day using P code only and P code with LORAN. This is essentially unchanged from the previous results. On the other hand a priori knowledge of the clock synchronization as represented by this weighted constraint does mean that GPS fixes are possible with only two satellites.

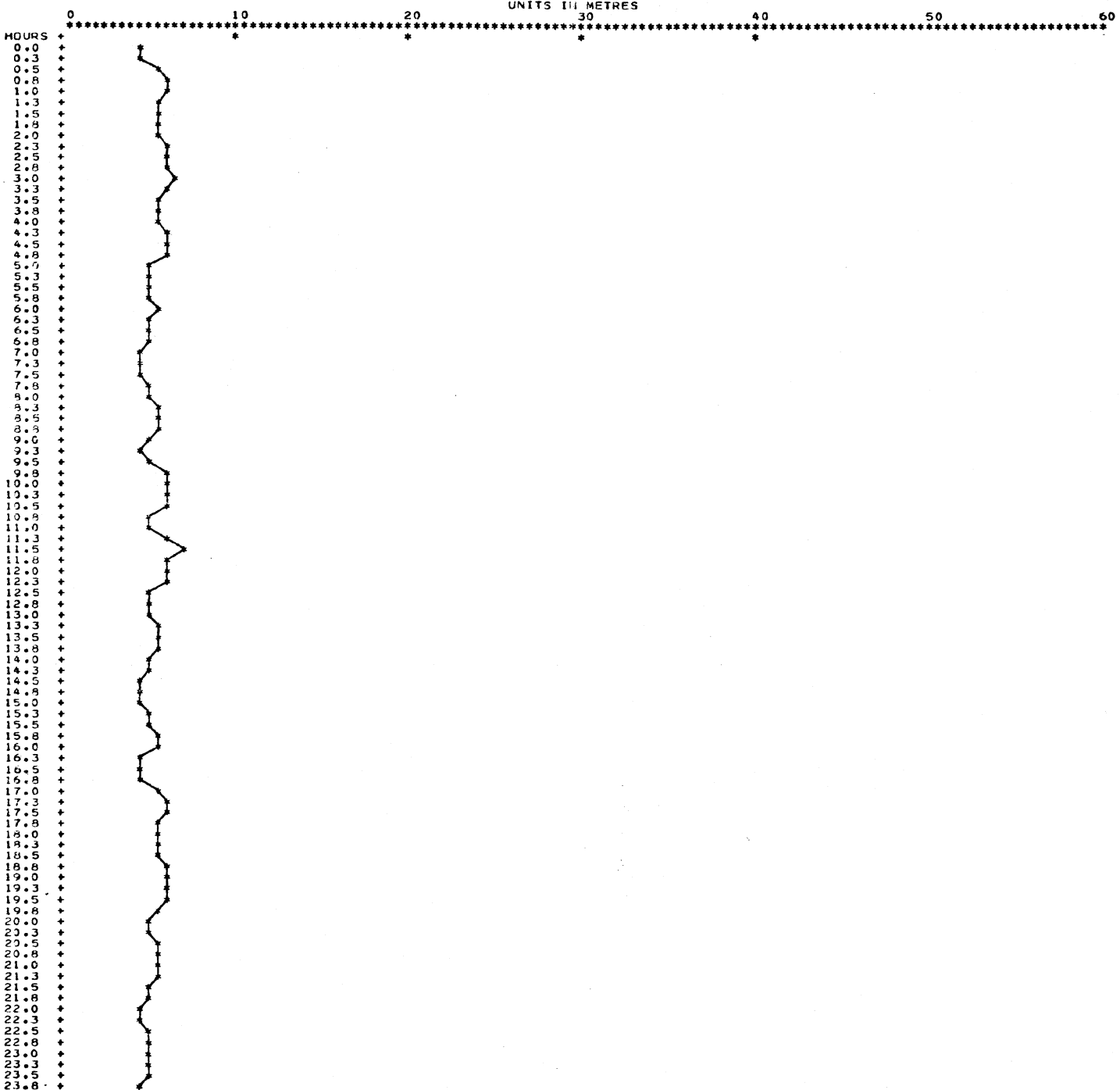
4.5 Fully implemented GPS performance

The performance of a full GPS constellation of 24 satellites was simulated by generating almanacs for satellites spaced 45° apart in mean anomaly M_0 , in each of three orbit planes separated in right ascension by 120° and inclined at 63° .

For this analysis, all visible satellites were used in a two dimensional position fix, with the clock synchronization constrained as above. This of course differs from the usually proposed mode of four parameter fixes (three dimensions plus clock synchronization) using only the best four of the available satellites.

Using P-code only, the results shown in Figure 10 indicate continuous coverage, with the standard error ellipse semi major axis at about 5 metres.

NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE



Davis Strait (65°N, 60°W) using P-code.
Full satellite constellation.
Figure 10.

5. Conclusions

During the present phase of GPS development, during which only limited GPS coverage is available, the variation in GPS performance has a predominant 24 hour cycle. The nature of this cycle is strongly dependent on the number and relative positions of the GPS satellites, and were weakly dependent on the receiver position.

The 24 hour cycle evolves slightly from day to day as the satellites precess, however more information on the variation of GPS satellite almanac parameters with time is required before firm conclusions can be drawn on the nature of this evolution.

The results presented here predict that the present six-satellite GPS configuration will provide 150 metre or better positioning about 11 hours per day for the area studied (Labrador to Baffin Bay). This coverage degrades slightly as latitude of the tracking station increases, and is worse for C/A-code GPS ranging unaided by LORAN-C.

The main objective of this study was to assess the feasibility of using GPS in its present limited deployment as an operational survey positioning system in the eastern Canadian arctic. Consistent with this objective the mathematical models and error models used, while reasonably realistic, are simple and contain several approximations identified in this report. The principal conclusion of this report then is:

<p>It is feasible to use GPS if 150 metres or better positioning for about 11 hours per day meets the requirements of an operational survey.</p>
--

It is deemed that the approximations used in this analysis will not affect this principal conclusion.

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This Appendix contains a listing of the software used to generate the results in this report. It consists of a main routine and eleven subroutines.

MAIN PROGRAM	A-2
FUNCTION MODUL 0	A-5
SUBROUTINE HHMSS	A-5
SUBROUTINE ROTREF	A-6
SUBROUTINE PLXYZ	A-7
SUBROUTINE XYZPLH	A-7
SUBROUTINE DERIV	A-8
SUBROUTINE SAIVC	A-9
SUBROUTINE MAPMPH	A-10
SUBROUTINE ELIPS	A-10
SUBROUTINE PLINIT	A-11
SUBROUTINE PLOT	A-11

```

IMPLICIT REAL*8(A-H,O-Z)
REAL *8 MO , INC , NO , MK
INTEGER ELEV , AZIM , SLAT , SLON , EA , EB , PHI
C
DIMENSION SLAT(6) , SLON(6)
DIMENSION SIGRG(3) , SIGLRN(2) , PRN(2) , XLAT(3) , XLON(3)
DIMENSION MO( 6) , DN( 6) , E( 6) , A( 6) , CW( 6) , INC( 6) ,
# W( 6) , CWD( 6) , TOE( 6) , ISAT( 6) , NO( 6) ,
# JD( 6) , TJD( 6) , IH( 6) , IM( 6) , IS( 6)
DIMENSION ELEV( 6) , AZIM( 6) , EPOCH( 6) , XS(3)
DIMENSION DA(6,3),ATPA(3,3),IW1(3),IW2(3)
DIMENSION PX(3)
C
COMMON /PLOTS/ XMIN,XMAX
COMMON /ALMNAC/ A, MO , NO , E , W , INC , CW , CWD ,
# TOE , EPOCH , ISAT
C
XMIN=0.D0
XMAX=600.D0
CALL PLINIT(8,120)
PI = DARCOS(-1.D0)
RHO = PI/180.D0
C
DATA ICR /5/ , IPR/6/ , PRN / 8HPRECISE , 8H C/A /
C
REFERENCE ELLIPSOID PARAMETERS
C
DATA GM /3.986008D14/ , WE /7.292115147D-5/
DATA AE / 6378135.D0 / , BE / 6356750.5D0 /
C
DATA XLAT / 46.77560556D0 , 59.98813055D0 , 64.90738333D0 /
DATA XLON / 306.8255111D0 , 314.8257028D0 , 336.0772917D0 /
C
(UNCORRELATED) RANGE ERROR SCHEDULES
C
MCODE = 1 , PRECISE MODE , SIGRG = 4.00 M
C
2 , C/A MODE , SIGRG = 16.00 M
C
3 , SIGRG = 1.00 (IDENTITY WEIGHT MATRIX)
C
SIGRG(1) = 4.00D0
SIGRG(2) = 16.00D0
SIGRG(3) = 1.00D0
C
PX(1) = 1./100.D0
PX(2) = 1./100.D0
PX(3) = 1./10000.D0
C
LORAN RANGE ERROR SCHEDULES
C
MLORN = 1 , WEAK SIGNAL(S/N RATIO SNR=0.5)
2 , STRONG SIGNAL(S/N RATIO SNR=10.0)
C
SIGLRN(1) = 100. / DSQRT(0.5D0)
SIGLRN(2) = 100. / DSQRT(10.D0)
C
DO 20 I = 1,3
XLAT(I) = XLAT(I) * RHO
20 XLON(I) = XLON(I) * RHO
C
READ(ICR,1001) OLAT,OLONG,HT,DAY1,ELMIN,NSAT,MCODE,MLORN,LORAN
IF(OLONG.LT.0.D0) OLONG = OLONG + 360.D0
C
SNR = 0.5
IF(MLORN.EQ.2) SNR = 10.
WRITE(IPR,2016) OLAT,OLONG,PRN(MCODE),SIGRG(MCODE),SNR

```



```

C
C READ SATELLITE ALMANAC
C
C ISAT - SATELLITE NUMBER
C TOE - ALMANAC REFERENCE TIME; TIME OF THE WEEK (SEC)
C A - SQUARE ROOT OF THE SEMI-MAJOR AXIS
C MO - MEAN ANOMALY AT REFERENCE TIME (RAD)
C E - ECCENTRICITY
C W - ARGUMENT OF THE PERIGEE (RAD)
C INC - INCLINATION ANGLE AT REFERENCE TIME (RAD)
C CW - RIGHT ASCENSION AT REFERENCE TIME (RAD)
C CWD - RATE OF RIGHT ASCENSION (RAD/SEC)
C JD - ALMANAC REFERENCE TIME; JULIAN DAY OF YEAR
C TJD - TIME OF JULIAN DAY
C
C DO 10 I = 1, NSAT
C READ(ICR,1000) ISAT(I),TOE(I),A(I),MO(I),E(I),W(I),INC(I),
# CW(I),CWD(I),JD(I),TJD(I)
C NO(I) = DSQRT(GM)/(A(I)**3)
C A(I) = A(I)**2
C EPOCH(I) = DFLOAT(JD(I)) + TJD(I)/86400.
C TOJD = TJD(I)
C CALL HHMSS (TOJD,IH(I),IM(I),IS(I))
10 CONTINUE
C I1 = 1
13 I2 = I1 + 5
C IF(I2.GT.NSAT) I2 = NSAT
C WRITE(IPR,2001) (ISAT(I),I=I1,I2)
C WRITE(IPR,2002) (TOE(I),I=I1,I2)
C WRITE(IPR,2011) (JD(I),IH(I),IM(I),IS(I),I=I1,I2)
C WRITE(IPR,2003) (A(I),I=I1,I2)
C WRITE(IPR,2004) (MO(I),I=I1,I2)
C WRITE(IPR,2005) (E(I),I=I1,I2)
C WRITE(IPR,2006) (W(I),I=I1,I2)
C WRITE(IPR,2007) (INC(I),I=I1,I2)
C WRITE(IPR,2008) (CW(I),I=I1,I2)
C WRITE(IPR,2009) (CWD(I),I=I1,I2)
C WRITE(IPR,2010) (NO(I),I=I1,I2)
C IF(I2.EQ.NSAT) GO TO 12
C I1 = I2 + 1
C GO TO 13
12 CONTINUE
C WRITE(IPR,2014)
C WRITE(IPR,2012) ISAT
C WRITE(IPR,2015)
C
C HOUR = 0.00
C FSTDAY = DAY1
14 DAY1 = FSTDAY + HOUR/24.00
C
C NN = 0
C DO 11 I = 1, NSAT
C
C COMPUTE SATELLITE (EARTH FIXED) COORDINATES
C
C CALL SATVEC(I, DAY1, XS)
C CALL XYZPLH(XS(1), XS(2), XS(3), PLAT, PLON, HSAT)
C
C COMPUTE LAT AND LONG OF SATELLITE SUBPOINT
C
C SLAT(I) = DINT(PLAT/RHO)
C SLON(I) = DINT(PLON/RHO)

```

```

C
C
C COMPUTE SATELLITE AZIMUTH , ELEVATION ANGLE , SLANT RANGE AND
C ITS DERIVATIVE WITH RESPECT TO LAT AND LONG
C CALL DERIV (IPR,AE,BE,OLAT,OLONG,HT,XS,S,DSDP,DSDL,EL,AZ,IER)
C
C ELEV(I) = DINT(EL)
C AZIM(I) = DINT(AZ)
-----
C
C IDAY = DAY1
C TOD = HOUR*3600.D0
C CALL HHMMSS (TOD,IHR,IMIN,ISEC)
C IHR = MODULO(IHR,24)
C T=DFLOAT(IHR)+IMIN/60.D0
-----
C
C CHECK FOR MINIMUM ELEVATION ANGLE
C IF(EL .LT. ELMIN) GO TO 17
C NN = NN + 1
-----
C
C FORM DESIGN MATRIX
C
C WGTRG = 1.D0/SIGRG(MCODE)
C DA(NN,1) = DSDP * WGTRG
C DA(NN,2) = DSDL * WGTRG
C DA(NN,3) = 1.D0 * WGTRG
-----
C
C GO TO 11
C 17 ELEV(I) = 0
C AZIM(I) = 0
C EA = 0
C EB = 0
C PHI = 0
C EEA = 0.
-----
C
C 11 CONTINUE
C NPR = NN
C LRN = 0
C IF(NN .GT. 3) GO TO 18
C IF(NN .LT. 2) GO TO 16
C IF(LGRAN .EQ. 0) GO TO 18
-----
C
C IF LESS THAN 3 PSEUDO-RANGES AVAILABLE TRY COMBINED PERFORMANCE
C WITH LGRAN RANGES
C
C DO 19 L = 1,3
C CALL PLXYZ(XLAT(L),XLON(L),0.D0,0.D0,0.D0,0.D0,AE,BE,XX,YY,ZZ)
C XS(1) = XX
C XS(2) = YY
C XS(3) = ZZ
C CALL DERIV(IPR,AE,BE,OLAT,OLONG,HT,XS,S,DSDP,DSDL,EL,AZ,IER)
C LRN = LRN + 1
C NN = NPR + LRN
-----
C
C WGTRG = 1./SIGLRN(MLORN)
C DA(NN,1) = DSDP * WGTRG
C DA(NN,2) = DSDL * WGTRG
C DA(NN,3) = 1.D0 * WGTRG
-----
C 19 CONTINUE
C 18 CONTINUE
C CALL MATMPY(DA,DA,ATPA,3,NN,3,6,6,3,2)
C DO 30 II = 1,3
C 30 ATPA(II,II) = ATPA(II,II) + PX(II)
C CALL MINVD(ATPA,3,3,DETA,IW1,IW2)

```

```

C
C COMPUTE STANDARD ERROR ELLIPSE
C
CALL ELIPS(ATPA(1,1),ATPA(2,1),ATPA(2,2),EEA,EEB,1.D0,FI)
EA = DINT(EEA*6371.D3*RHO)
EB = DINT(EEB*6371.D3*RHO)
PHI = DINT(FI/RHO)
EEA = EEA * 6371.D3 * RHO
16 CONTINUE
WRITE(IPR,2013) IDAY,IHR,IMIN,(ELEV(I),AZIM(I),
# SLAT(I),SLON(I),I=1,NSAT),EA,EB,PHI,NPR,LRN
CALL PLOT(8,120,EEA,T)
HOUR = HOUR + 5./60.
IF(HOUR.LT.24.D0) GO TO 14
1000 FORMAT(I4,F8.0,4D16.12,4X,/,3E16.12,I4,F8.0)
1001 FORMAT(3F8.0,2F4.0,4I4)
2001 F0RMA T(/,5X,'SATELLITE NO.',11X,6I16)
2002 FORMAT(/,5X,'REF. TIME - TIME OF WEEK (SEC)',1X,6D16.8)
2003 FORMAT(/,5X,'SEMI - MAJOR AXIS (M)',6D16.8)
2004 FORMAT(/,5X,'MEAN ANOMALY @ TREF (RADIANS)',6D16.8)
2005 FORMAT(/,5X,'ECCENTRICITY',19X,6D16.8)
2006 FORMAT(/,5X,'ARG OF PERIGEE (RADIANS)',6X,6D16.8)
2007 FORMAT(/,5X,'INCLINATION (RADIANS)',9X,6D16.8)
2008 FORMAT(/,5X,'RIGHT ASCENSION (RADIANS)',5X,6D16.8)
2009 FORMAT(/,5X,'RATE OF RA (RADIANS/SEC)',6X,6D16.8)
2010 FORMAT(/,5X,'MEAN MOTION (RADIANS/SEC)',5X,6D16.8)
2011 FORMAT(/,5X,'JULIAN DATE (DDD HH MM SS)',4X,6(4X,4I3))
2012 FORMAT(11X,6(5X,'SAT # ',I2,4X),2X,'ERROR ELLIPSE',/)
2013 FORMAT(I5,2I3,6(I3,2I4,I5,1X),I6,2I4,2I3)
2014 FORMAT(//)
2015 FORMAT(2X,'DAY HH MM',6(' EL AZ LAT LONG '),3X,'AA',2X,'BB',2
# 'PHI',//)
2016 FORMAT(50X,'GPS PERFORMANCE PRE-ANALYSIS',//,40X,'LATITUDE =',
# F8.4,10X,'LONGITUDE =',F8.4,//,20X,'OPTIONS USED FOR THIS R
# //,40X,'CODE : ',A8,//,40X,'SIGMA PSEUDO-RANGE = ',F6.2,
#5X,'(M)',//,40X,'SIGMA LORAN-RANGE = 100/SQRT(',F4.1,') (M)'
STOP
END

```

```

FUNCTION MODULO(I,J)
MODULO = I - (I-1)/J*J
RETURN
END

```

```

SUBROUTINE HHMMSS (TJD,IH,IM,IS)
IMPLICIT REAL*8(A-H,O-Z)

```

```

C
IH = TJD / 36.D2
IM = ((TJD/36.D2) - IH)*60.
IS = TJD - IH*3600. - IM*60.
RETURN
END

```

```

SUBROUTINE ROTREF(NUM,NAXIS,ANGLE,ROT)
C*****
C*
C*   COMPUTE PRODUCT MATRIX OF SEQUENCE OF ROTATIONS AND REFLECTIONS *
C*
C*   INPUTS
C*     NUM = NUMBER OF ROTATIONS AND REFLECTIONS IN SEQUENCE
C*     NAXIS = SEQUENCE OF ROTATION AND REFLECTION AXES
C*             FOR ROTATIONS USE    1, 2, OR 3
C*             FOR REFLECTIONS USE  -1, -2, OR -3
C*     ANGLE = SEQUENCE OF ROTATION ANGLES IN RADIANs
C*             FOR REFLECTIONS THIS ANGLE IS IGNORED (ASSUMED ZERO)
C*
C*   OUTPUT
C*     ROT = 3X3 PRODUCT MATRIX
C*****
C     IMPLICIT REAL*8(A-H,O-Z)
C     DIMENSION ROT(3,3),R1(3,3),R2(3),ANGLE(NUM),NAXIS(NUM)
C     EPS = 1D-15
C
C     ...INITIALIZE (SET 'ROT' = IDENTITY MATRIX)
C
C     DO 10 I=1,3
C     DO 10 J=1,3
C     ROT(I,J)=0.
C     IF(I.EQ.J) ROT(I,J)=1.
10  CONTINUE
C
C     ...PROCESS SEQUENCE OF ROTATIONS AND REFLECTIONS ONE AT A TIME
C
C     DO 100 N=1,NUM
C
C     ...DEFINE 3 AXES FOR CURRENT ROTATION OR REFLECTION
C
C     N1=IABS(NAXIS(N))
C     N2=N1+1
C     IF(N2.GT.3) N2=N2-3
C     N3=N2+1
C     IF(N3.GT.3) N3=N3-3
C
C     ...DEFINE DIAGONAL ELEMENTS
C
C     R1(N1,N1) = 1.
C     IF(NAXIS(N).LT.0.) R1(N1,N1) = -1.
C     R1(N2,N2) = DCOS(ANGLE(N))
C     IF(NAXIS(N).LT.0.) R1(N2,N2) = 1.
C     R1(N3,N3) = R1(N2,N2)
C
C     ...DEFINE NONZERO OFF-DIAGONAL ELEMENTS
C
C     R1(N2,N3) = DSIN(ANGLE(N))
C     IF(NAXIS(N).LT.0.) R1(N2,N3) = 0.
C     R1(N3,N2) = -R1(N2,N3)
C
C     ...DEFINE ZERO OFF-DIAGONAL ELEMENTS
C
C     R1(N1,N2) = 0.
C     R1(N1,N3) = 0.
C     R1(N2,N1) = 0.
C     R1(N3,N1) = 0.
C
C     ...FORM PRODUCT (SET 'ROT' = 'R1' * 'ROT')
C
C     DO 100 J=1,3
C     DO 30 I=1,3
C     R2(I) = 0.
C     DO 30 K=1,3
30  R2(I) = R2(I) + R1(I,K)*ROT(K,J)
C     DO 100 I=1,3
C     ROT(I,J) = R2(I)
C     IF(DABS(ROT(I,J)).LT.EPS) ROT(I,J) = 0.
100 CONTINUE
C     RETURN
C     END

```

SUBROUTINE PLHXYZ(PHI,RLAM,H,X0,Y0,Z0,A,B,X,Y,Z)

THIS ROUTINE COMPUTES THE CARTESIAN COORDINATES X,Y,Z GIVEN THE ELLIPSOIDAL COORDINATES PHI,RLAM,H.

INPUT:

PHI-ELLIPSOIDAL LATITUDE IN RADIANS.
 RLAM-ELLIPSOIDAL LONGITUDE IN RADIANS.
 (POSITIVE EAST OF GREENWICH)
 H-ELLIPSOIDAL HEIGHT IN METRES.
 X0,Y0,Z0-TRANSLATION COMPONENTS FROM THE ORIGIN OF THE
 CARTESIAN COORDINATE SYTEM (X,Y,Z) TO THE CENTER
 OF THE REFERENCE ELLIPSOID. (IN METRES.)
 A,B-SEMI-MAJOR AND SEMI-MINOR AXES OF THE REFERENCE
 ELLIPSOID IN METRES.

OUTPUT:

X,Y,Z-CARTESIAN COORDINATES OF THE POINT IN METRES.

WRITTEN BY R.R.STEEVES
 JUNE,1977

IMPLICIT REAL*8(A-Z)
 E2=(A*A-B*B)/(A*A)
 SP=DSIN(PHI)
 CP=DCOS(PHI)
 N=A/DSQRT(1.00-E2*SP**2)
 X=X0+(N+H)*CP*DCOS(RLAM)
 Y=Y0+(N+H)*CP*DSIN(RLAM)
 Z=Z0+(N*(1.00-E2)+H)*SP
 RETURN
 END

SUBROUTINE XYZPLH (X,Y,Z,PHI,RLAM,H)

THIS ROUTINE COMPUTES THE ELLIPSOIDAL COORDINATES PHI,RLAM,H GIVEN THE CARTESIAN COORDINATES X,Y,Z.

INPUT:

X,Y,Z-CARTESIAN COORDINATES OF THE POINT IN METRES.
 X0,Y0,Z0-TRANSLATION COMPONENTS FROM THE ORIGIN OF THE
 CARTESIAN COORDINATE SYTEM (X,Y,Z) TO THE CENTER
 OF THE REFERENCE ELLIPSOID. (IN METRES.)
 A,B-SEMI-MAJOR AND SEMI-MINOR AXES OF THE REFERENCE
 ELLIPSOID IN METRES.

OUTPUT:

PHI-ELLIPSOIDAL LATITUDE IN RADIANS.
 RLAM-ELLIPSOIDAL LONGITUDE IN RADIANS.
 (POSITIVE EAST OF GREENWICH)
 H-ELLIPSOIDAL HEIGHT IN METRES.

WRITTEN BY R.R.STEEVES
 JUNE,1977

IMPLICIT REAL*8(A-Z)

NOTE ADOPTED ELLIPSOID OF REFERENCE 'NWL 9D'

DATA A, B, X0, Y0, Z0 /6378135.00, 6356750.5000, 3*000/

E2=(A*A-B*B)/(A*A)
 XP=X-X0
 YP=Y-Y0
 ZP=Z-Z0
 S=DSQRT(XP**2+YP**2)
 RLAM=DATAN2(YP,XP)
 ZPS=ZP/S
 H=DSQRT(XP**2+YP**2+ZP**2)-A
 PHI=DATAN(ZPS/(1.00-E2*A/(A+H)))
 1 N=A/DSQRT(1.00-E2*DSIN(PHI)**2)
 HP=H
 PHIP=PHI
 H=S/DCOS(PHI)-N
 PHI=DATAN(ZPS/(1.00-E2*N/(N+H)))
 IF(DABS(PHIP-PHI).GT.1.0-11.0R.DABS(HP-H).GT.1.0-5)GO TO 1
 RETURN
 END

```

SUBROUTINE DERIV(LU,AE,BE,XLAT,XLON,HGT,XS,
$           S,DSDP,DSDL,ELEV,AZ,IER)
DOUBLE PRECISION AE,ANG,BE,BOA,CL,CP,DATN2,DCOS,
$           DEPOK,DRDL,DRDP,DSDL,DSDP,DSIN,DSQRT,DX,
$           ELEV,PI,RM,RN,ROT,S,SEC,SL,SP,HGT,AZ,
$           XLAT,XLON,XR,XS,XT
DIMENSION   ANG(3),DRDL(3),DRDP(3),DX(3),NAXIS(3),
$           ROT(3,3),XR(3),XS(3), XT(3)
DATA       NAXIS /3,2,-2/,
$           PI /3.14159265359D0/
C
C PURPOSE   DERIV COMPUTES SLANT RANGE(S) TO SATELLITE, ITS
C           DERIVATIVES WITH RESPECT TO LAT (DSDP) AND LONG (DSDL),
C           AND ELEVATION ANGLE (ELEV)
C
C INPUT ARGUMENTS
C           LU = LISTING LU
C           AE = SEMI-MAJOR AXIS OF EARTH ELLIPSOID (M)
C           BE = SEMI-MINOR AXIS (M) OR RECIPROCAL FLATTENING
C           XLAT = RECEIVER LATITUDE (DEG)
C           XLON = RECEIVER LONGITUDE (DEG)
C           HGT = RECEIVER ELLIPSOID HEIGHT (M)
C           INDEX = DOPPLER INTERVAL NUMBER (SINCE LOCKON)
C           XS(3,33) = SATELLITE LOCAL TERRESTRIAL COORDS (M)
C
C OUTPUT ARGUMENTS
C           S = RECEIVER TO SATELLITE SLANT RANGE (M)
C           DSDP = DERIVATIVE OF S WITH RESPECT TO LATITUDE (M/DEG)
C           DSDL = DERIVATIVE OF S WITH RESPECT TO LONG (M/DEG)
C           ELEV = SATELLITE ELEVATION ABOVE HORIZON (DEG)
C           IER = 0 SUCCESSFUL RETURN
C
C EXTERNALS   DATN2,DCOS,DEPOK,DSIN,DSQRT,ROTRF
C
C           IER = 0
C COMPUTE RECEIVER LOCAL TERRESTRIAL COORDS XR
CP = DCOS(XLAT*PI/180.)
SP = DSIN(XLAT*PI/180.)
CL = DCOS(XLON*PI/180.)
SL = DSIN(XLON*PI/180.)
BOA = (BE / AE)**2
IF(BE .LT. 6D3) BOA = (1. - 1./BE)**2
RN = AE / DSQRT(CP**2 + BOA * SP**2)
RM = RN * BOA * (RN/AE)**2
XR(1) = (RN+HGT) * CP * CL
XR(2) = (RN+HGT) * CP * SL
XR(3) = (RN*BOA + HGT) * SP
C COMPUTE DERIVATIVES OF XR WITH RESPECT TO LAT AND LONG
DRDP(1) = -(RM+HGT) * SP * CL * PI / 180.
DRDP(2) = -(RM+HGT) * SP * SL * PI / 180.
DRDP(3) = (RM+HGT) * CP * PI / 180.
DRDL(1) = -XR(2) * PI / 180.
DRDL(2) = XR(1) * PI / 180.
DRDL(3) = 0.
C WRITE(LU,1001) XR,DRDP,DRDL
C COMPUTE SLANT RANGE AND ITS DERIVATIVES
DO 10 I = 1,3
10 DX(I) = XS(I) - XR(I)
S = DSQRT(DX(1)**2 + DX(2)**2 + DX(3)**2)
DSDP = -(DX(1)*DRDP(1) + DX(2)*DRDP(2) + DX(3)*DRDP(3)) / S
DSDL = -(DX(1)*DRDL(1) + DX(2)*DRDL(2) + DX(3)*DRDL(3)) / S
C COMPUTE ELEVATION ANGLE
ANG(1) = (XLON - 180.)*PI/180.
ANG(2) = (XLAT - 90.)*PI/180.
ANG(3) = 0.D0
CALL ROTREF(3,NAXIS,ANG,ROT)
DO 20 I = 1,3
XT(I) = 0.
DO 20 J = 1,3
20 XT(I) = XT(I) + ROT(I,J) * DX(J)
ELEV = DATAN2(XT(3),DSQRT(XT(1)**2 + XT(2)**2)) * 180. / PI
AZ = DATAN2(XT(2),XT(1)) * 180. / PI
C WRITE(LU,1002) S,DSDP,DSDL,ELEV,AZ
RETURN
1001 FORMAT(' DERIV1',20X,3F14.2,2(/27X,3F14.2))
1002 FORMAT(' DERIV2',20X,3F14.2,2F6.1)
END

```

SUBROUTINE SATVEC(I, DAY1, XS)

SATVEC COMPUTES SATELLITE (EARTH FIXED) COORDINATES FROM
ORBITAL KEPLERIAN PARAMETERS TRANSMITTED BY THE NAVIGATION MESSAGE

IMPLICIT REAL*8(A-H, D-Z)
REAL *8 MO, NO, INC, MK
DIMENSION M3(6), N3(6), A(6), E(6), W(6), INC(6),
CW(6), CWD(6), EPOCH(6), TOE(6), ISAT(6), XS(3)

COMMON /ALMNAC/ A, MO, NO, E, W, INC, CW, CWD,
TOE, EPOCH, ISAT
WE = 7.292115147D-5

TIME FROM ALMANAC REFERENCE EPOCH

TK = (DAY1 - EPOCH(I))*864.D2

MEAN ANOMALY (RAD)

MK = MO(I) + NO(I)*TK

SOLVE KEPLER'S EQUATION FOR THE ECCENTRIC ANOMALY

EK0 = MK + E(I)*DSIN(MK) + (E(I)**2/2.)*DSIN(2.*MK)
50 FTM = EK0 - E(I)*DSIN(EK0)
DFTM = FTM - MK
EK0 = EK0 - DFTM/(1. - E(I)*DCOS(EK0))
IF(DABS(DFTM) .GT. 1.D-12) GO TO 50
EK = EK0
15 CONTINUE

TRUE ANOMALY (RAD)

ECOSEK = 1.D0 - E(I)*DCOS(EK)
COSVK = (DCOS(EK) - E(I)) / ECOSEK
SINVK = DSQRT(1.D0 - E(I)**2)*DSIN(EK) / ECOSEK

VK = DATAN2(SINVK, COSVK)

ARGUMENT OF LATITUDE

FK = VK + W(I)

COMPUTE SECOND HARMONIC PERTURBATIONS IN

ARGUMENT OF LATITUDE
SATELLITE RADIUS
INCLINATION
(CORRECTIONS NOT IMPLEMENTED YET)

UK = FK
RK = A(I) * (1.D0 - E(I)*DCOS(EK))

POSITION IN THE ORBITAL PLANE

XPK = RK * DCOS(UK)
YPK = RK * DSIN(UK)

CORRECTED LATITUDE OF THE ASCENDING NODE

CWK = CW(I) + (CWD(I) - WE)*TK - WE*TOE(I)

EARTH FIXED COORDINATES

XK = XPK*DCOS(CWK) - YPK*DCOS(INC(I))*DSIN(CWK)
YK = XPK*DSIN(CWK) + YPK*DCOS(INC(I))*DCOS(CWK)
ZK = YPK*DSIN(INC(I))

XS(1) = XK
XS(2) = YK
XS(3) = ZK
RETURN
END

SUBROUTINE MATMPY(M1,M2,M3,L,M,N,JL,JM,JN,ICODE)

```

C
C NAME          MATMPY
C
C PURPOSE      TO COMPUTE THE PRODUCT OF TWO MATRICES IN ANY
C              ALLOWABLE TRANSPOSE COMBINATION AS FOLLOWS:
C
C              OPTION ICODE          PRODUCT M3
C              1                      M1*M2
C              2                      (M1)T*M2
C              3                      M1*(M2)T
C              4                      (M1)T*(M2)T
C
C              (L,M),(M,N),(L,N) ARE THE DIMENSIONS OF THE
C              PRE-, POST- AND PRODUCT-MATRICES
C              RESPECTIVELY
C              JL,JM,JN ARE CORRESPONDING DECLARED ROW
C              DIMENSIONS AT THE CALLINE PROGRAM
C
C REAL *8 M1,M2,M3
C DIMENSION M1(JL,1) , M2(JM,1) , M3(JN,1)
C
C DO 11 I = 1,L
C   DO 11 J = 1,N
C     M3(I,J) = 0.
C     DO 11 K = 1,M
C       GO TO(1,2,3,4),ICODE
C     1  CONTINUE
C     M3 = M1 * M2
C     M3(I,J) = M3(I,J) + M1(I,K)*M2(K,J)
C     GO TO 11
C     2  CONTINUE
C     M3 = M1 TRANSPOSE * M2
C     M3(I,J) = M3(I,J) + M1(K,I)*M2(K,J)
C     GO TO 11
C     3  CONTINUE
C     M3 = M1 * M2 TRANSPOSE
C     M3(I,J) = M3(I,J) + M1(I,K)*M2(J,K)
C     GO TO 11
C     4  CONTINUE
C     M3 = M1 TRANSPOSE * M2 TRANSPOSE
C     M3(I,J) = M3(I,J) + M1(K,I)*M2(J,K)
C 11 CONTINUE
C   RETURN
C   END
C
C SUBROUTINE ELIPS(QXX,QXY,QYY,A,B,C,PHI)
C *****
C* ELIPS COMPUTES THE SEMI-MAJOR AND SEMI-MINOR AXES AND THE ORIENTATIO
C* (AZIMUTH OF THE MAJOR AXIS) OF THE ERROR ELLIPSE SPECIFIED BY QXX, Q
C* QXY AND THE FACTOR C.
C*
C* INPUT:
C* QXX,QXY,QYY- ELEMENTS OF THE 2 BY 2 COVARIANCE MATRIX OF THE VARI
C* FOR WHICH AN ERROR ELLIPSE IS REQUIRED
C* C-- FACTOR FOR THE ELLIPSE IN RAISING IT TO A SPECIFIC
C* PROBABILITY LEVEL (COMPUTED IN ERREL)
C*
C* OUTPUT:
C* A,B- SEMI-MAJOR AND SEMI-MINOR AXES OF THE ELLIPSE
C* PHI- AZIMUTH OF THE MAJOR AXIS (IN RADIANS)
C*
C*
C* WRITTEN BY:
C* R.R. STEEVES, APRIL, 1976
C*
C *****
C IMPLICIT REAL*8(A-H,O-Z)
C P1=(QXX+QYY)/2.D0
C P2=DSQRT(((QXX-QYY)**2/4.0D0+QXY**2)
C A=DSQRT(P1+P2)*C
C B=DSQRT(P1-P2)*C
C PI=3.141592653589793D0
C IF(QXX.LT.1.D0-20.AND.QYY.LT.1.D0-20)PHI=0.D0
C IF(QXX.LT.1.D0-20.AND.QYY.LT.1.D0-20)GOTO1
C PHI=-0.5D0*DATAN2(-2.D0*QXY,QYY-QXX)
C IF(PHI.LT.0.D0)PHI=PHI+2.D0*PI
C 1 RETURN
C END

```



```

SUBROUTINE PLINIT(LU,LPLOT)
C
C   INITIALIZE + PLOT HORIZONTAL AXIS
C
DOUBLE PRECISION XMIN,XMAX
DIMENSION IPLOT(120)
COMMON /PLOTS/ XMIN,XMAX
DATA IAX/1H+/, IBL/1H / , IST/1H*/
DO 1 I=1,LPLOT
  IPLOT(I)=IST
1 CONTINUE
C
C   PLOT AXIS
C
WRITE(LU,1000)(IPLOT(I),I=1,LPLOT)
1000 FORMAT(1H1.8X,120A1)
DO 2 I=1,LPLOT
  IF(I/20*20.EQ.I) GO TO 2
  IPLOT(I)=IBL
2 CONTINUE
WRITE(LU,1001)(IPLOT(I),I=1,LPLOT)
1001 FORMAT(' ',7X,'+',120A1)
WRITE(LU,1002)
1002 FORMAT(' ')
RETURN
END

```

```

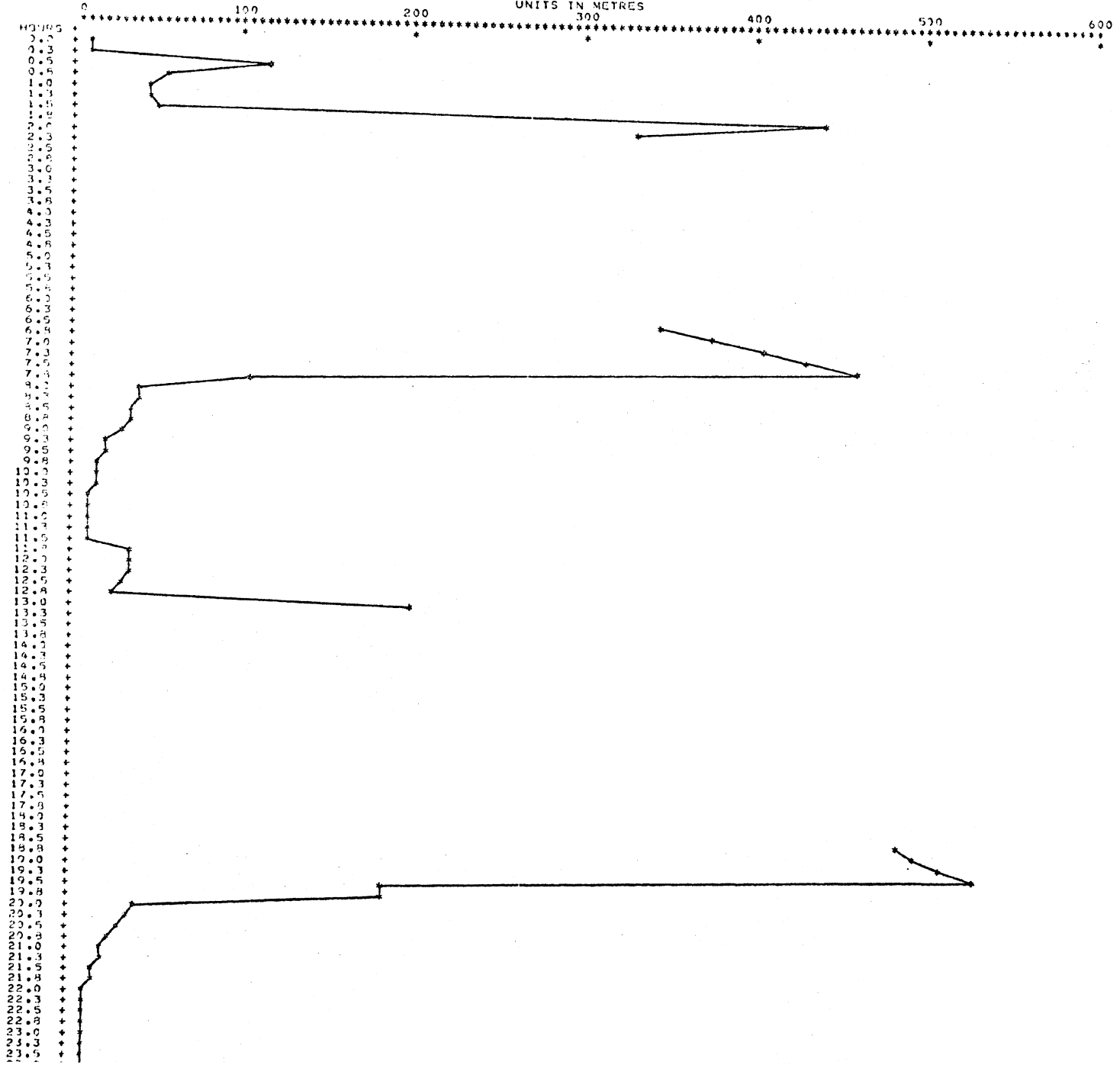
SUBROUTINE PLOT(LU,LPLOT,X,T)
DOUBLE PRECISION XMIN,XMAX,X,T
DIMENSION IPLOT(120)
COMMON /PLOTS/ XMIN,XMAX
DATA IBL/1H / , IAX/1H+/, IST/1H*/
DO 1 I=1,LPLOT
  IPLOT(I)=IBL
1 CONTINUE
IF(X.LE.XMIN) GO TO 2
K=(((X-XMIN)/(XMAX-XMIN))*LPLOT+0.5)
IF(K.LT.1.OR.K.GT.LPLOT) GO TO 2
IPLOT(K)=IST
2 WRITE(LU,1001)T,(IPLOT(I),I=1,LPLOT)
1001 FORMAT(' ',F5.1,2X,'+',120A1)
WRITE(LU,1002)
1002 FORMAT(' ',7X,'+')
RETURN
END

```

1. BAFFIN BAY P-CODE	NO LORAN
2. BAFFIN BAY C/A CODE	NO LORAN
3. BAFFIN BAY C/A CODE	WITH LORAN
4. DAVIS STRAIT P-CODE	NO LORAN
5. DAVIS STRAIT C/A CODE	NO LORAN
6. DAVIS STRAIT C/A CODE	WITH LORAN
7. LABRADOR P-CODE	NO LORAN
8. LABRADOR C/A CODE	NO LORAN
9. LABRADOR C/A CODE	WITH LORAN
10. AZORES P-CODE	NO LORAN
11. GRAND BANKS P-CODE	NO LORAN
12. HUDSON BAY P-CODE	NO LORAN
13. BEAUFORT SEA P-CODE	NO LORAN
14. ARCTIC OCEAN P-CODE	NO LORAN
15. BRITISH COLUMBIA P-CODE	NO LORAN
16. 20°N 25°W P-CODE	NO LORAN
17. 40°N 25°W P-CODE	NO LORAN
18. 60°N 25°W P-CODE	NO LORAN
19. 20°N 70°W P-CODE	NO LORAN
20. 40°N 70°W P-CODE	NO LORAN
21. 60°N 70°W P-CODE	NO LORAN

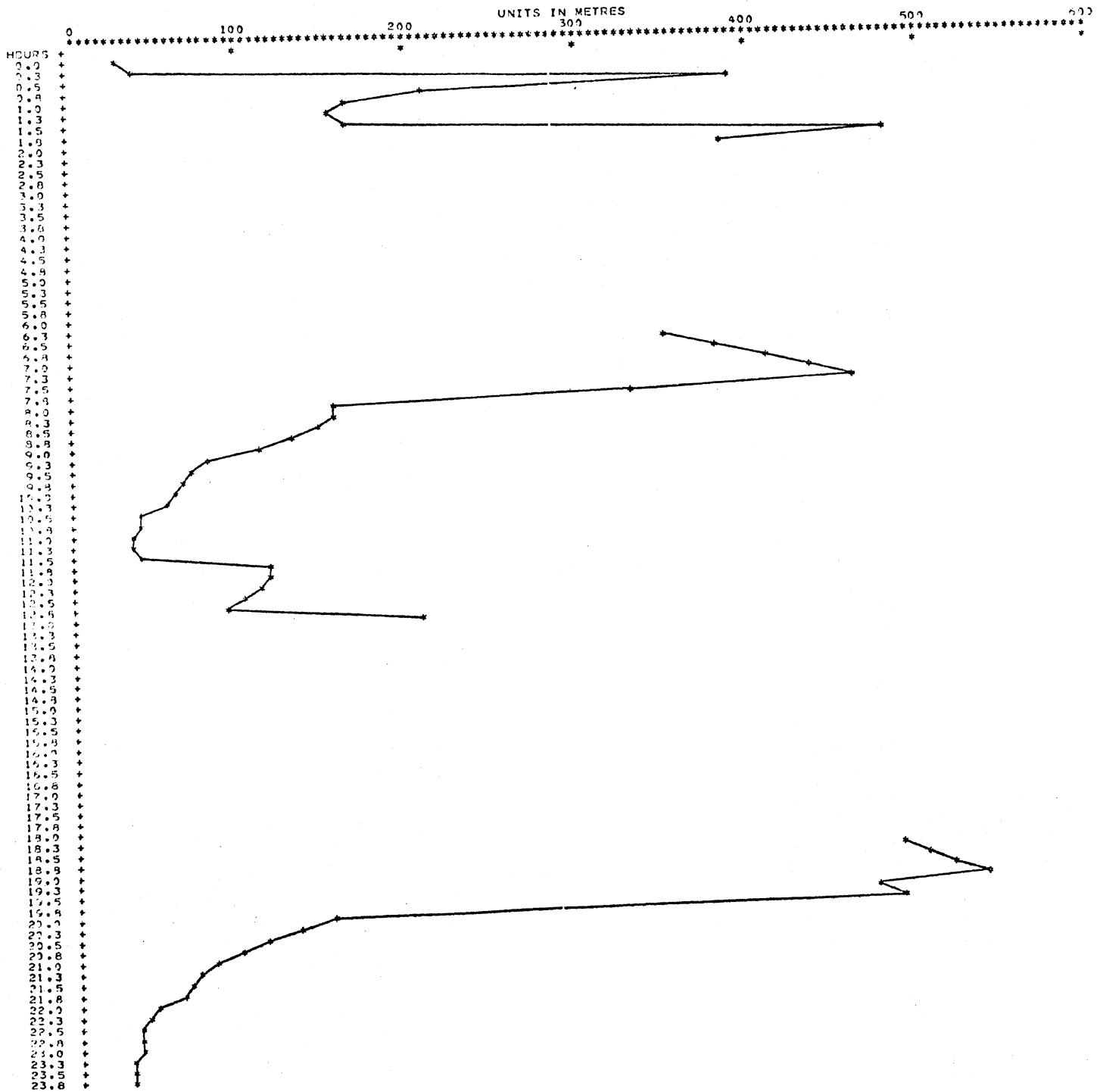
- NOTES: 1. In all plots the length of the semi-major axis standard error ellipse is plotted against time for the 24 hour period starting at 0000 UT 1 Oct. 1980.
2. All plots are for the present GPS configuration of six satellites.

NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

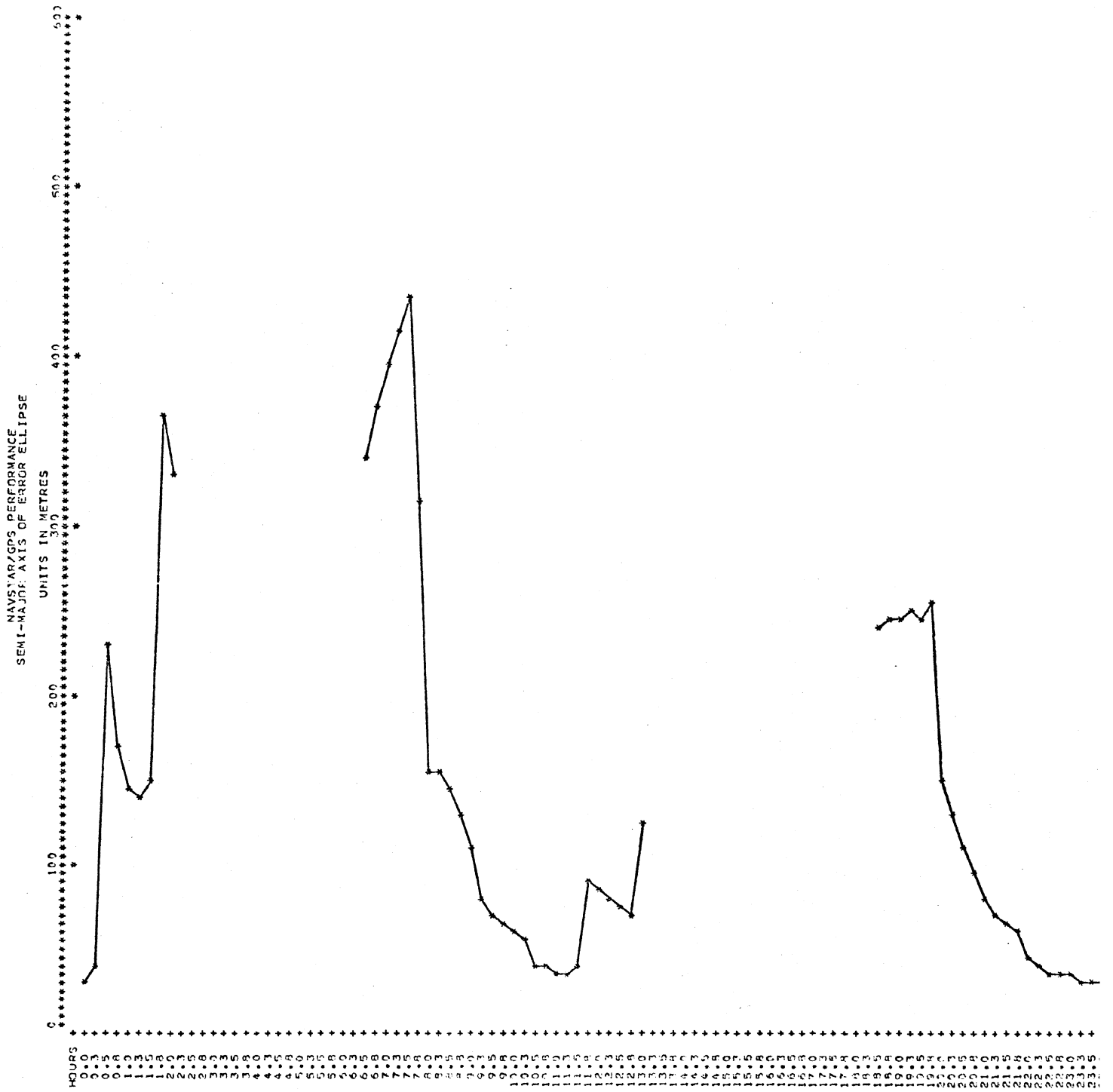


Baffin Bay (70°N, 68°W) using P-code.

NAVSTAR/CPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

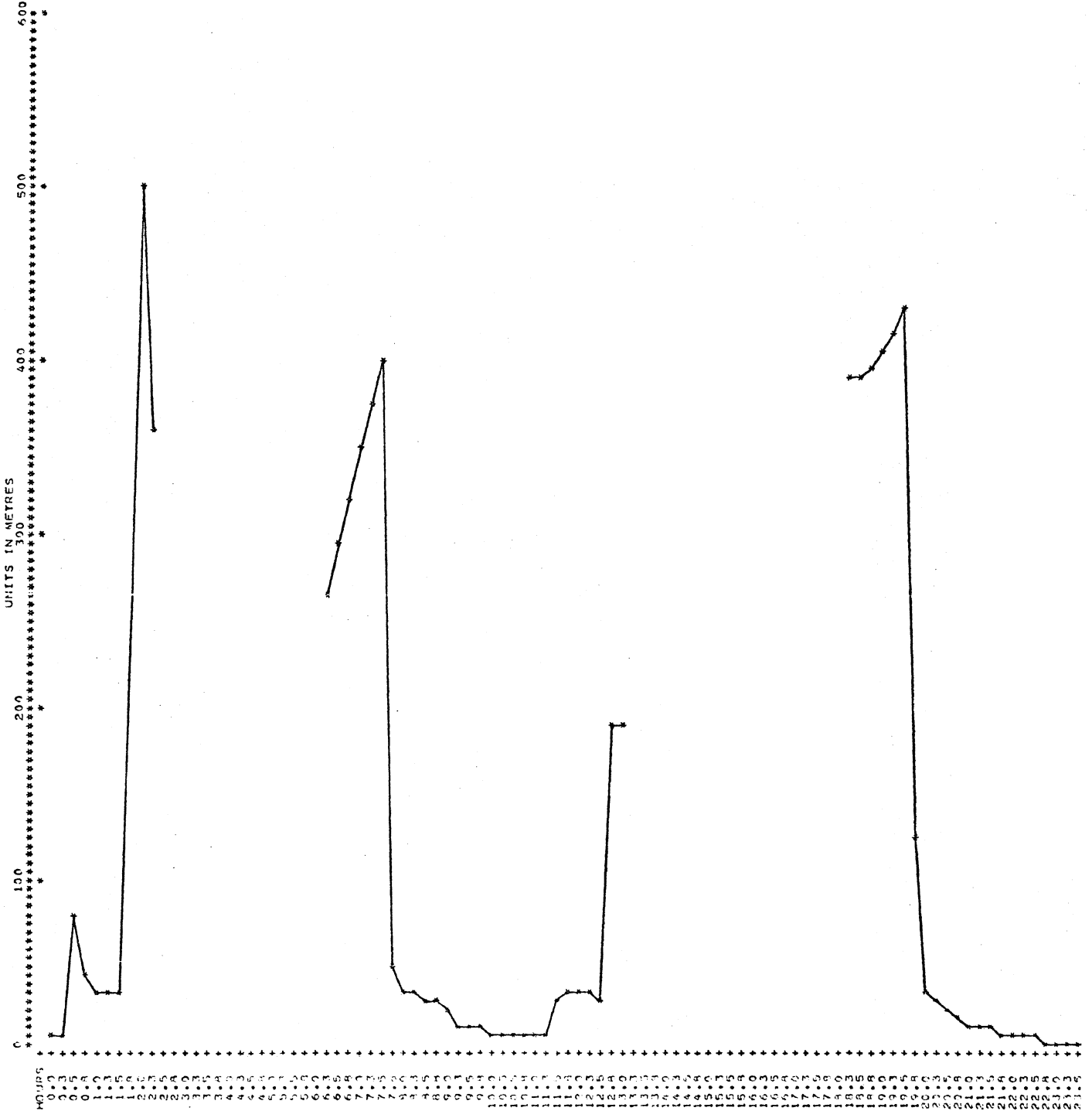


Baffin Bay (70°N, 68°W) using C/A-code

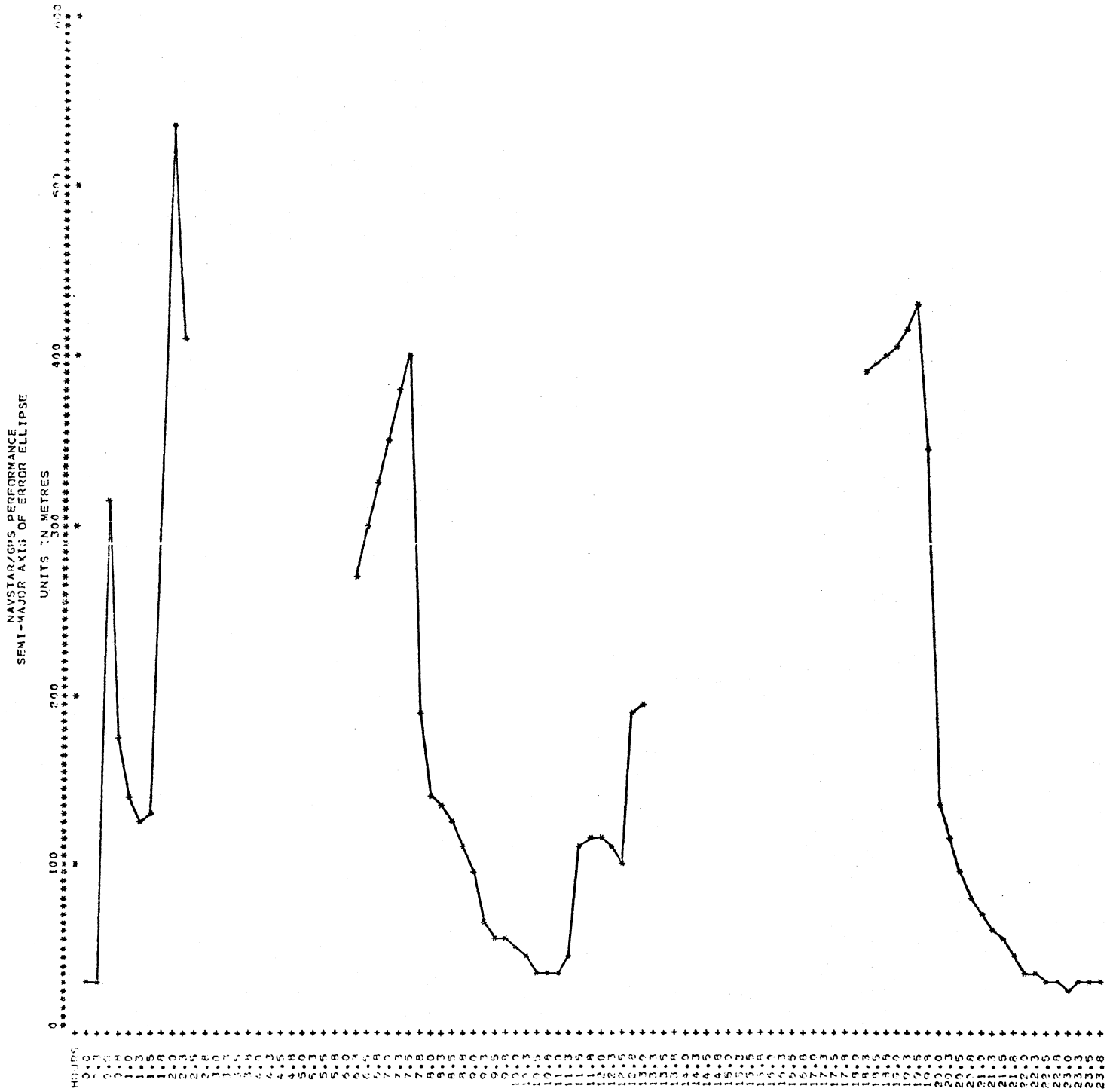


Baffin Bay (70°N, 68°W) using C/A-code in combination with LORAN-C

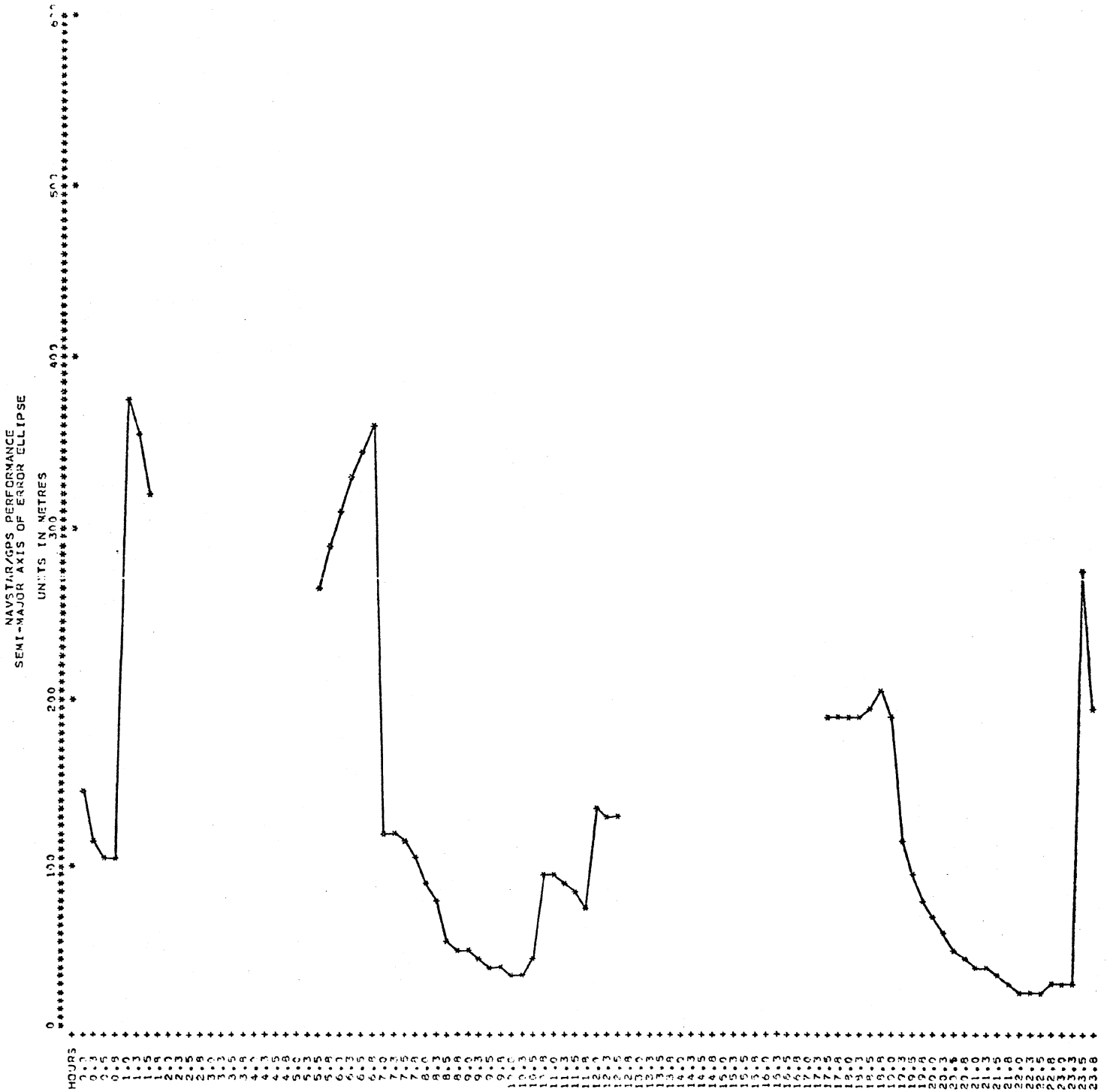
NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE



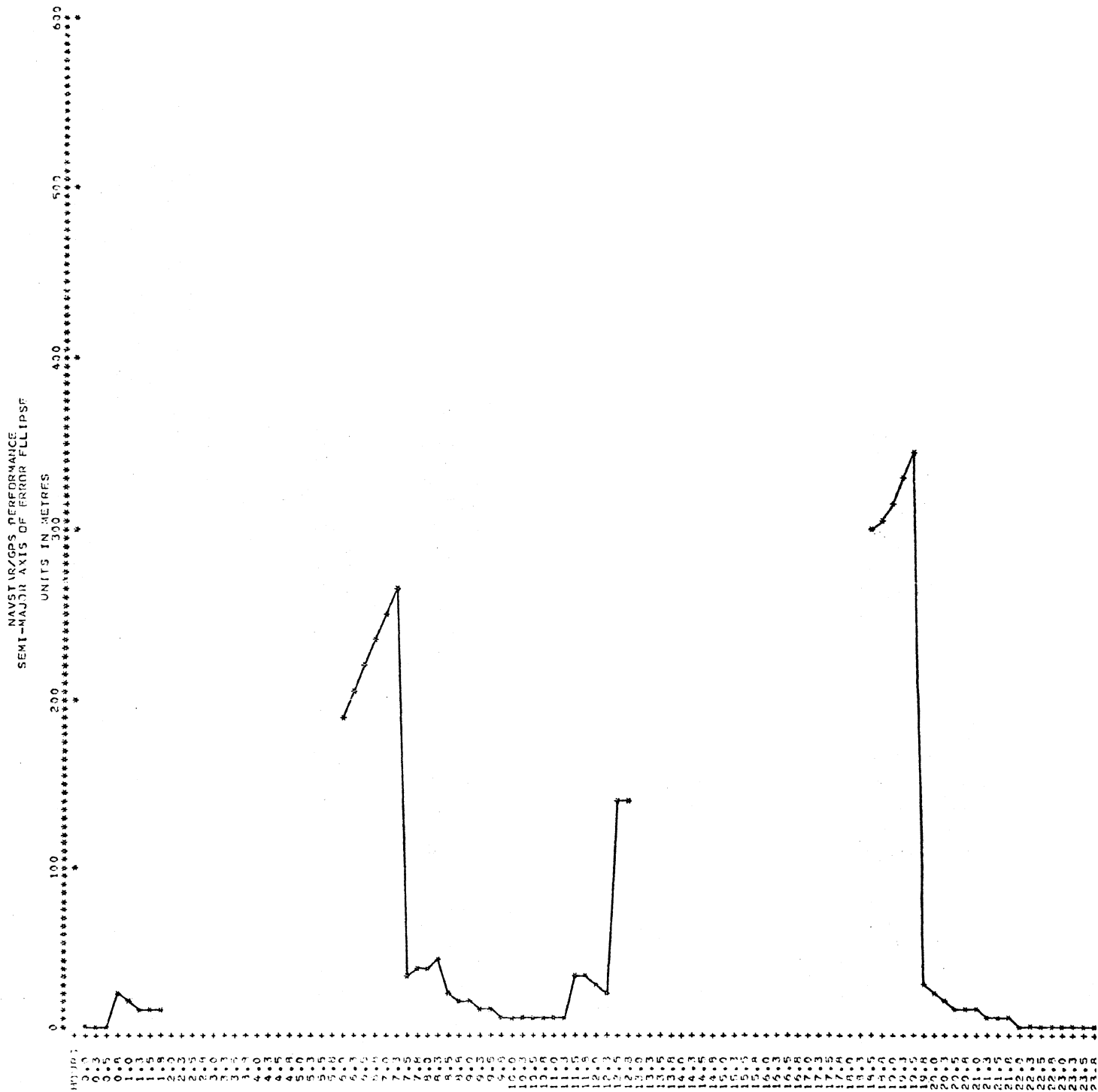
Davis Strait (65°N, 60°W) using P-code.



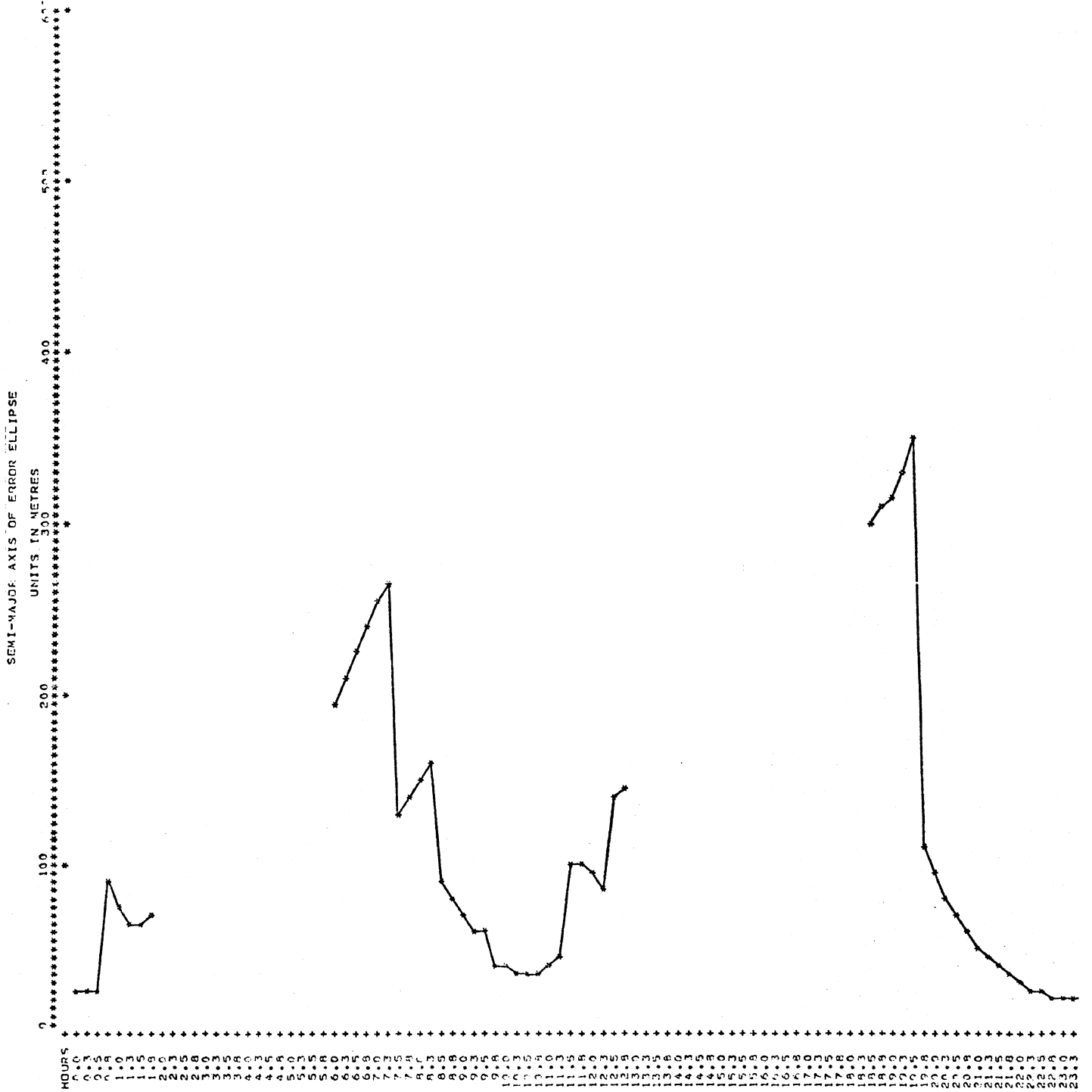
Davis Strait (65°N, 60°W) using C/A-code



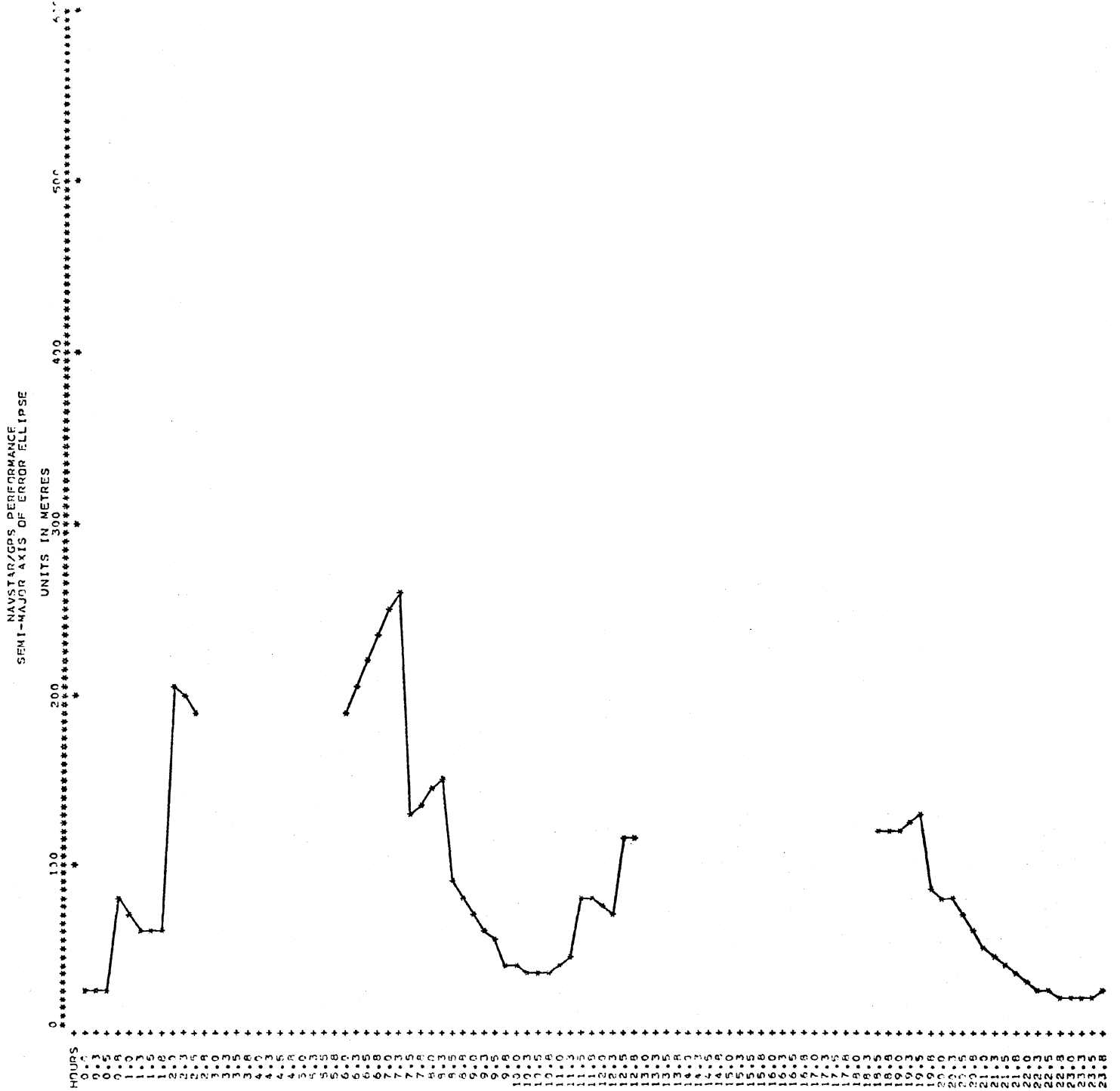
Davis Strait (65°N, 60°W) using C/A-code
in combination with LORAN-C



Labrador (55°N, 65°W) using P-code

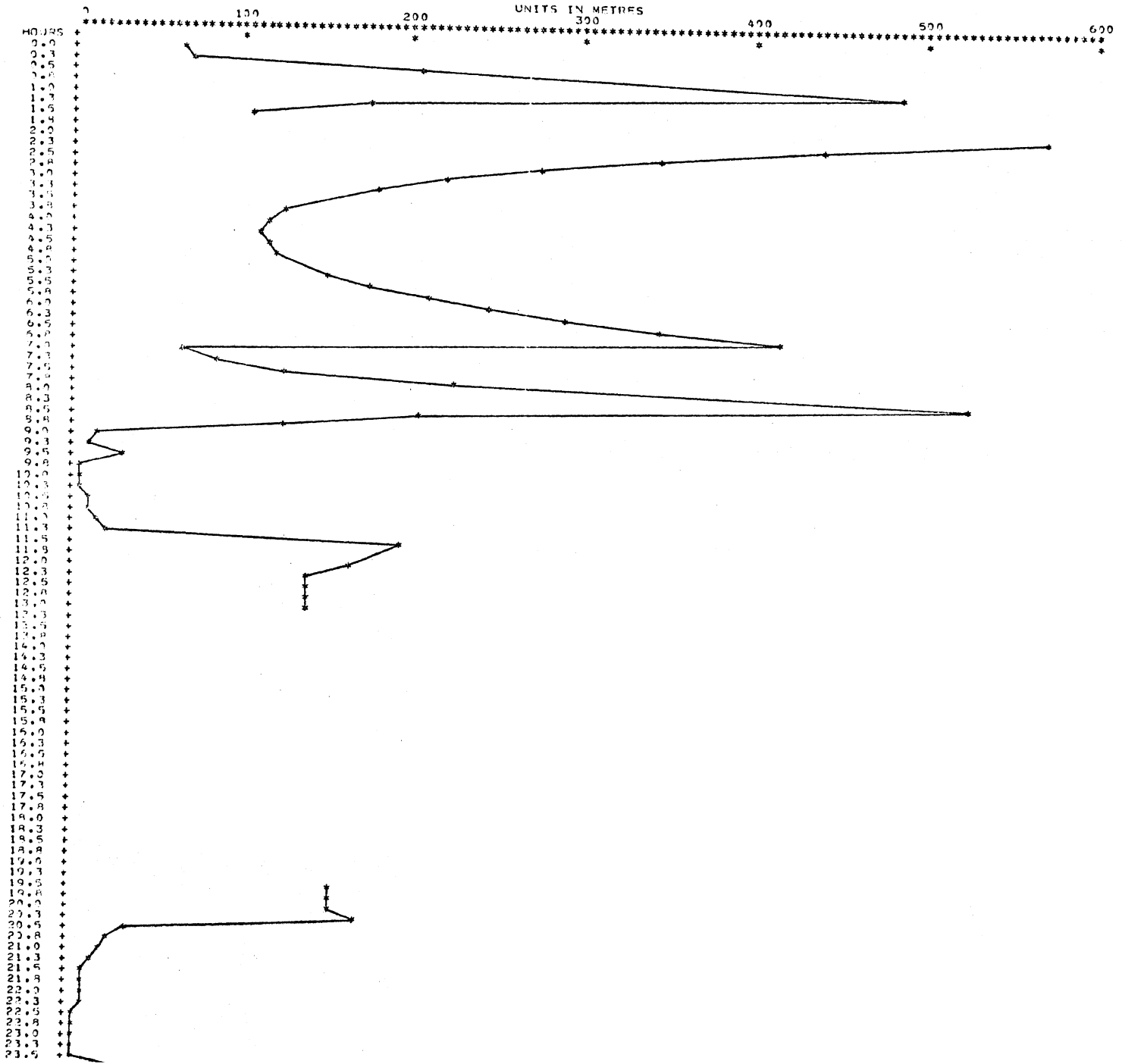


Labrador (55°N, 65°W) using C/A code



Labrador (55°N, 65°W) using C/A-code in combination with LORAN-C

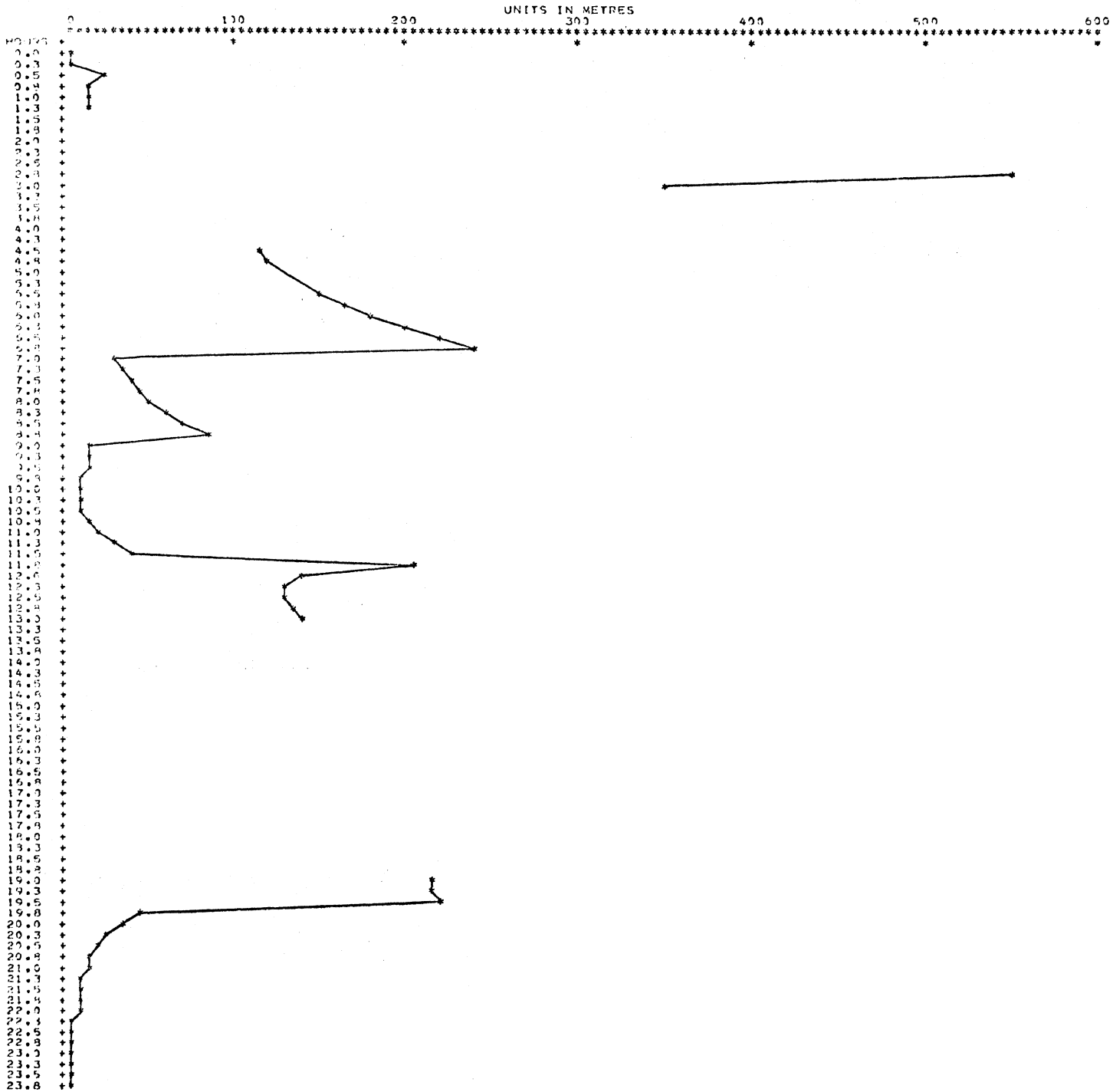
NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

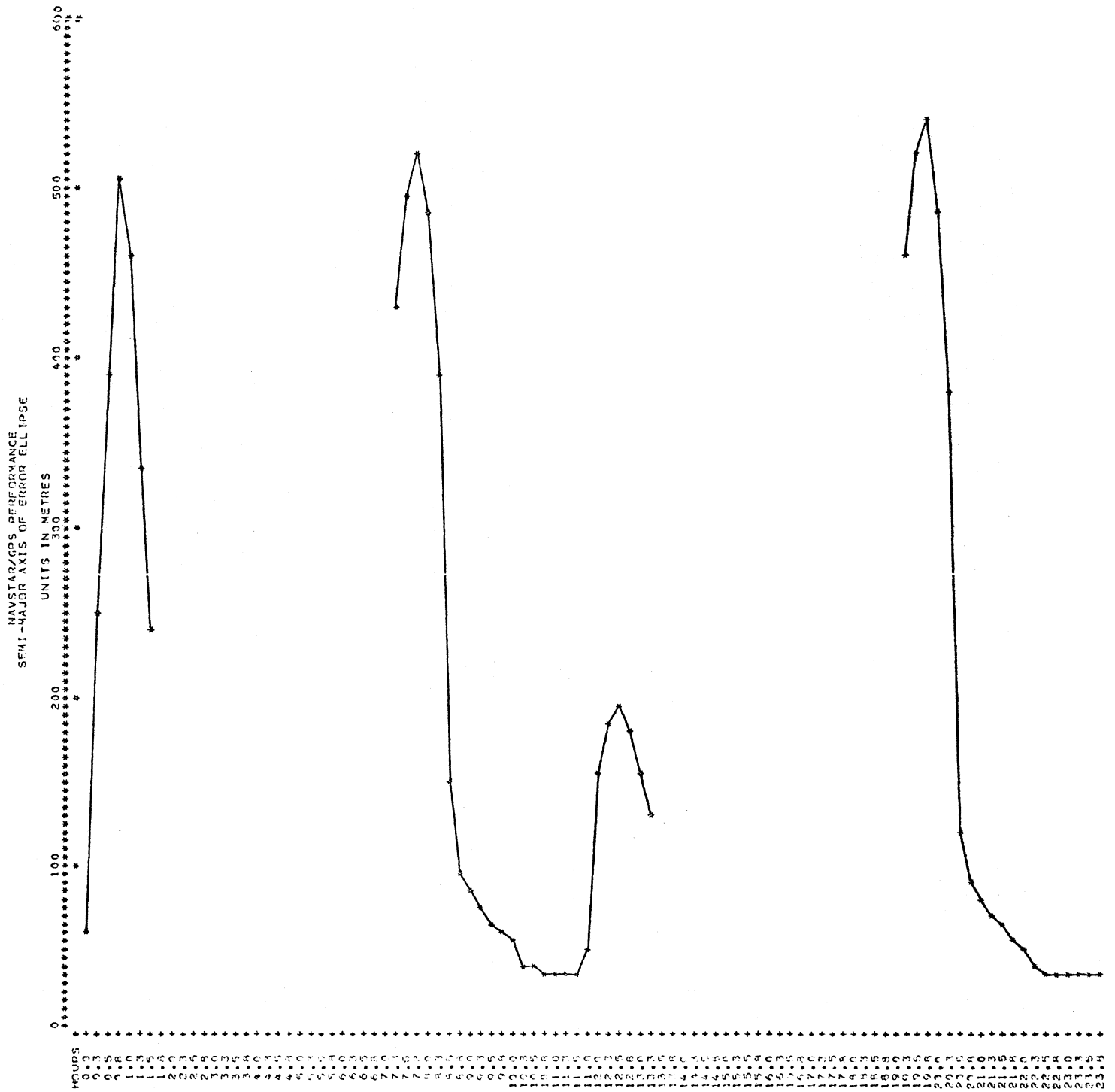


Azores (40°N, 30°W) using P-Code

NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

Grand Banks (45°N, 50°W) using P-Code

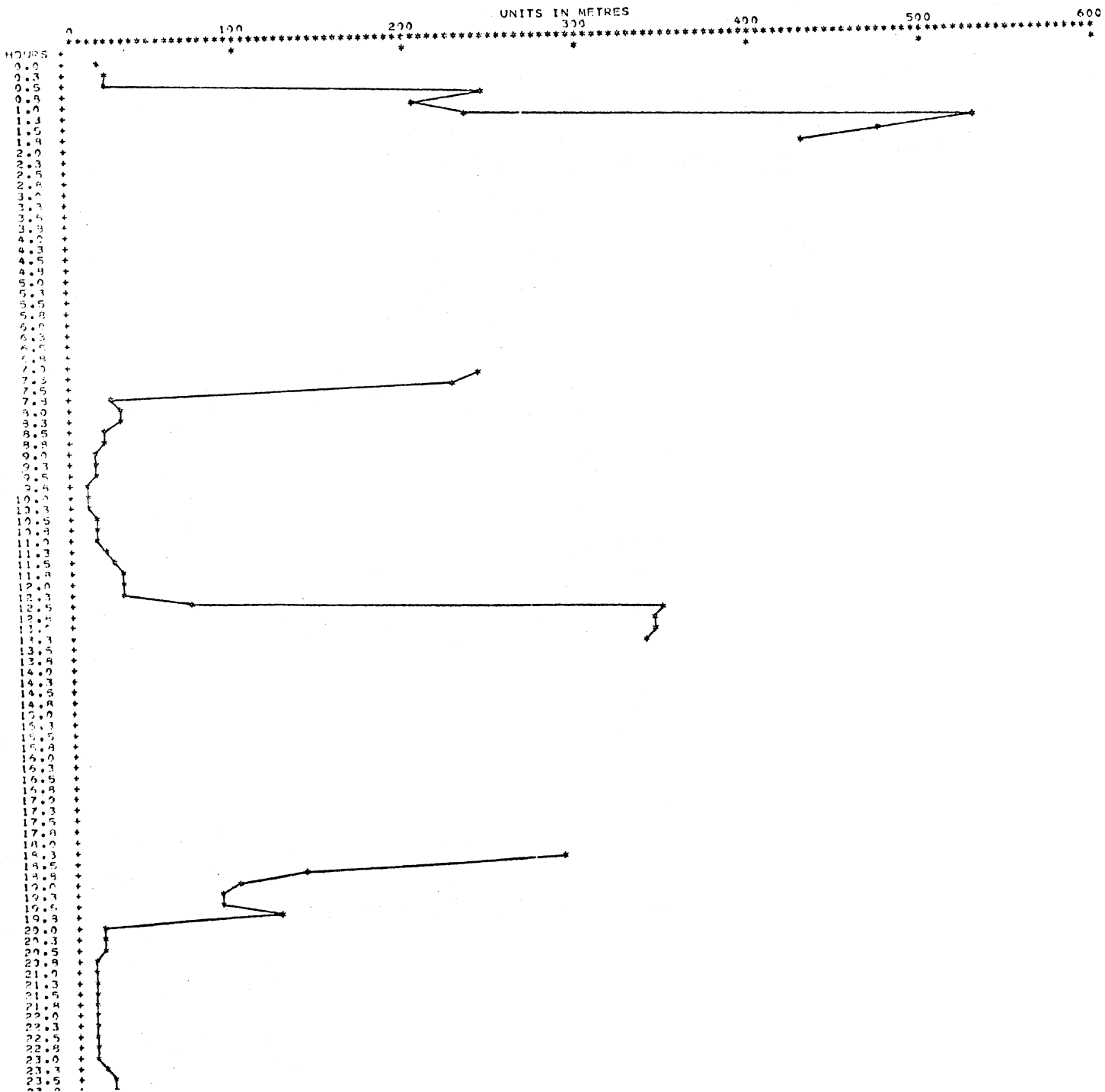




Hudson Bay (85°N, 60°W) using P-Code.

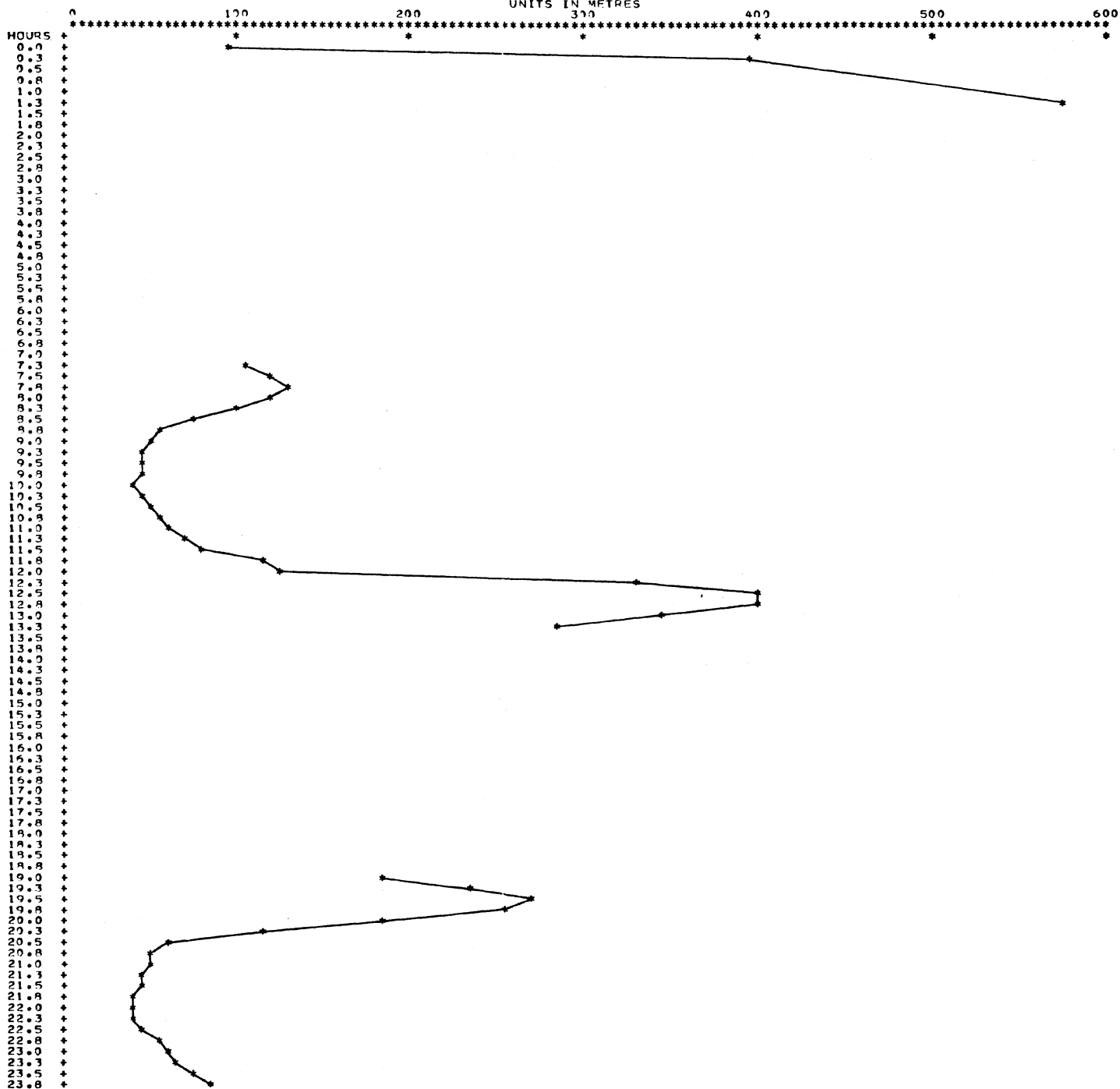
NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

UNITS IN METRES



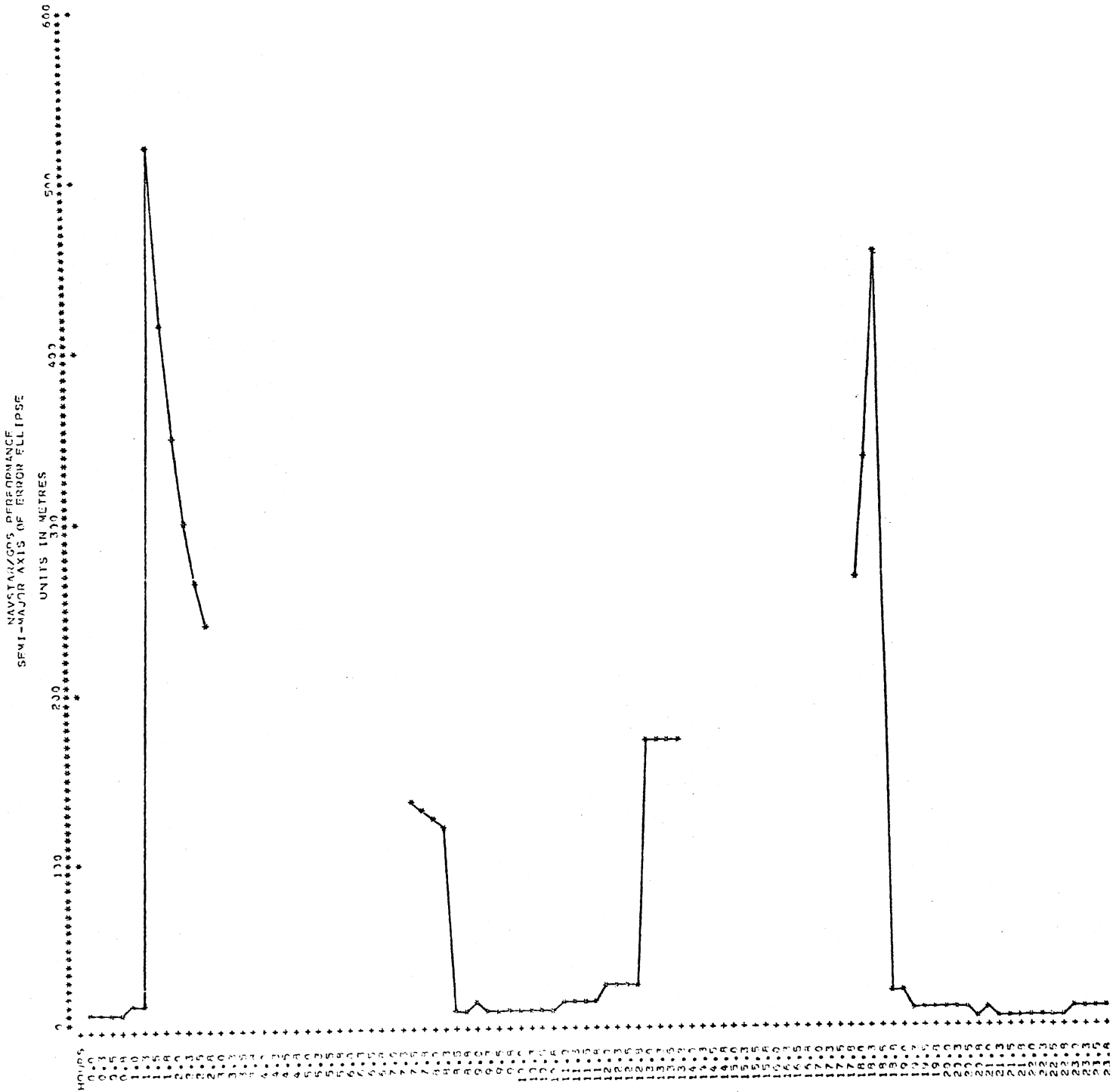
Beauford Sea (70°N, 130°W) using P-code

NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE



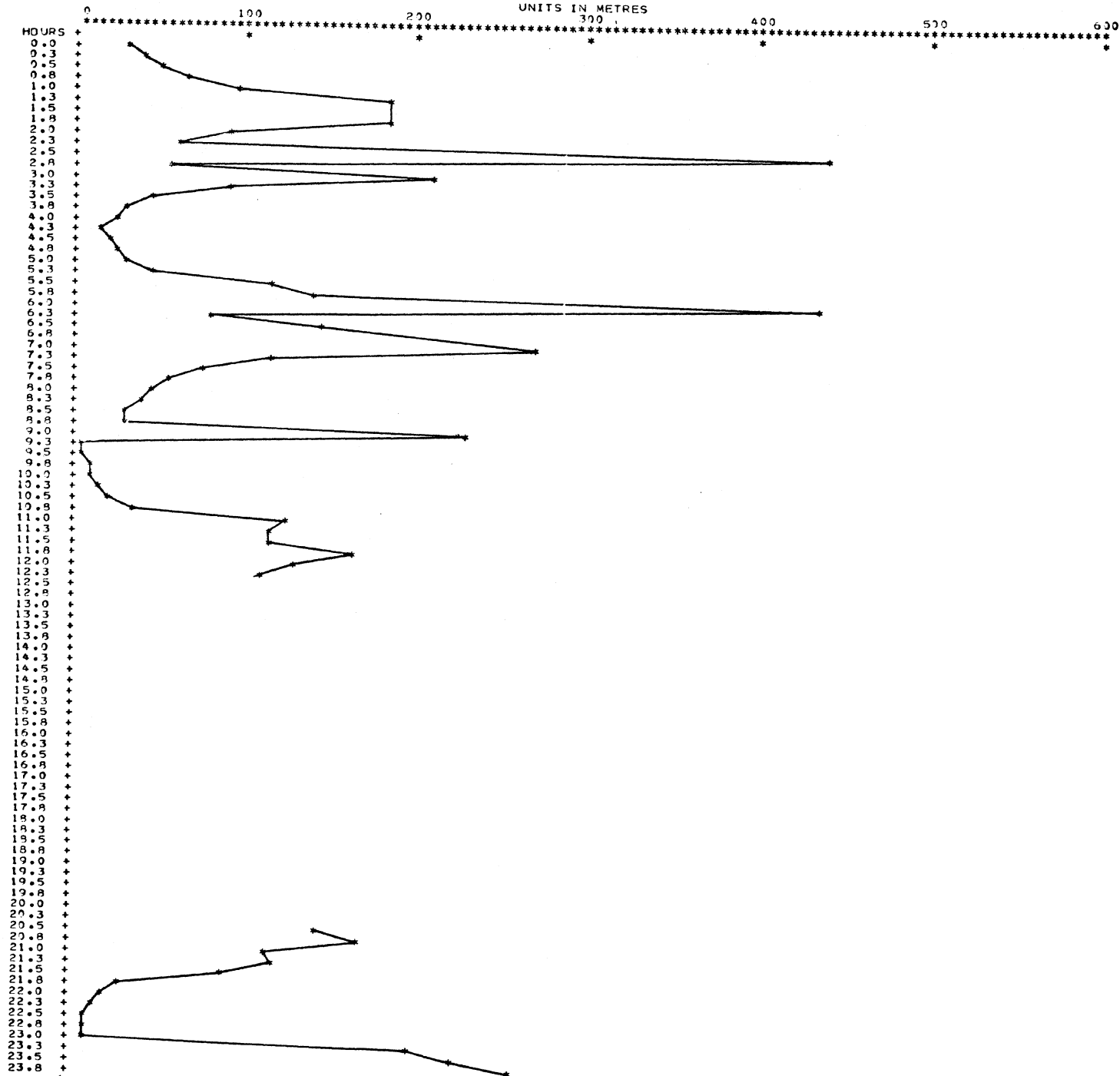
Arctic Ocean (85°N, 130°W) using P-code

15



British Columbia (50°N, 130°W) using P-Code

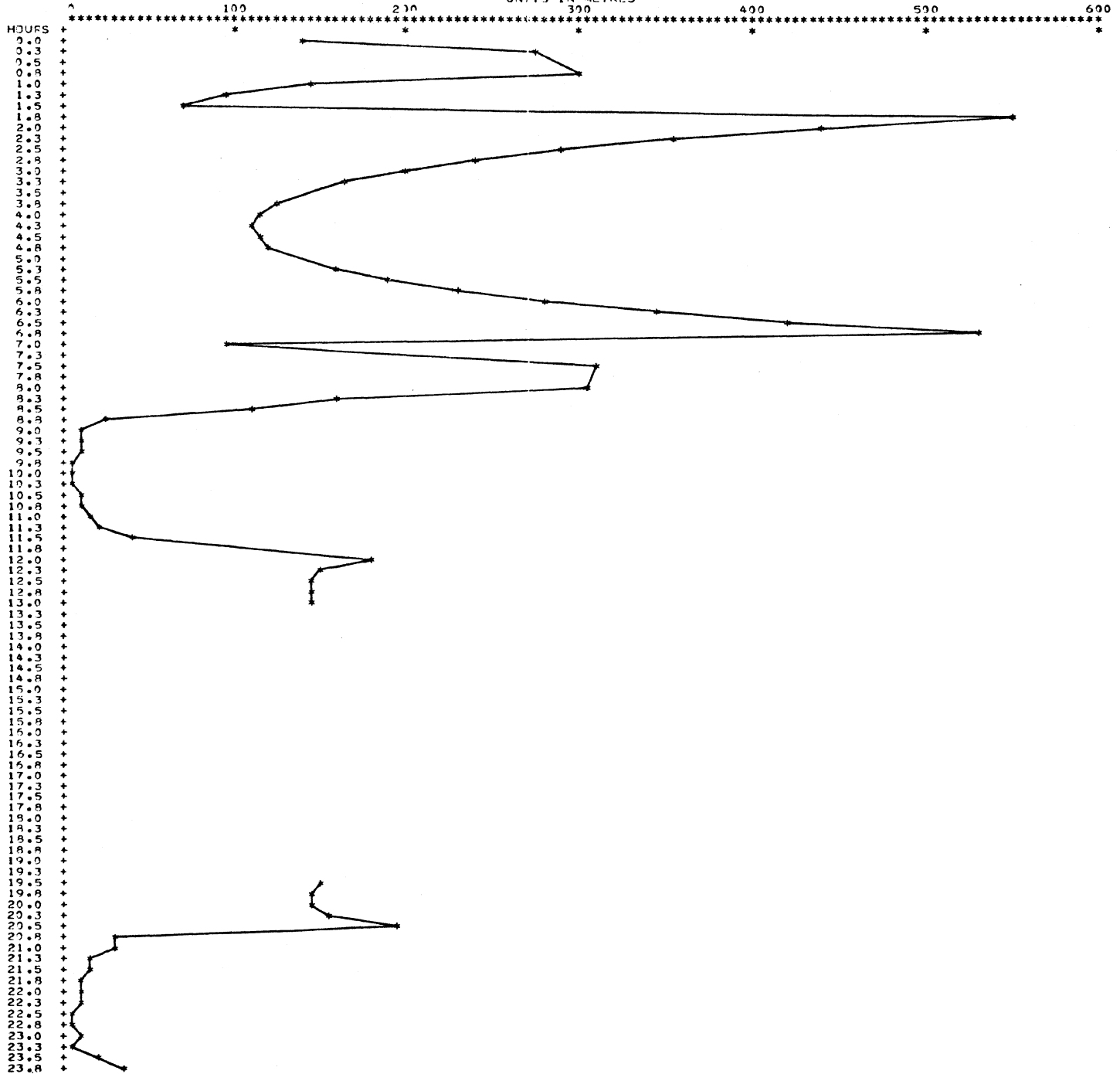
NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE



Latitude 20° N , Longitude 25° W using P-code

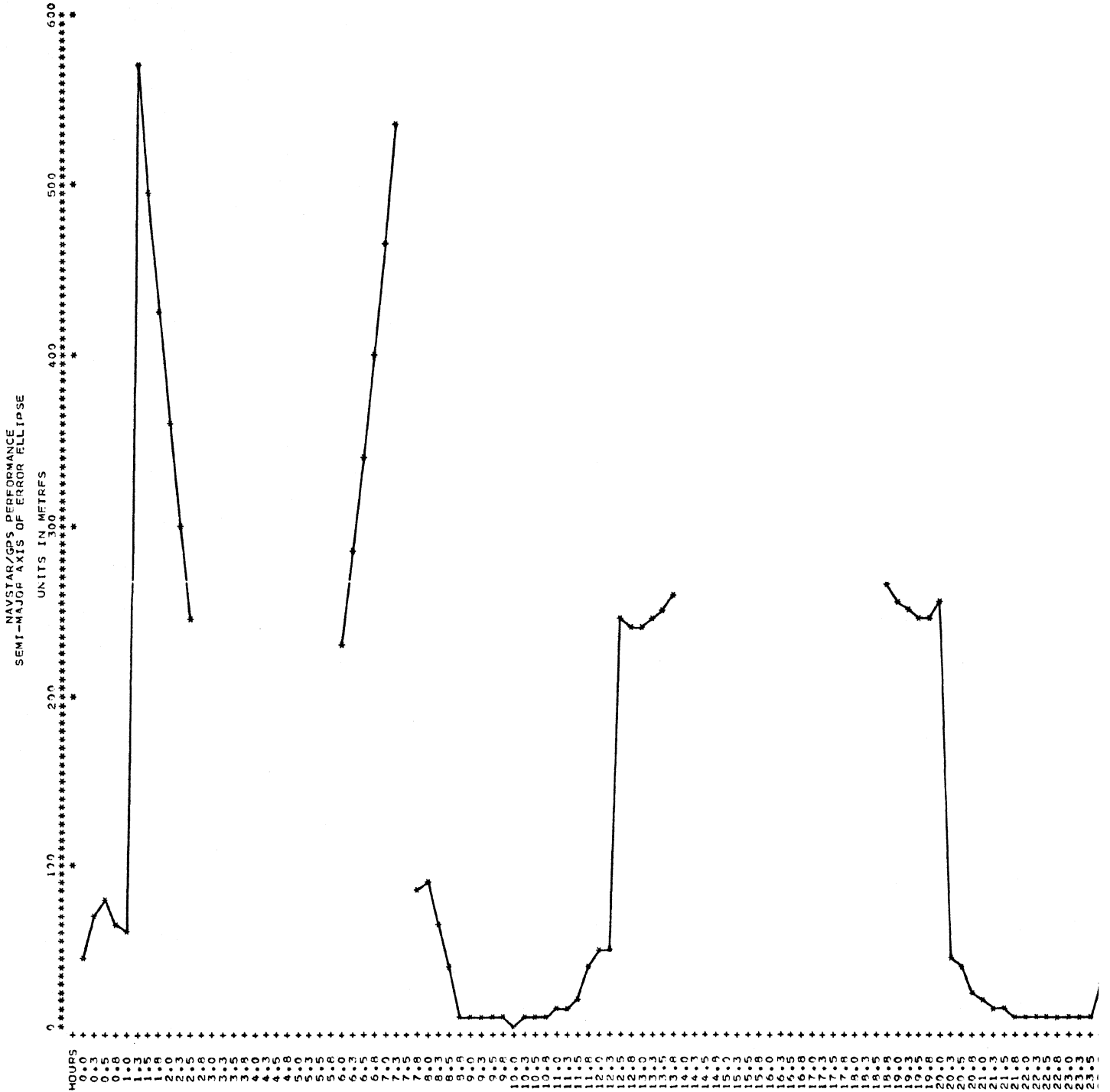
NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

UNITS IN METRES

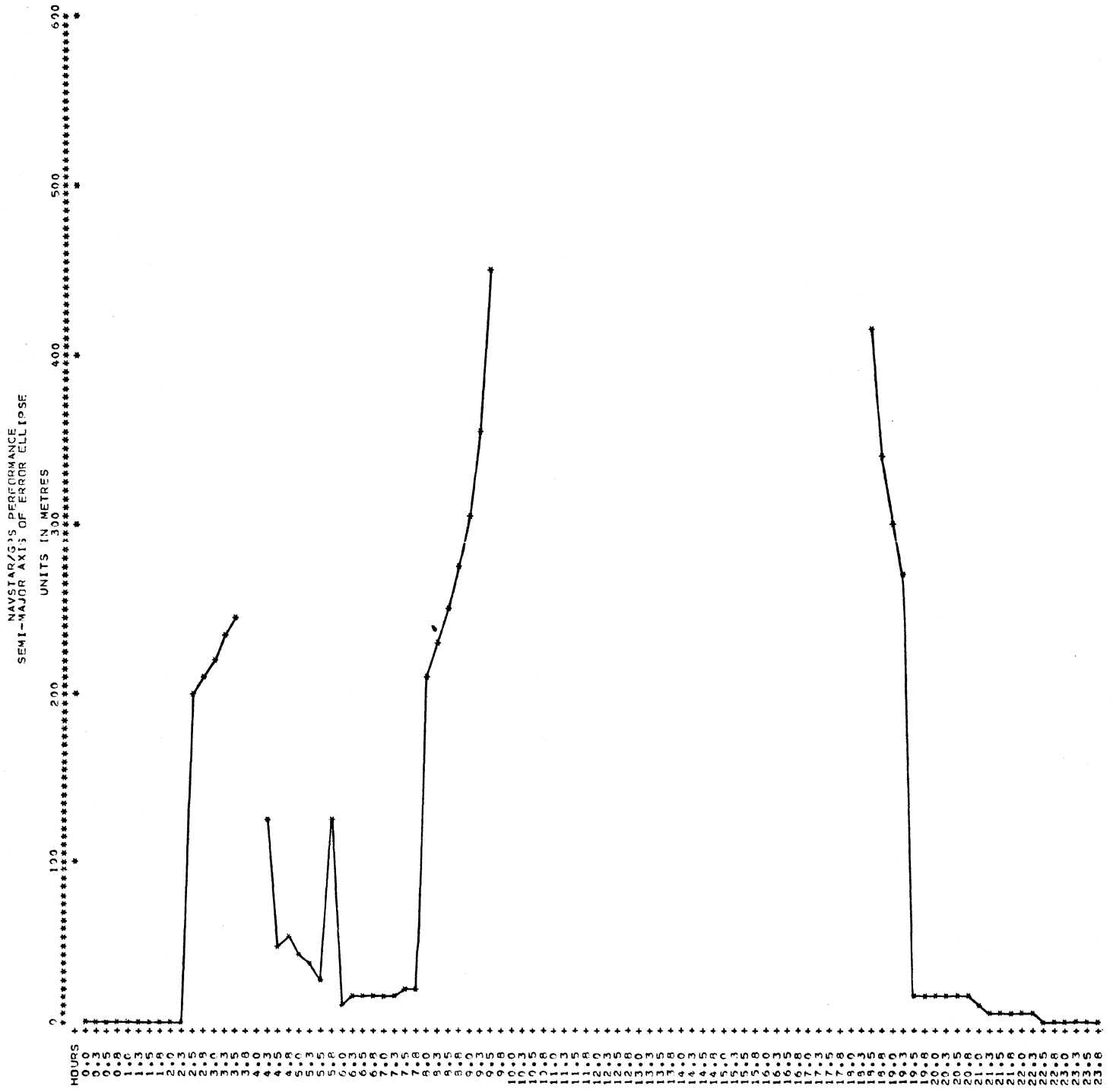


Latitude 40° N, Longitude 25° W using P-code

18



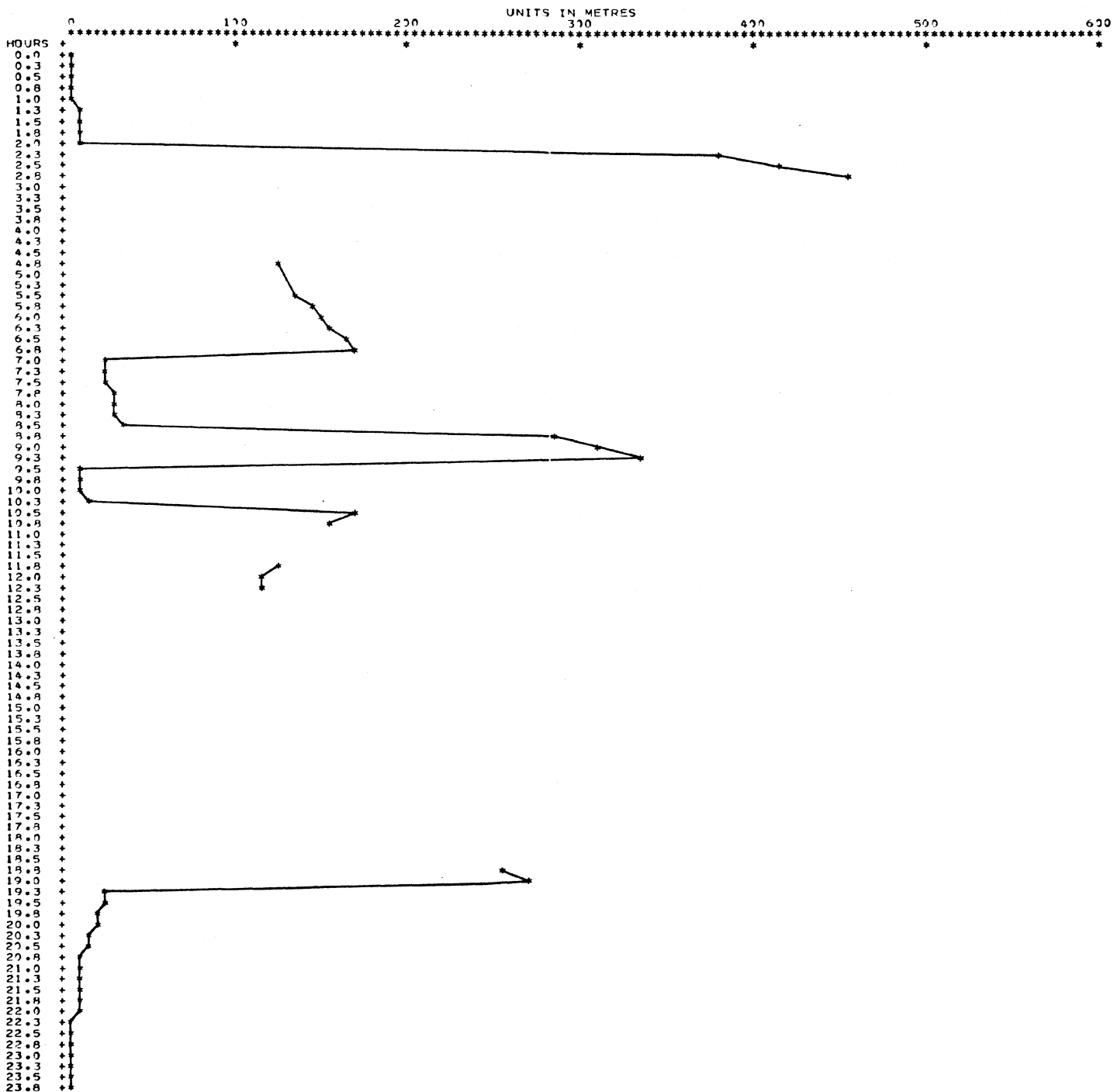
Latitude 60° N , longitude 25° W using P-code

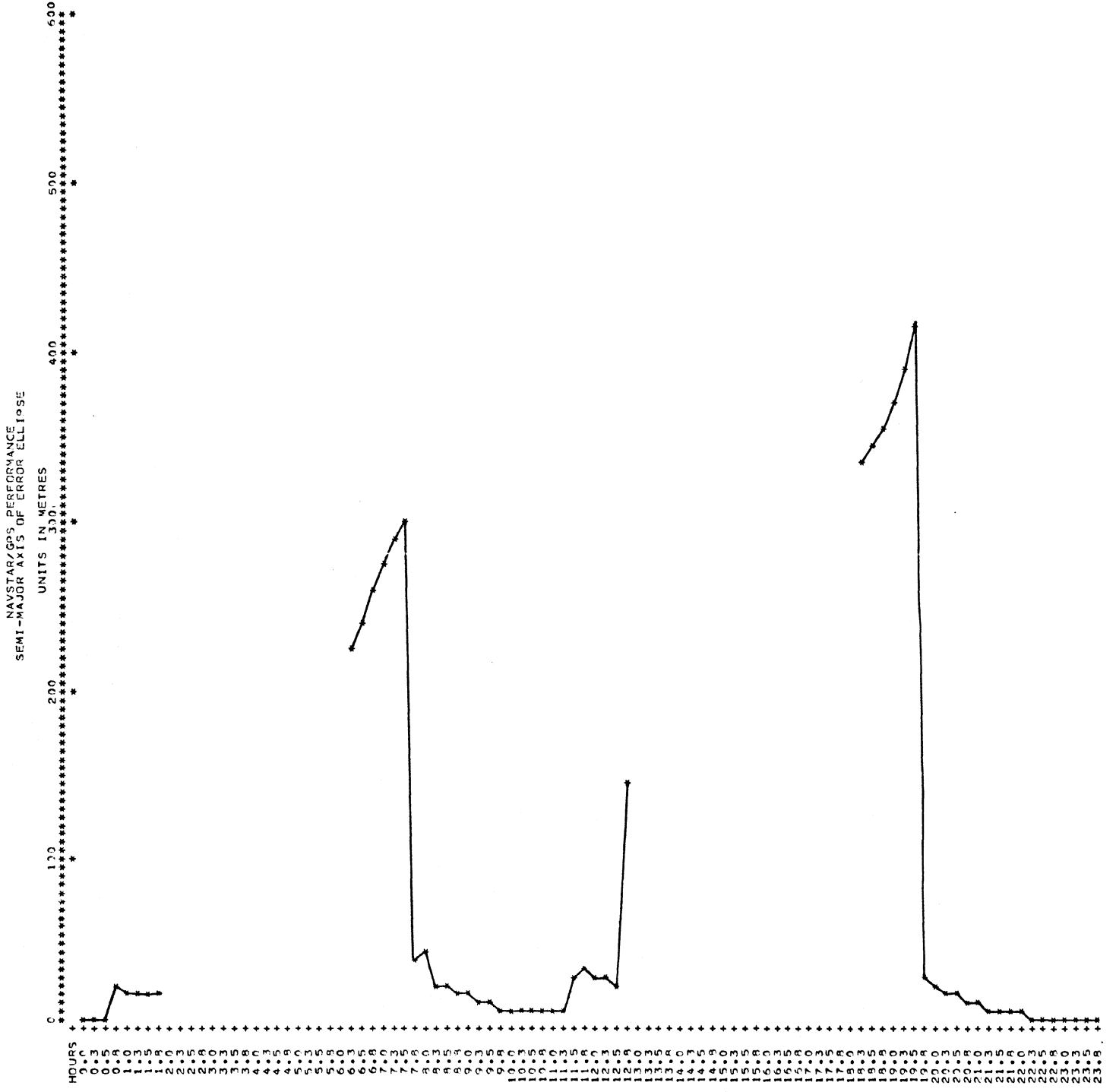


Latitude 20° N , longitude 70° W using p-code

NAVSTAR/GPS PERFORMANCE
SEMI-MAJOR AXIS OF ERROR ELLIPSE

Latitude 40° N, Longitude 70° W using P-code





Latitude 60° N , longitude 70° W using P-code

APPENDIX CLISTINGS OF RESULTS

1. BAFFIN BAY P-CODE	NO LORAN
2. BAFFIN BAY C/A CODE	NO LORAN
3. BAFFIN BAY C/A CODE	WITH LORAN
4. DAVIS STRAIT P-CODE	NO LORAN
5. DAVIS STRAIT C/A CODE	NO LORAN
6. DAVIS STRAIT C/A CODE	WITH LORAN
7. LABRADOR P-CODE	NO LORAN
8. LABRADOR C/A CODE	NO LORAN
9. LABRADOR C/A CODE	WITH LORAN

Column headings for each listing

DAY HH MM	1980 day, hour minute
EL AZ LAT LONG	elevation and azimuth of satellite in degrees, as seen from ground station, and latitude and longitude of satellite ground track, in degrees
AA BB PHI	GPS error ellipse semi-major axis (AA), semi-minor axis (BB), and orientation of semi-major axis (clockwise from north). AA, BB in metres, PHI in degrees.
no headings	number of satellites visible number of Loran-C ranges combined with GPS

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 70.0000 LONGITUDE = 292.0000

BAFFIN BAY
P - Code

OPTIONS USED FOR THIS RUN

CODE : PRECISE

SIGMA PSEUDO-RANGE = 4.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.59572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91859777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585563D-03

DAY	SAT # 4				SAT # 5				SAT # 6				SAT # 7				SAT # 8				SAT # 9			ERROR ELLIPSE							
	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	AA	BB	PHI						
275	0	0	59	117	51	-31	59	-92	57	-119	0	0	-26	-97	39	-74	51	-148	5	104	13	1	8	-127	9	-116	7	6	28	5	0
275	0	4	55	117	50	-29	60	-93	59	-116	0	0	-28	-97	38	-77	49	-146	3	105	11	1	6	-127	7	-116	7	6	32	5	0
275	0	9	52	117	48	-28	63	-94	60	-113	0	0	-30	-96	37	-80	47	-145	1	106	9	1	4	-128	5	-116	7	6	37	5	0
275	0	14	53	118	46	-27	65	-95	61	-110	0	0	-32	-96	35	-82	45	-144	0	0	7	1	2	-128	2	-116	10	7	6	4	0
275	0	19	47	118	44	-25	67	-97	62	-106	0	0	-34	-96	34	-84	43	-143	0	0	4	1	0	0	0	-116	822	8	51	3	0
275	0	24	45	118	42	-25	70	-100	62	-102	0	0	-36	-95	32	-86	41	-142	0	0	2	1	0	0	-1	-116	213	8	52	3	0
275	0	29	42	119	40	-24	72	-104	63	-98	0	0	-38	-95	30	-88	39	-141	0	0	0	1	0	0	-3	-116	117	8	53	3	0
275	0	34	40	119	38	-23	74	-109	63	-93	0	0	-40	-94	28	-90	37	-140	0	0	-1	1	0	0	-6	-116	83	8	54	3	0
275	0	39	37	120	36	-23	76	-116	63	-89	0	0	-42	-93	26	-92	35	-140	0	0	-4	0	0	0	-8	-117	66	8	54	3	0
275	0	44	35	120	34	-22	77	-125	63	-85	0	0	-44	-92	24	-93	33	-139	0	0	-6	0	0	0	-10	-117	56	8	55	3	0
275	0	49	33	121	32	-22	78	-136	63	-80	0	0	-46	-91	22	-95	31	-139	0	0	-8	0	0	0	-12	-117	50	8	56	3	0
275	0	54	30	122	30	-22	79	-150	62	-76	0	0	-48	-90	20	-96	29	-139	0	0	-10	0	0	0	-14	-117	47	8	56	3	0
275	0	59	28	122	27	-21	78	-163	61	-73	0	0	-50	-89	18	-97	27	-139	0	0	-13	0	0	0	-17	-117	44	8	57	3	0
275	1	4	25	123	25	-21	77	-175	60	-69	0	0	-52	-87	16	-98	24	-139	0	0	-15	0	0	0	-19	-117	43	8	58	3	0
275	1	9	23	124	23	-21	76	-175	59	-66	0	0	-53	-85	14	-99	22	-138	0	0	-17	0	0	0	-21	-117	42	8	58	3	0
275	1	14	21	125	21	-21	74	-167	58	-63	0	0	-55	-83	12	-100	20	-138	0	0	-19	0	0	0	-23	-117	42	8	58	3	0
275	1	19	18	125	19	-21	72	-162	57	-60	0	0	-56	-81	9	-101	18	-138	0	0	-21	0	0	0	-25	-117	43	8	59	3	0
275	1	24	16	126	16	-21	70	-158	55	-58	0	0	-58	-78	7	-102	15	-138	0	0	-24	0	0	0	-27	-116	45	8	59	3	0
275	1	29	14	127	14	-21	67	-155	53	-56	0	0	-59	-75	5	-103	13	-139	0	0	-26	0	0	0	-30	-116	48	8	59	3	0
275	1	34	12	128	12	-21	65	-153	52	-54	0	0	-60	-72	3	-103	11	-139	0	0	-28	0	0	0	-32	-116	52	8	59	3	0

24

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 70.0000 LONGITUDE = 292.0000

BAFFIN BAY

OPTIONS USED FOR THIS RUN

C/A - Code

CODE : C/A

SIGMA PSEUDO-RANGE = 16.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

DAY	SAT # 4					SAT # 5					SAT # 6					SAT # 7					SAT # 8					SAT # 9					ERROR ELLIPSE		
	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	AA	BB	PHI
275	0	0	58	117	51	-31	58	-92	57	-119	0	0	-26	-97	39	-74	51	-148	5	104	13	1	8	-127	9	-116	30	25	28	5	0		
275	0	4	55	117	50	-29	60	-93	59	-116	0	0	-28	-97	38	-77	49	-146	3	105	11	1	6	-127	7	-116	30	26	32	5	0		
275	0	9	52	117	48	-28	63	-94	60	-113	0	0	-30	-96	37	-80	47	-145	1	106	9	1	4	-128	5	-116	30	26	37	5	0		
275	0	14	50	118	46	-27	65	-95	61	-110	0	0	-32	-96	35	-82	45	-144	0	0	7	1	2	-128	2	-116	42	28	6	4	0		
275	0	19	47	118	44	-25	67	-97	62	-106	0	0	-34	-96	34	-84	43	-143	1	0	4	1	0	0	0	-116	83	35	51	3	0		
275	0	24	45	118	42	-25	70	-100	62	-102	0	0	-36	-95	32	-86	41	-142	0	0	2	1	0	0	-1	-116	57	35	52	3	0		
275	0	29	42	119	40	-24	72	-104	63	-98	0	0	-38	-95	30	-88	39	-141	0	0	0	1	0	0	-3	-116	39	34	53	3	0		
275	0	34	40	119	38	-23	74	-109	63	-93	0	0	-40	-94	28	-90	37	-140	0	0	-1	1	0	0	-6	-116	29	34	53	3	0		
275	0	39	37	120	36	-23	76	-116	63	-89	0	0	-42	-93	26	-92	35	-140	0	0	-4	0	0	0	-8	-117	24	34	54	3	0		
275	0	44	35	120	34	-22	77	-125	63	-85	0	0	-44	-92	24	-93	33	-139	0	0	-6	0	0	0	-10	-117	21	34	55	3	0		
275	0	49	33	121	32	-22	78	-136	63	-80	0	0	-46	-91	22	-95	31	-139	0	0	-8	0	0	0	-12	-117	18	33	56	3	0		
275	0	54	30	122	30	-22	79	-150	62	-76	0	0	-48	-90	20	-96	29	-139	0	0	-10	0	0	0	-14	-117	17	33	56	3	0		
275	0	59	28	122	27	-21	78	-163	61	-73	0	0	-50	-89	18	-97	27	-139	0	0	-13	0	0	0	-17	-117	16	33	57	3	0		
275	1	4	25	123	25	-21	77	-175	60	-69	0	0	-52	-87	16	-98	24	-139	0	0	-15	0	0	0	-19	-117	15	33	57	3	0		
275	1	9	23	124	23	-21	75	-175	59	-66	0	0	-53	-85	14	-99	22	-138	0	0	-17	0	0	0	-21	-117	15	32	58	3	0		
275	1	14	21	125	21	-21	74	-167	58	-63	0	0	-55	-83	12	-100	20	-138	0	0	-19	0	0	0	-23	-117	15	32	58	3	0		
275	1	19	18	125	19	-21	72	-162	57	-60	0	0	-56	-81	9	-101	18	-138	0	0	-21	0	0	0	-25	-117	15	32	58	3	0		
275	1	24	16	126	16	-21	70	-158	55	-58	0	0	-58	-78	7	-102	15	-138	0	0	-24	0	0	0	-27	-116	15	32	58	3	0		
275	1	29	14	127	14	-21	67	-155	53	-56	0	0	-59	-75	5	-103	13	-139	0	0	-26	0	0	0	-30	-116	16	32	58	3	0		
275	1	34	12	128	12	-21	65	-153	52	-54	0	0	-60	-72	3	-103	11	-139	0	0	-28	0	0	0	-32	-116	17	32	58	3	0		

275	1	3	9	9	129	13	-	62	152	50	-52	0	0	-61	-68	1	104	9	-139	0	0	-30	1	0	0	-34	-115	178	32	58	3	0
275	1	1	4	5	129	131	-	60	151	48	-51	0	0	-62	-65	0	0	7	-139	0	0	-32	0	0	0	-36	-115	478	76	37	2	0
275	1	1	5	5	130	131	-	57	150	46	-50	0	0	-62	-61	0	0	4	-139	0	0	-34	0	0	0	-40	-115	447	81	37	2	0
275	1	1	5	3	131	131	-	55	149	44	-49	0	0	-62	-56	0	0	2	-139	0	0	-36	0	0	0	-42	-113	416	86	37	2	0
275	2	2	4	0	0	0	-	52	149	42	-48	0	0	-63	-52	0	0	0	-139	0	0	-38	0	0	0	-44	-112	386	92	0	0	0
275	2	2	4	0	0	0	-	50	149	40	-47	0	0	-63	-48	0	0	1	-139	0	0	-40	0	0	0	-46	-111	0	0	0	0	0
275	2	2	9	0	0	0	-	47	146	38	-47	0	0	-62	-44	0	0	1	-139	0	0	-42	0	0	0	-46	-111	0	0	0	0	0
275	2	2	9	0	0	0	-	45	149	36	-46	0	0	-62	-40	0	0	1	-140	0	0	-44	0	0	0	-47	-110	0	0	0	0	0
275	2	2	9	0	0	0	-	42	149	34	-46	0	0	-60	-36	0	0	1	-140	0	0	-46	0	0	0	-49	-109	0	0	0	0	0
275	2	2	4	0	0	0	-	39	150	32	-45	0	0	-60	-32	0	0	1	-140	0	0	-48	0	0	0	-51	-107	0	0	0	0	0
275	2	2	9	0	0	0	-	37	150	30	-45	0	0	-59	-29	0	0	1	-140	0	0	-50	0	0	0	-53	-105	0	0	0	0	0
275	2	2	9	0	0	0	-	34	150	28	-45	0	0	-58	-26	0	0	1	-140	0	0	-52	0	0	0	-54	-103	0	0	0	0	0
275	2	2	3	0	0	0	-	32	151	26	-45	0	0	-57	-23	0	0	1	-140	0	0	-53	0	0	0	-56	-101	0	0	0	0	0
275	2	2	4	0	0	0	-	29	151	23	-45	0	0	-55	-21	0	0	1	-140	0	0	-55	0	0	0	-57	-99	0	0	0	0	0
275	2	2	4	0	0	0	-	27	152	21	-45	0	0	-54	-18	0	0	1	-140	0	0	-56	0	0	0	-58	-96	0	0	0	0	0
275	2	2	5	0	0	0	-	25	152	19	-45	0	0	-52	-16	0	0	1	-140	0	0	-58	0	0	0	-59	-93	0	0	0	0	0
275	2	2	5	0	0	0	-	22	152	17	-45	0	0	-50	-15	0	0	1	-140	0	0	-59	0	0	0	-60	-89	0	0	0	0	0
275	2	2	4	0	0	0	-	20	153	15	-45	0	0	-49	-13	0	0	1	-140	0	0	-60	0	0	0	-61	-86	0	0	0	0	0
275	2	2	9	0	0	0	-	17	153	12	-45	0	0	-47	-12	0	0	1	-140	0	0	-61	0	0	0	-62	-82	0	0	0	0	0
275	2	2	9	0	0	0	-	15	154	10	-45	0	0	-45	-11	0	0	1	-139	0	0	-62	0	0	0	-62	-78	0	0	0	0	0
275	2	2	9	0	0	0	-	13	154	8	-45	0	0	-43	-10	0	0	1	-139	0	0	-62	0	0	0	-62	-74	0	0	0	0	0
275	2	2	4	0	0	0	-	10	155	6	-45	0	0	-41	-9	0	0	1	-138	0	0	-63	0	0	0	-62	-70	0	0	0	0	0
275	2	2	9	0	0	0	-	8	155	3	-45	0	0	-39	-8	0	0	1	-138	0	0	-63	0	0	0	-62	-66	0	0	0	0	0
275	2	2	3	0	0	0	-	6	156	1	-45	0	0	-37	-8	0	0	1	-137	0	0	-63	0	0	0	-62	-62	0	0	0	0	0
275	2	2	3	0	0	0	-	4	156	0	-45	0	0	-35	-7	0	0	1	-137	0	0	-62	0	0	0	-61	-58	0	0	0	0	0
275	2	2	4	0	0	0	-	1	157	0	-46	0	0	-33	-7	0	0	1	-136	0	0	-62	0	0	0	-60	-54	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-31	-7	0	0	1	-135	0	0	-61	0	0	0	-60	-51	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-28	-6	0	0	1	-134	0	0	-61	0	0	0	-60	-48	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-26	-6	0	0	1	-132	0	0	-61	0	0	0	-60	-45	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-24	-6	0	0	1	-131	0	0	-62	0	0	0	-60	-42	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-22	-6	0	0	1	-129	0	0	-63	0	0	0	-60	-40	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-20	-6	0	0	1	-127	0	0	-63	0	0	0	-60	-38	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-18	-6	0	0	1	-125	0	0	-64	0	0	0	-60	-36	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-15	-6	0	0	1	-122	0	0	-64	0	0	0	-60	-35	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-13	-6	0	0	1	-119	0	0	-65	0	0	0	-60	-33	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-11	-6	0	0	1	-116	0	0	-65	0	0	0	-60	-32	0	0	0	0	0
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275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-6	-6	0	0	1	-109	0	0	-66	0	0	0	-60	-30	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-4	-6	0	0	1	-105	0	0	-66	0	0	0	-60	-29	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-46	0	0	-2	-6	0	0	1	-101	0	0	-67	0	0	0	-60	-29	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-45	0	0	0	-6	0	0	1	-97	0	0	-67	0	0	0	-60	-29	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-45	0	0	2	-7	0	0	1	-92	0	0	-67	0	0	0	-60	-28	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-44	0	0	4	-7	0	0	1	-88	0	0	-67	0	0	0	-60	-27	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-44	0	0	6	-7	0	0	1	-84	0	0	-67	0	0	0	-60	-27	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-42	0	0	8	-7	0	0	1	-80	0	0	-67	0	0	0	-60	-27	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-42	0	0	10	-7	0	0	1	-76	0	0	-67	0	0	0	-60	-27	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-40	0	0	12	-7	0	0	1	-73	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-38	0	0	14	-7	0	0	1	-70	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-36	0	0	15	-7	0	0	1	-67	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-34	0	0	17	-7	0	0	1	-64	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-32	0	0	19	-7	0	0	1	-60	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-29	0	0	21	-7	0	0	1	-58	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-26	0	0	23	-7	0	0	1	-57	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-23	0	0	25	-6	0	0	1	-55	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-20	0	0	28	-6	0	0	1	-54	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-16	0	0	30	-6	0	0	1	-54	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-12	0	0	32	-5	0	0	1	-53	0	0	-67	0	0	0	-60	-26	0	0	0	0	0
275	2	2	4	0	0	0	-	0	0	0	-7	0	0	34	-5	0	0	1	-52	0	0	-67	0	0	0	-60	-26	0</				

275	12	59	0	0	27	158	29	2	61	108	0	0	-1	50	91	4	63	26	40	0	0	-13	-179	0	0	-17	62	203	42	32	2	0
275	13	9	0	0	24	158	28	0	60	111	0	0	-52	93	22	2	64	23	40	0	0	-16	-179	0	0	-20	62	204	40	32	0	0
275	13	14	0	0	22	158	26	-1	59	114	0	0	-54	95	0	0	64	21	41	0	0	-18	-179	0	0	-22	62	205	39	32	0	0
275	13	19	0	0	20	158	25	-3	57	117	0	0	-55	97	0	0	0	19	41	0	0	-20	-179	0	0	-24	62	0	0	0	0	0
275	13	24	0	0	18	158	23	-5	56	120	0	0	-56	99	0	0	0	17	41	0	0	-22	-179	0	0	-26	62	0	0	0	0	0
275	13	29	0	0	16	159	22	-7	54	122	0	0	-57	102	0	0	0	15	41	0	0	-24	-179	0	0	-28	63	0	0	0	0	0
275	13	34	0	0	13	159	20	-10	53	124	0	0	-58	105	0	0	0	12	40	0	0	-27	-179	0	0	-30	63	0	0	0	0	0
275	13	39	0	0	11	158	18	-11	51	126	0	0	-59	109	0	0	0	10	40	0	0	-29	-179	0	0	-33	63	0	0	0	0	0
275	13	44	0	0	9	158	17	-11	49	127	0	0	-60	112	0	0	0	8	40	0	0	-31	-178	0	0	-35	64	0	0	0	0	0
275	13	49	0	0	7	158	15	-11	47	128	0	0	-62	116	0	0	0	6	40	0	0	-33	-178	0	0	-37	64	0	0	0	0	0
275	13	54	0	0	4	158	13	-11	45	129	0	0	-62	120	0	0	0	3	40	0	0	-35	-178	0	0	-39	65	0	0	0	0	0
275	13	59	0	0	2	158	11	-11	44	130	0	0	-63	124	0	0	0	1	40	0	0	-37	-177	0	0	-41	65	0	0	0	0	0
275	14	4	0	0	0	157	9	-11	42	131	0	0	-63	129	0	0	0	0	40	0	0	-39	-176	0	0	-43	66	0	0	0	0	0
275	14	9	0	0	-1	157	7	-11	40	132	0	0	-62	133	0	0	0	-2	40	0	0	-41	-176	0	0	-45	67	0	0	0	0	0
275	14	14	0	0	-4	157	5	-11	37	133	0	0	-62	137	0	0	0	-5	39	0	0	-43	-175	0	0	-46	68	0	0	0	0	0
275	14	19	0	0	-6	157	3	-11	35	133	0	0	-62	141	0	0	0	-7	39	0	0	-45	-174	0	0	-48	69	0	0	0	0	0
275	14	24	0	0	-8	157	1	-11	33	133	0	0	-61	145	0	0	0	-9	39	0	0	-47	-173	0	0	-50	71	0	0	0	0	0
275	14	29	0	0	-10	157	0	-11	31	134	0	0	-60	148	0	0	0	-11	39	0	0	-49	-171	0	0	-52	72	0	0	0	0	0
275	14	34	0	0	-13	157	0	-11	29	134	0	0	-59	151	0	0	0	-13	39	0	0	-51	-170	0	0	-53	74	0	0	0	0	0
275	14	39	0	0	-15	157	0	-11	27	134	0	0	-57	154	0	0	0	-16	39	0	0	-52	-168	0	0	-55	76	0	0	0	0	0
275	14	44	0	0	-17	157	0	-11	25	134	0	0	-56	157	0	0	0	-18	39	0	0	-54	-166	0	0	-56	79	0	0	0	0	0
275	14	49	0	0	-19	157	0	-11	22	134	0	0	-55	159	0	0	0	-20	39	0	0	-56	-164	0	0	-58	81	0	0	0	0	0
275	14	54	0	0	-21	157	0	-11	20	134	0	0	-53	161	0	0	0	-22	39	0	0	-57	-162	0	0	-59	84	0	0	0	0	0
275	14	59	0	0	-24	157	0	-11	18	134	0	0	-51	163	0	0	0	-24	39	0	0	-58	-159	0	0	-60	88	0	0	0	0	0
275	15	4	0	0	-26	157	0	-11	16	134	0	0	-50	165	0	0	0	-27	39	0	0	-59	-156	0	0	-61	91	0	0	0	0	0
275	15	9	0	0	-28	157	0	-11	14	134	0	0	-48	166	0	0	0	-29	39	0	0	-60	-152	0	0	-61	95	0	0	0	0	0
275	15	14	0	0	-30	157	0	-11	11	134	0	0	-46	167	0	0	0	-31	40	0	0	-61	-149	0	0	-62	99	0	0	0	0	0
275	15	19	0	0	-32	158	0	-11	9	134	0	0	-44	169	0	0	0	-33	40	0	0	-62	-145	0	0	-62	103	0	0	0	0	0
275	15	24	0	0	-34	158	0	-11	7	134	0	0	-42	169	0	0	0	-35	40	0	0	-62	-141	0	0	-62	107	0	0	0	0	0
275	15	29	0	0	-36	159	0	-11	5	134	0	0	-40	170	0	0	0	-37	41	0	0	-63	-136	0	0	-62	111	0	0	0	0	0
275	15	34	0	0	-39	159	0	-11	2	133	0	0	-38	171	0	0	0	-39	41	0	0	-63	-132	0	0	-62	115	0	0	0	0	0
275	15	39	0	0	-41	160	0	-11	0	133	0	0	-36	171	0	0	0	-41	42	0	0	-63	-128	0	0	-62	119	0	0	0	0	0
275	15	44	0	0	-43	161	0	-11	-1	133	0	0	-34	172	0	0	0	-43	43	0	0	-62	-124	0	0	-61	123	0	0	0	0	0
275	15	49	0	0	-45	162	0	-11	-3	133	0	0	-32	172	0	0	0	-45	44	0	0	-62	-120	0	0	-60	126	0	0	0	0	0
275	15	54	0	0	-46	163	0	-11	-6	133	0	0	-30	173	0	0	0	-47	45	0	0	-61	-116	0	0	-59	130	0	0	0	0	0
275	15	59	0	0	-48	164	0	-11	-8	133	0	0	-28	173	0	0	0	-49	46	0	0	-60	-112	0	0	-58	133	0	0	0	0	0
275	16	4	0	0	-50	165	0	-11	-10	133	0	0	-25	173	0	0	0	-51	47	0	0	-59	-109	0	0	-57	135	0	0	0	0	0
275	16	9	0	0	-52	167	0	-11	-12	133	0	0	-23	173	0	0	0	-52	49	0	0	-57	-106	0	0	-55	138	0	0	0	0	0
275	16	14	0	0	-53	169	0	-11	-14	133	0	0	-21	173	0	0	0	-54	51	0	0	-56	-104	0	0	-54	140	0	0	0	0	0
275	16	19	0	0	-55	171	0	-11	-17	133	0	0	-19	173	0	0	0	-55	53	0	0	-55	-101	0	0	-52	142	0	0	0	0	0
275	16	24	0	0	-57	173	0	-11	-19	133	0	0	-17	173	0	0	0	-57	55	0	0	-53	-99	0	0	-50	144	0	0	0	0	0
275	16	29	0	0	-58	176	0	-11	-21	133	0	0	-14	173	0	0	0	-58	58	0	0	-51	-97	0	0	-49	145	0	0	0	0	0
275	16	34	0	0	-59	179	0	-11	-23	133	0	0	-12	173	0	0	0	-59	61	0	0	-50	-96	0	0	-47	146	0	0	0	0	0
275	16	39	0	0	-60	177	0	-11	-26	133	0	0	-10	173	0	0	0	-60	64	0	0	-48	-94	0	0	-45	147	0	0	0	0	0
275	16	44	0	0	-61	173	0	-11	-28	133	0	0	-8	173	0	0	0	-61	68	0	0	-46	-93	0	0	-43	148	0	0	0	0	0
275	16	49	0	0	-62	169	0	-11	-30	133	0	0	-6	173	0	0	0	-62	72	0	0	-44	-92	0	0	-41	149	0	0	0	0	0
275	16	54	0	0	-62	165	0	-11	-32	133	0	0	-3	173	0	0	0	-63	76	0	0	-42	-91	0	0	-39	150	0	0	0	0	0
275	16	59	0	0	-63	157	0	-11	-34	134	0	0	-1	173	0	0	0	-63	80	0	0	-40	-91	0	0	-37	151	0	0	0	0	0
275	17	4	0	0	-63	157	0	-11	-36	134	0	0	0	172	0	0	0	-63	84	0	0	-38	-90	0	0	-35	151	0	0	0	0	0
275	17	9	0	0	-63	152	0	-11	-38	135	0	0	2	172	0	0	0	-63	88	0	0	-36	-89	0	0	-33	152	0	0	0	0	0
275	17	14	0	0	-62	148	0	-11	-40	135	0	0	5	172	0	0	0	-63	93	0	0	-34	-89	0	0	-31	152	0	0	0	0	0
275	17	19	0	0	-62	144	0	-11	-42	136	0	0	7	172	0	0	0	-62	97	0	0	-32	-89	0	0	-29	152	0	0	0	0	0
275	17	24	0	0	-61	140	0	-11	-44	137	0	0	9	172	0	0	0	-61	101	0	0	-29	-88	0	0	-27	152	0	0	0	0	0
275	17	29	0	0	-60	137	0	-11	-46	138	0	0	11	172	0	0	0	-60	104	0	0	-27	-88	0	0	-25	152	0	0	0	0	0
275	17	34	0	0	-59	133	0	-11	-48	139	0	0	14	172	0	0	0	-59	107	0	0	-25	-88	0	0	-22	153	0	0	0	0	0
275	17	39	0	0																												

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 70.0000 LONGITUDE = 292.0000

BAFFIN BAY
C/A Code
Loran - C

OPTIONS USED FOR THIS RUN

CODE : C/A

SIGMA PSEUDO-RANGE = 16.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG. OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

SAT # 4		SAT # 5				SAT # 6				SAT # 7				SAT # 8				SAT # 9				ERROR ELLIPSE									
DAY	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	AA	BB	PHI		
275	0	0	58	117	51	-31	58	-92	57	-119	0	0	-26	-97	39	-74	51	-148	5	104	13	1	8	-127	9	-116	30	25	28	5	0
275	0	4	55	117	50	-29	60	-93	59	-116	0	0	-28	-97	38	-77	49	-146	3	105	11	1	6	-127	7	-116	30	26	32	5	0
275	0	9	52	117	48	-28	63	-94	60	-113	0	0	-30	-96	37	-80	47	-145	1	106	9	1	4	-128	5	-116	30	26	37	5	0
275	0	14	50	118	46	-27	65	-95	61	-110	0	0	-32	-96	35	-82	45	-144	0	0	7	1	2	-128	2	-116	42	28	6	4	0
275	0	19	47	119	44	-25	67	-97	62	-106	0	0	-34	-96	34	-84	43	-143	0	0	4	1	0	0	0	-116	271	34	49	3	2
275	0	24	45	118	42	-25	70	-100	62	-102	0	0	-36	-95	32	-86	41	-142	0	0	2	1	0	0	-1	-116	256	34	50	3	2
275	0	29	42	119	40	-24	72	-104	63	-98	0	0	-38	-95	30	-88	39	-141	0	0	0	1	0	0	-3	-116	231	34	51	3	2
275	0	34	41	119	38	-23	74	-109	63	-93	0	0	-40	-94	28	-90	37	-140	0	0	-1	1	0	0	-6	-116	207	33	52	3	2
275	0	39	37	120	36	-23	76	-116	63	-89	0	0	-42	-93	26	-92	35	-140	0	0	-4	0	0	0	-8	-117	187	33	53	3	2
275	0	44	35	120	34	-22	77	-125	63	-85	0	0	-44	-92	24	-93	33	-139	0	0	-6	0	0	0	-10	-117	172	33	54	3	2
275	0	49	33	121	32	-22	78	-136	63	-80	0	0	-46	-91	22	-95	31	-139	0	0	-8	0	0	0	-12	-117	160	33	55	3	2
275	0	54	30	122	30	-22	79	-150	62	-76	0	0	-48	-90	20	-96	29	-139	0	0	-10	0	0	0	-14	-117	152	33	55	3	2
275	0	59	28	122	27	-21	78	-163	61	-73	0	0	-50	-89	18	-97	27	-139	0	0	-13	0	0	0	-17	-117	146	32	56	3	2
275	1	4	25	123	25	-21	77	-175	60	-69	0	0	-52	-87	16	-98	24	-139	0	0	-15	0	0	0	-19	-117	143	32	57	3	2
275	1	9	23	124	23	-21	75	175	59	-66	0	0	-53	-85	14	-99	22	-138	0	0	-17	0	0	0	-21	-117	141	32	57	3	2
275	1	14	21	125	21	-21	74	167	58	-63	0	0	-55	-83	12	-100	20	-138	0	0	-19	0	0	0	-23	-117	142	32	57	3	2
275	1	19	19	125	19	-21	72	162	57	-60	0	0	-56	-81	9	-101	18	-138	0	0	-21	0	0	0	-25	-117	143	32	58	3	2
275	1	24	16	126	16	-21	70	158	55	-58	0	0	-58	-78	7	-102	15	-138	0	0	-24	0	0	0	-27	-116	147	32	58	3	2
275	1	29	14	127	14	-21	67	155	53	-56	0	0	-59	-75	5	-103	13	-139	0	0	-26	0	0	0	-30	-116	151	32	58	3	2
275	1	34	12	128	12	-21	65	153	52	-54	0	0	-60	-72	3	-103	11	-139	0	0	-28	0	0	0	-32	-116	157	31	58	3	2

GPS PERFORMANCE PRE ANALYSIS

LATITUDE = 65.0000 LONGITUDE = 300.0000

OPTIONS USED FOR THIS RUN

DAVIS STRATI
P - Code

CODE : PRECISE

SIGMA PSEUDO-RANGE = 4.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (ODD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26550449D+08	0.26560017D+08	0.26560147C+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

		SAT # 4			SAT # 5			SAT # 6			SAT # 7			SAT # 8			SAT # 9			ERROR ELLIPSE												
DAY	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	AA	BB	PHI							
275	0	0	64	117	51	-31	53	-76	57	-119	0	0	-26	-97	34	-63	51	-148	10	110	13	1	8	-117	9	-116	7	4	42	5	0	
275	0	4	61	118	50	-29	56	-75	59	-116	0	0	-28	-97	33	-66	49	-146	8	111	11	1	6	-118	7	-116	7	4	43	5	0	
275	0	9	59	119	48	-28	58	-75	60	-113	0	0	-30	-96	32	-68	47	-145	6	112	9	1	4	-119	5	-116	7	4	44	5	0	
275	0	14	55	120	46	-27	61	-75	61	-110	0	0	-32	-96	30	-71	45	-144	4	113	7	1	2	-119	2	-116	7	4	45	5	0	
275	0	19	54	121	44	-25	63	-75	62	-106	0	0	-34	-96	29	-73	43	-143	2	114	4	1	0	-120	0	-116	7	4	46	5	0	
275	0	24	51	121	42	-25	66	-76	62	-102	0	0	-36	-95	28	-75	41	-142	0	115	2	1	0	0	-1	-116	10	7	4	47	4	0
275	0	29	49	122	40	-24	69	-77	63	-98	0	0	-38	-95	26	-77	39	-141	0	0	0	1	0	0	-3	-116	81	6	46	3	0	
275	0	34	46	123	38	-23	70	-79	63	-93	0	0	-40	-94	24	-79	37	-140	0	0	-1	1	0	0	-6	-116	62	6	47	3	0	
275	0	39	44	124	36	-23	73	-81	63	-89	0	0	-42	-93	22	-81	35	-140	0	0	-4	0	0	0	-8	-117	51	6	47	3	0	
275	0	44	41	125	34	-22	75	-85	63	-85	0	0	-44	-92	21	-82	33	-139	0	0	-6	0	0	0	-10	-117	44	6	48	3	0	
275	0	49	39	126	32	-22	77	-91	63	-80	0	0	-46	-91	19	-84	31	-139	0	0	-8	0	0	0	-12	-117	40	6	48	3	0	
275	0	54	36	127	30	-22	79	-100	62	-76	0	0	-48	-90	17	-85	29	-139	0	0	-10	0	0	0	-14	-117	37	6	49	3	0	
275	0	59	34	128	27	-21	81	-112	61	-73	0	0	-50	-89	15	-87	27	-139	0	0	-13	0	0	0	-17	-117	35	6	49	3	0	
275	1	4	32	129	25	-21	82	-129	60	-69	0	0	-52	-87	13	-88	24	-139	0	0	-15	0	0	0	-19	-117	34	6	49	3	0	
275	1	9	29	130	23	-21	82	-148	59	-66	0	0	-53	-85	11	-89	22	-138	0	0	-17	0	0	0	-21	-117	33	6	49	3	0	
275	1	14	27	131	21	-21	81	-164	58	-63	0	0	-55	-83	9	-90	20	-138	0	0	-19	0	0	0	-23	-117	32	6	50	3	0	
275	1	19	25	131	19	-21	79	-177	57	-60	0	0	-56	-81	7	-91	18	-138	0	0	-21	0	0	0	-25	-117	33	6	50	3	0	
275	1	24	23	132	16	-21	77	-174	55	-58	0	0	-58	-78	5	-93	15	-138	0	0	-24	0	0	0	-27	-116	33	6	50	3	0	
275	1	29	20	133	14	-21	75	-168	53	-56	0	0	-59	-75	3	-93	13	-139	0	0	-26	0	0	0	-30	-116	34	6	50	3	0	
275	1	34	18	134	12	-21	72	-165	52	-54	0	0	-60	-72	1	-94	11	-139	0	0	-28	0	0	0	-32	-116	36	6	50	3	0	

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 65.0000 LONGITUDE = 300.0000

DAVIS STRAIT
C/A - Code

OPTIONS USED FOR THIS RUN

CODE : C/A

SIGMA PSEUDO-RANGE = 16.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.25560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474330D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	0.10636919D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.25814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

DAY	HH	MM	SAT # 4			SAT # 5			SAT # 6			SAT # 7			SAT # 8			SAT # 9			ERROR ELLIPSE										
			EL	AZ	LAT LONG	EL	AZ	LAT LONG	EL	AZ	LAT LONG	EL	AZ	LAT LONG	EL	AZ	LAT LONG	EL	AZ	LAT LONG	AA	BB	PHI								
275	0	0	64	117	51	-31	53	-76	57	-119	0	0	-26	-97	34	-63	51	-148	17	110	13	1	8	-117	9	-116	30	19	42	5	0
275	0	4	61	118	50	-29	56	-75	59	-116	0	0	-28	-97	33	-66	49	-146	8	111	11	1	6	-118	7	-116	30	19	43	5	0
275	0	9	59	119	48	-28	58	-75	60	-113	0	0	-30	-96	32	-68	47	-145	6	112	9	1	4	-119	5	-116	30	19	44	5	0
275	0	14	56	120	46	-27	61	-75	61	-110	0	0	-32	-96	30	-71	45	-144	4	113	7	1	2	-119	2	-116	31	19	45	5	0
275	0	19	54	121	44	-25	63	-75	62	-106	0	0	-34	-96	29	-73	43	-143	2	114	4	1	0	-120	0	-116	31	19	46	5	0
275	0	24	51	121	42	-25	66	-76	62	-102	0	0	-36	-95	28	-75	41	-142	0	115	2	1	0	0	-1	-116	414	19	47	4	0
275	0	29	49	122	40	-24	68	-77	63	-98	0	0	-38	-95	26	-77	39	-141	0	0	0	1	0	0	-3	-116	315	27	46	3	0
275	0	34	46	123	38	-23	71	-79	63	-93	0	0	-40	-94	24	-79	37	-140	0	0	-1	1	0	0	-6	-116	242	26	47	3	0
275	0	39	44	124	36	-23	73	-81	63	-89	0	0	-42	-93	22	-81	35	-140	0	0	0	0	0	0	-8	-117	201	26	47	3	0
275	0	44	41	125	34	-22	75	-85	63	-85	0	0	-44	-92	21	-82	33	-139	0	0	-6	0	0	0	-10	-117	175	26	48	3	0
275	0	49	39	126	32	-22	77	-91	63	-80	0	0	-46	-91	19	-84	31	-139	0	0	-8	0	0	0	-12	-117	157	25	48	3	0
275	0	54	35	127	30	-22	79	-100	62	-76	0	0	-48	-90	17	-85	29	-139	0	0	-10	0	0	0	-14	-117	145	25	48	3	0
275	0	59	34	128	27	-21	81	-112	61	-73	0	0	-50	-89	15	-87	27	-139	0	0	-13	0	0	0	-17	-117	137	25	49	3	0
275	1	4	32	129	25	-21	82	-129	60	-69	0	0	-52	-87	13	-88	24	-139	0	0	-15	0	0	0	-19	-117	131	25	49	3	0
275	1	9	29	130	23	-21	82	-143	59	-66	0	0	-53	-85	11	-89	22	-138	0	0	-17	0	0	0	-21	-117	128	25	49	3	0
275	1	14	27	131	21	-21	81	-164	58	-63	0	0	-55	-83	9	-90	20	-138	0	0	-19	0	0	0	-23	-117	126	24	50	3	0
275	1	19	25	131	19	-21	79	-177	57	-60	0	0	-56	-81	7	-91	18	-138	0	0	-21	0	0	0	-25	-117	126	24	50	3	0
275	1	24	22	132	16	-21	77	-174	55	-58	0	0	-58	-78	5	-93	15	-138	0	0	-24	0	0	0	-27	-116	127	24	50	3	0
275	1	29	21	133	14	-21	75	-168	53	-56	0	0	-59	-75	3	-93	13	-139	0	0	-26	0	0	0	-30	-116	130	24	50	3	0
275	1	34	18	134	12	-21	72	-165	52	-54	0	0	-60	-72	1	-94	11	-139	0	0	-28	0	0	0	-32	-116	134	24	50	3	0

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 65.0000 LONGITUDE = 300.0000

DAVIS STRAIT
C/A - Code
Loran - C

OPTIONS USED FOR THIS RUN

CODE : C/A
SIGMA PSEUDO-RANGE = 16.00 (M)
SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.585728000+06	0.585728000+06	0.585728000+06	0.585728000+06	0.585728000+06	0.225280000+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.265603990+08	0.265609430+08	0.265602540+08	0.265604490+08	0.265600170+08	0.265601470+08
MEAN ANOMALY @ TREF (RADIAN)	-0.211596850+01	0.128333930+01	0.854311820+00	-0.328709600+00	0.172125730+01	-0.918697770+00
ECCENTRICITY	0.149679200-02	0.194740300-02	0.597000120-03	0.695514680-02	0.917434690-03	0.693225910-02
ARG OF PERIGEE (RADIAN)	0.311877890+01	-0.106360190+01	0.172425810+01	0.134195580+01	0.538189110-01	0.146045830+01
INCLINATION (RADIAN)	0.110351150+01	0.111257150+01	0.110119860+01	0.110768800+01	0.110366130+01	0.109817850+01
RIGHT ASCENSION (RADIAN)	-0.578791020+00	-0.580886780+00	-0.268144510+01	-0.264117740+01	-0.578039530+00	0.311434530+01
RATE OF RA (RADIAN/SEC)	-0.626311710-08	-0.618311580-08	-0.620597080-08	-0.637740790-08	-0.621739990-08	-0.622882990-08
MEAN MOTION (RADIAN/SEC)	0.145853610-03	0.145849130-03	0.145854810-03	0.145853200-03	0.145856760-03	0.145855680-03

DAY	SAT # 4				SAT # 5				SAT # 6				SAT # 7				SAT # 8				SAT # 9				ERROR ELLIPSE						
	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	AA	BB	PHI				
275	0	0	64	117	51	-31	53	-76	57	-119	0	0	-26	-97	34	-63	51	-148	10	110	13	1	8	-117	9	-116	30	19	42	5	0
275	0	4	61	118	50	-29	56	-75	59	-116	0	0	-28	-97	33	-65	49	-146	8	111	11	1	6	-118	7	-116	30	19	43	5	0
275	0	0	59	119	48	-23	58	-75	60	-113	0	0	-30	-96	32	-68	47	-145	6	112	9	1	4	-119	5	-116	30	19	44	5	0
275	0	14	56	120	46	-27	61	-75	61	-110	0	0	-32	-96	30	-71	45	-144	4	113	7	1	2	-119	2	-116	31	19	45	5	0
275	0	19	54	120	44	-25	63	-75	62	-106	0	0	-34	-96	29	-73	43	-143	2	114	4	1	0	-120	0	-116	31	19	46	5	0
275	0	24	51	121	42	-25	66	-76	62	-102	0	0	-36	-95	28	-75	41	-142	0	115	2	1	0	0	-1	-116	414	19	47	4	0
275	0	29	49	122	40	-24	68	-77	63	-98	0	0	-38	-95	26	-77	39	-141	0	0	0	1	0	0	-3	-116	203	26	45	3	2
275	0	34	46	123	38	-23	70	-79	63	-93	0	0	-40	-94	24	-79	37	-140	0	0	-1	1	0	0	-6	-116	180	26	46	3	2
275	0	39	44	124	36	-23	73	-81	63	-89	0	0	-42	-93	22	-81	35	-140	0	0	-4	0	0	0	-8	-117	162	25	47	3	2
275	0	44	41	125	34	-22	75	-85	63	-85	0	0	-44	-92	21	-82	33	-139	0	0	-6	0	0	0	-10	-117	148	25	47	3	2
275	0	49	39	126	32	-22	77	-91	63	-80	0	0	-46	-91	19	-84	31	-139	0	0	-8	0	0	0	-12	-117	137	25	47	3	2
275	0	54	36	127	30	-22	79	-100	62	-76	0	0	-48	-90	17	-85	29	-139	0	0	-10	0	0	0	-14	-117	130	25	48	3	2
275	0	59	34	128	27	-21	81	-112	61	-73	0	0	-50	-89	15	-87	27	-139	0	0	-13	0	0	0	-17	-117	124	25	48	3	2
275	1	4	32	129	25	-21	82	-129	60	-69	0	0	-52	-87	13	-88	24	-139	0	0	-15	0	0	0	-19	-117	120	24	49	3	2
275	1	0	29	130	23	-21	82	-148	59	-66	0	0	-53	-85	11	-89	22	-138	0	0	-17	0	0	0	-21	-117	118	24	49	3	2
275	1	14	27	131	21	-21	81	-164	58	-63	0	0	-55	-83	9	-90	20	-138	0	0	-19	0	0	0	-23	-117	117	24	49	3	2
275	1	19	25	131	19	-21	79	-177	57	-60	0	0	-56	-81	7	-91	18	-138	0	0	-21	0	0	0	-25	-117	117	24	49	3	2
275	1	24	22	132	16	-21	77	174	55	-58	0	0	-58	-78	5	-93	15	-138	0	0	-24	0	0	0	-27	-116	119	24	50	3	2
275	1	29	20	133	14	-21	75	168	53	-56	0	0	-59	-75	3	-93	13	-139	0	0	-26	0	0	0	-30	-116	121	24	50	3	2
275	1	34	18	134	12	-21	72	165	52	-54	0	0	-60	-72	1	-94	11	-139	0	0	-28	0	0	0	-32	-116	124	24	50	3	2

275	18	39	0	0	-35	-112	0	0	-63	-177	13	-42	43	176	0	0	-35	128	13	-147	5	-89	0	0	8	152	185	14	2	2	2	2	2
275	18	44	0	0	-32	-112	0	0	-63	-173	16	-42	45	177	0	0	-33	129	15	-146	7	-89	0	0	10	152	184	14	2	2	2	2	
275	18	40	0	0	-30	-111	0	0	-62	-168	18	-42	47	178	0	0	-31	129	18	-145	10	-89	0	0	12	152	185	15	2	2	2	2	
275	18	54	0	0	-28	-111	0	0	-62	-164	20	-42	49	-179	0	0	-29	129	20	-144	12	-89	0	0	14	152	185	15	2	2	2	2	
275	18	59	0	0	-25	-111	0	0	-61	-161	22	-42	51	-178	0	0	-27	130	22	-144	14	-89	0	0	17	152	185	15	1	1	1	1	
275	19	4	0	0	-24	-111	0	0	-60	-157	24	-42	52	-176	0	0	-24	130	25	-143	16	-89	0	0	19	152	186	16	1	1	1	1	
275	19	4	0	0	-22	-111	0	0	-59	-154	27	-43	54	-174	0	0	-22	130	27	-142	18	-89	0	0	21	152	186	16	1	1	1	1	
275	19	14	0	0	-19	-111	0	0	-57	-151	29	-43	56	-172	0	0	-20	130	30	-141	21	-89	0	0	23	152	187	17	1	1	1	1	
275	19	19	0	0	-17	-111	0	0	-56	-149	31	-44	57	-169	0	0	-18	130	32	-141	23	-89	0	0	25	152	189	17	1	1	1	1	
275	19	24	0	0	-15	-111	0	0	-54	-147	33	-44	58	-165	0	0	-16	130	34	-140	25	-89	0	0	28	152	190	18	1	1	1	1	
275	19	30	0	0	-13	-111	0	0	-52	-145	36	-45	59	-163	0	0	-13	130	37	-139	27	-89	0	0	30	152	192	19	1	1	1	1	
275	19	34	0	0	-11	-111	0	0	-51	-143	38	-45	60	-160	0	0	-11	130	39	-138	29	-88	0	0	32	153	194	20	2	2	2	2	
275	19	40	0	0	-8	-111	0	0	-49	-142	40	-45	61	-156	0	0	-9	130	42	-137	31	-88	0	0	34	153	197	21	2	2	2	2	
275	19	44	0	0	-6	-111	0	0	-47	-140	42	-49	62	-152	0	0	-7	129	44	-137	34	-88	1	-27	36	154	184	15	0	3	3	2	
275	19	44	0	0	-4	-111	0	0	-45	-139	44	-51	62	-148	0	0	-4	129	47	-136	36	-87	3	-27	38	154	186	15	1	1	1	1	
275	19	54	0	0	-2	-111	0	0	-43	-138	46	-53	63	-144	0	0	-2	129	50	-135	38	-87	5	-27	40	155	198	16	1	3	3	2	
275	19	5	0	0	0	-12	0	0	-41	-138	47	-55	63	-140	0	0	0	129	52	-135	40	-86	7	-27	42	156	135	13	356	4	4	0	0
275	20	4	0	0	0	-12	0	0	-39	-137	49	-58	62	-135	0	0	1	129	55	-134	42	-85	9	-27	44	157	127	13	356	4	4	0	0
275	20	14	0	0	0	-12	0	0	-37	-136	51	-60	62	-131	0	0	4	129	57	-133	44	-85	11	-29	46	158	119	14	356	4	4	0	0
275	20	19	0	0	0	-12	0	0	-35	-136	52	-64	61	-127	0	0	6	129	60	-133	46	-84	14	-28	43	159	112	14	356	4	4	0	0
275	20	24	0	0	0	-12	0	0	-33	-135	53	-67	61	-124	0	0	8	129	62	-133	48	-82	16	-29	50	160	106	15	356	4	4	0	0
275	20	24	0	0	11	-120	0	0	-31	-135	54	-71	60	-120	0	0	10	128	65	-132	49	-81	18	-29	52	162	100	15	356	4	4	0	0
275	20	29	0	0	13	-119	0	0	-28	-135	55	-75	58	-117	0	0	13	128	63	-132	51	-79	20	-29	53	164	94	16	356	4	4	0	0
275	20	34	0	0	16	-118	0	0	-26	-135	56	-80	57	-114	0	0	15	128	70	-133	53	-78	22	-30	55	166	89	16	356	4	4	0	0
275	20	39	0	0	18	-117	0	0	-24	-135	55	-84	56	-111	0	0	17	128	73	-134	54	-76	24	-31	56	169	85	17	356	4	4	0	0
275	20	44	0	0	20	-116	0	0	-22	-135	56	-89	54	-109	0	0	19	128	75	-135	56	-73	26	-32	58	171	80	18	356	4	4	0	0
275	20	44	0	0	22	-115	0	0	-20	-135	55	-93	53	-107	0	0	22	128	73	-135	57	-71	28	-33	59	175	76	18	356	4	4	0	0
275	20	54	0	0	24	-114	0	0	-17	-135	55	-97	51	-105	0	0	24	128	80	-142	59	-68	30	-34	60	178	72	19	356	4	4	0	0
275	20	59	0	0	27	-113	0	0	-15	-135	54	-102	49	-104	0	0	26	129	83	-151	60	-65	32	-36	61	-177	69	20	356	4	4	0	0
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275	22	34	0	0	73	-96	0	0	26	-136	16	-137	9	-96	26	-21	61	155	46	-93	47	-4	40	-91	44	-120	29	14	354	6	6	0	0
275	22	39	0	0	75	-96	0	0	29	-136	13	-138	7	-96	27	-22	62	159	44	-94	45	-3	39	-94	42	-119	28	14	355	6	6	0	0
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275	22	49	0	0	80	-100	0	0	33	-135	9	-139	3	-96	30	-27	63	167	39	-96	41	-1	36	-99	38	-118	27	14	356	6	6	0	0
275	22	54	0	0	83	-105	0	0	35	-135	6	-140	0	-96	32	-29	63	171	37	-97	39	0	34	-101	36	-117	27	14	357	6	6	0	0

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 55.0000 LONGITUDE =295.0000

LABRADOR
P -Code

OPTIONS USED FOR THIS RUN

CODE : PRECISE

SIGMA PSEUDO-RANGE = 4.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777C+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

			SAT # 4			SAT # 5			SAT # 6			SAT # 7			SAT # 8			SAT # 9			ERROR ELLIPSE										
DAY	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	AA	BB	PHI						
275	0	0	63	84	51	-31	52	-61	57	-119	0	0	-26	-97	31	-58	51	-148	10	101	13	1	16	-118	9	-116	5	4	68	5	0
275	0	4	61	88	50	-29	54	-59	59	-116	0	0	-28	-97	30	-60	49	-146	8	102	11	1	13	-119	7	-116	5	4	68	5	0
275	0	9	59	91	48	-28	56	-57	60	-113	0	0	-30	-96	30	-63	47	-145	7	104	9	1	11	-120	5	-116	5	4	68	5	0
275	0	14	57	93	46	-27	58	-56	61	-110	0	0	-32	-96	29	-66	45	-144	5	105	7	1	9	-121	2	-116	5	4	69	5	0
275	0	19	55	96	44	-25	61	-54	62	-106	0	0	-34	-96	28	-68	43	-143	3	106	4	1	7	-122	0	-116	5	4	69	5	0
275	0	24	53	98	42	-25	63	-52	62	-102	0	0	-36	-95	27	-71	41	-142	1	108	2	1	5	-123	-1	-116	5	4	69	5	0
275	0	29	50	101	40	-24	65	-49	63	-98	0	0	-38	-95	26	-73	39	-141	0	0	0	1	3	-124	-3	-116	5	5	311	4	0
275	0	34	48	103	38	-23	67	-47	63	-93	0	0	-40	-94	25	-75	37	-140	0	0	-1	1	1	-125	-6	-116	5	5	292	4	0
275	0	39	46	105	36	-23	70	-44	63	-89	0	0	-42	-93	23	-78	35	-140	0	0	-4	0	0	0	-8	-117	25	5	64	3	0
275	0	44	44	107	34	-22	72	-41	63	-85	0	0	-44	-92	22	-80	33	-139	0	0	-6	0	0	0	-10	-117	23	5	65	3	0
275	0	49	42	109	32	-22	74	-38	63	-80	0	0	-46	-91	20	-82	31	-139	0	0	-8	0	0	0	-12	-117	21	5	65	3	0
275	0	54	40	111	30	-22	77	-34	62	-76	0	0	-48	-90	19	-84	29	-139	0	0	-10	0	0	0	-14	-117	19	5	66	3	0
275	0	59	37	113	27	-21	79	-28	61	-73	0	0	-50	-89	17	-85	27	-139	0	0	-13	0	0	0	-17	-117	18	5	66	3	0
275	1	4	35	114	25	-21	81	-20	60	-69	0	0	-52	-87	15	-87	24	-139	0	0	-15	0	0	0	-19	-117	17	5	67	3	0
275	1	9	33	116	23	-21	83	-7	59	-66	0	0	-53	-85	13	-89	22	-138	0	0	-17	0	0	0	-21	-117	17	5	67	3	0
275	1	14	31	118	21	-21	85	13	58	-63	0	0	-55	-83	12	-90	20	-138	0	0	-19	0	0	0	-23	-117	16	5	67	3	0
275	1	19	29	119	19	-21	85	47	57	-60	0	0	-56	-81	10	-92	18	-138	0	0	-21	0	0	0	-25	-117	16	5	68	3	0
275	1	24	27	121	16	-21	85	79	55	-58	0	0	-58	-78	8	-93	15	-138	0	0	-24	0	0	0	-27	-116	16	5	68	3	0
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275	1	34	22	124	12	-21	81	109	52	-54	0	0	-60	-72	4	-96	11	-139	0	0	-28	0	0	0	-32	-116	16	5	68	3	0

275	18	39	0	0	-35	-112	0	0	-63	-177	8	-43	43	176	0	0	-35	128	24	-149	5	-89	0	0	8	152	303	3	4	2	0	0		
275	18	44	0	0	-32	-112	0	0	-63	-173	10	-42	45	177	0	0	-33	129	26	-148	7	-89	0	0	10	152	305	3	4	2	0	0		
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275	22	34	73	-54	60	-86	19	-88	26	-136	26	-138	9	96	17	-21	61	155	42	75	47	-4	43	-83	44	120	1768	4	4	4	4	0	0	0
275	22	39	74	-47	61	-83	20	-86	29	-136	23	-139	7	96	18	-22	62	159	40	77	45	-3	42	-86	42	119	1866	4	4	4	4	0	0	0
275	22	44	76	-39	62	-79	22	-84	31	-136	21	-140	5	96	20	-24	62	163	38	78	43	-2	41	-89	40	119	1970	4	4	4	4	0	0	0
275	22	49	77	-30	62	-75	24	-83	33	-135	19	-141	3	96	22	-25	63	167	36	80	41	-1	40	-92	38	118	2081	4	4	4	4	0	0	0
275	22	54	78																															

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 55.0000 LONGITUDE = 295.0000

OPTIONS USED FOR THIS RUN

CODE : C/A

SIGMA PSEUDO-RANGE = 16.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

LABRADOR
C/A - Code

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

		SAT # 4			SAT # 5			SAT # 6			SAT # 7			SAT # 8			SAT # 9			ERROR ELLIPSE												
DAY	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AA	BB	PHI										
275	0	0	63	84	51	-31	52	-61	57	-119	0	0	-26	-97	31	-58	51	-148	10	101	13	1	16	-118	9	-116	23	16	68	5	0	
275	0	4	61	88	50	-29	54	-59	59	-116	0	0	-28	-97	30	-50	49	-146	8	102	11	1	13	-119	7	-116	23	16	68	5	0	
275	0	9	59	91	48	-28	56	-57	60	-113	0	0	-30	-96	30	-63	47	-145	7	104	9	1	11	-120	5	-116	23	16	68	5	0	
275	0	14	57	93	46	-27	58	-56	61	-110	0	0	-32	-96	29	-66	45	-144	5	105	7	1	9	-121	2	-116	23	16	69	5	0	
275	0	19	55	96	44	-25	61	-54	62	-106	0	0	-34	-96	28	-68	43	-143	3	106	4	1	7	-122	0	-116	23	16	69	5	0	
275	0	24	53	98	42	-25	63	-52	62	-102	0	0	-36	-95	27	-71	41	-142	1	108	2	1	5	-123	-1	-116	23	16	69	5	0	
275	0	29	59	101	40	-24	65	-49	63	-98	0	0	-38	-95	26	-73	39	-141	0	0	0	1	3	-124	-3	-116	23	22	311	4	0	
275	0	34	49	103	38	-23	67	-47	63	-93	0	0	-40	-94	25	-75	37	-140	0	0	-1	1	1	-125	-6	-116	23	22	292	4	0	
275	0	39	46	105	36	-23	70	-44	63	-89	0	0	-42	-93	23	-78	35	-140	0	0	-4	0	0	0	0	-8	-117	103	22	64	3	0
275	0	44	44	107	34	-22	72	-41	63	-85	0	0	-44	-92	22	-80	33	-139	0	0	-6	0	0	0	0	-10	-117	92	22	65	3	0
275	0	49	42	109	32	-22	74	-38	63	-80	0	0	-46	-91	20	-82	31	-139	0	0	-8	0	0	0	0	-12	-117	84	22	65	3	0
275	0	54	40	111	30	-22	77	-34	62	-76	0	0	-48	-90	19	-84	29	-139	0	0	-10	0	0	0	0	-14	-117	78	21	66	3	0
275	0	59	37	113	27	-21	79	-28	61	-73	0	0	-50	-89	17	-85	27	-139	0	0	-13	0	0	0	0	-17	-117	73	21	66	3	0
275	1	4	35	114	25	-21	81	-20	60	-69	0	0	-52	-87	15	-87	24	-139	0	0	-15	0	0	0	0	-19	-117	70	21	67	3	0
275	1	9	33	116	23	-21	83	-7	59	-66	0	0	-53	-85	13	-89	22	-138	0	0	-17	0	0	0	0	-21	-117	68	21	67	3	0
275	1	14	31	118	21	-21	85	13	58	-63	0	0	-55	-83	12	-90	20	-138	0	0	-19	0	0	0	0	-23	-117	66	21	67	3	0
275	1	19	29	119	19	-21	85	47	57	-60	0	0	-56	-81	10	-92	18	-138	0	0	-21	0	0	0	0	-25	-117	65	21	68	3	0
275	1	24	27	121	16	-21	85	79	55	-58	0	0	-58	-78	8	-93	15	-138	0	0	-24	0	0	0	0	-27	-116	64	20	68	3	0
275	1	29	25	122	14	-21	83	98	53	-56	0	0	-59	-75	6	-95	13	-139	0	0	-26	0	0	0	0	-30	-116	64	20	68	3	0
275	1	34	22	124	12	-21	81	109	52	-54	0	0	-60	-72	4	-96	11	-139	0	0	-28	0	0	0	0	-32	-116	65	20	68	3	0

GPS PERFORMANCE PRE-ANALYSIS

LATITUDE = 55.0000 LONGITUDE = 295.0000

OPTIONS USED FOR THIS RUN

CODE : C/A

SIGMA PSEUDO-RANGE = 16.00 (M)

SIGMA LORAN-RANGE = 100/SQRT(0.5) (M)

LABRADUR
C/A - Code
Loran - C

SATELLITE NO.	4	5	6	7	8	9
REF. TIME - TIME OF WEEK (SEC)	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.58572800D+06	0.22528000D+06
JULIAN DATE (DDD HH MM SS)	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	145 18 42 8	169 14 34 40
SEMI - MAJOR AXIS (M)	0.26560399D+08	0.26560943D+08	0.26560254D+08	0.26560449D+08	0.26560017D+08	0.26560147D+08
MEAN ANOMALY @ TREF (RADIAN)	-0.21159685D+01	0.12833393D+01	0.85431182D+00	-0.32870960D+00	0.17212573D+01	-0.91869777D+00
ECCENTRICITY	0.14967920D-02	0.19474030D-02	0.59700012D-03	0.69551468D-02	0.91743469D-03	0.69322591D-02
ARG OF PERIGEE (RADIAN)	0.31187789D+01	-0.10636019D+01	0.17242581D+01	0.13419558D+01	0.53818911D-01	0.14604583D+01
INCLINATION (RADIAN)	0.11035115D+01	0.11125715D+01	0.11011986D+01	0.11076880D+01	0.11036613D+01	0.10981785D+01
RIGHT ASCENSION (RADIAN)	-0.57879102D+00	-0.58088678D+00	-0.26814451D+01	-0.26411774D+01	-0.57803953D+00	0.31143453D+01
RATE OF RA (RADIAN/SEC)	-0.62631171D-08	-0.61831158D-08	-0.62059708D-08	-0.63774079D-08	-0.62173999D-08	-0.62288299D-08
MEAN MOTION (RADIAN/SEC)	0.14585361D-03	0.14584913D-03	0.14585481D-03	0.14585320D-03	0.14585676D-03	0.14585568D-03

DAY	SAT # 4			SAT # 5			SAT # 6			SAT # 7			SAT # 8			SAT # 9			ERROR ELLIPSE												
	HH	MM	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AZ	LAT	LONG	EL	AA	BB	PHI									
275	0	0	63	84	51	-31	52	-61	57	-119	0	0	-26	-97	31	-58	51	-148	10	101	13	1	16	-118	9	-116	23	16	68	5	0
275	0	4	61	89	50	-29	54	-59	59	-116	0	0	-28	-97	30	-60	49	-146	8	102	11	1	13	-119	7	-116	23	16	68	5	0
275	0	9	59	91	48	-28	56	-57	60	-113	0	0	-30	-96	30	-63	47	-145	7	104	9	1	11	-120	5	-116	23	16	68	5	0
275	0	14	57	93	46	-27	58	-56	61	-110	0	0	-32	-96	29	-66	45	-144	5	105	7	1	9	-121	2	-116	23	16	69	5	0
275	0	19	55	96	44	-25	61	-54	62	-106	0	0	-34	-96	28	-68	43	-143	3	106	4	1	7	-122	0	-116	23	16	69	5	0
275	0	24	53	98	42	-25	63	-52	62	-102	0	0	-36	-95	27	-71	41	-142	1	108	2	1	5	-123	-1	-116	23	16	69	5	0
275	0	29	51	101	40	-24	65	-49	63	-98	0	0	-38	-95	26	-73	39	-141	0	0	0	1	3	-124	-3	-116	23	22	311	4	0
275	0	34	48	103	38	-23	67	-47	63	-93	0	0	-40	-94	25	-75	37	-140	0	0	-1	1	1	-125	-6	-116	23	22	292	4	0
275	0	39	46	105	36	-23	70	-44	63	-89	0	0	-42	-93	23	-78	35	-140	0	0	-4	0	0	0	-8	-117	88	22	64	3	2
275	0	44	44	107	34	-22	72	-41	63	-85	0	0	-44	-92	22	-80	33	-139	0	0	-6	0	0	0	-10	-117	81	22	65	3	2
275	0	49	42	109	32	-22	74	-38	63	-80	0	0	-46	-91	20	-82	31	-139	0	0	-8	0	0	0	-12	-117	75	22	65	3	2
275	0	54	41	111	30	-22	77	-34	62	-76	0	0	-48	-90	19	-84	29	-139	0	0	-10	0	0	0	-14	-117	71	21	66	3	2
275	0	59	37	113	27	-21	79	-28	61	-73	0	0	-50	-89	17	-85	27	-139	0	0	-13	0	0	0	-17	-117	67	21	66	3	2
275	1	4	35	114	25	-21	81	-26	60	-69	0	0	-52	-87	15	-87	24	-139	0	0	-15	0	0	0	-19	-117	64	21	67	3	2
275	1	9	33	116	23	-21	83	-24	59	-66	0	0	-53	-85	13	-89	22	-138	0	0	-17	0	0	0	-21	-117	62	21	67	3	2
275	1	14	31	118	21	-21	85	-22	58	-63	0	0	-55	-83	12	-90	20	-138	0	0	-19	0	0	0	-23	-117	61	21	67	3	2
275	1	19	29	119	19	-21	85	-20	57	-60	0	0	-56	-81	10	-92	18	-138	0	0	-21	0	0	0	-25	-117	60	20	68	3	2
275	1	24	27	121	16	-21	85	-18	55	-58	0	0	-58	-78	8	-93	15	-138	0	0	-24	0	0	0	-27	-116	59	20	68	3	2
275	1	29	25	122	14	-21	83	-16	53	-56	0	0	-59	-75	6	-95	13	-139	0	0	-26	0	0	0	-30	-116	59	20	68	3	2
275	1	34	22	124	12	-21	81	-14	52	-54	0	0	-60	-72	4	-96	11	-139	0	0	-28	0	0	0	-32	-116	59	20	68	3	2

