

SPLINE SMOOTHING OF TWO-DIMENSIONAL DATA SERIES WITH PRECISION ESTIMATION APPLIED TO SATELLITE NAVIGATION

SEE HEAN QUEK

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PREFACE

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March, 1983

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ABSTRACT

Noisy two-dimensional data series are a common occurrence in the geodetic field. As a result of this, numerous algorithms have been formulated to separate the systematic components from the noise within the observed data series. These algorithms, however, are not applicable to all types of data series. In this thesis, the performance of the piecewise cubic function, as a means of smoothing such data series, is investigated.

Cubic splines have, in the past, been used as smoothing algorithms. However, they proved ineffective in dealing with two-dimensional data series as they were developed with a weighting scheme for only one of the two variables. Hence they cannot accept a fully populated covariance matrix associated with each observed data point. The spline algorithm developed in this thesis uses both parameterized cubic splines and the method of least-squares to formulate a weighting scheme which allows the incorporation of the two-dimensional covariance matrices of the observations.

The resulting spline approximation technique is then used to smooth the navigation data sets of the three ice camps of the Lomonosov Ridge Experiment (LOREX) in the vicinity of the North Pole in 1979. The Navy Navigation Satellite

System (Transit) was used as the primary positioning system. Error models evaluating the accuracy of the position fixes using Transit satellites at high latitudes are developed. Smoothed positions and velocities for the three ice camps at one hour intervals are computed for the duration of the expedition.

To evaluate the performance of the spline algorithm, the smoothed data series produced by the spline algorithm (DSPLIN) and the real-time smoothing technique (SMOBS) used during LOREX are compared with those generated by the precise dynamic package (GEODOP), i.e. DSPLIN versus GEODOP and SMOBS versus GEODOP. The smoothed data series produced by the precise dynamic technique (GEODOP) are hence used as a reference standard. In the comparisons between the smoothed data series of positions and velocities for the three ice camps, a reduction of about 56 and 47 percent in the root mean square of the differences in position and velocity respectively, is achieved by DSPLIN over SMOBS. In the same comparisons, the maximum discrepancy between individual smoothed positions is reduced by about one-half (i.e. from 3758 m to 1564 m). The computed standardised position differences between the smoothed positions produced by the spline algorithm and the precise dynamic technique shows that the precision estimates computed by the spline algorithm are consistent with accuracy only over certain periods of time in the LOREX data spans.

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



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NOTATION

$:=$	equal by definition
ϵ	$:=$ belongs to
\subset	$:=$ subset
\cap	$:=$ intersection
$s(x)$	$:=$ polynomial function
s^n	$:=$ n th derivative of function s
$\langle a, b \rangle$	$:=$ closed interval: $a \leq x \leq b$
S_k	$:=$ Spline Space of degree k
P_k	$:=$ Polynomial Space of degree k
$C^n \langle a, b \rangle$	$:=$ Space of n th differentially continuous functions

SYMBOLS

	$:=$ data point
	$:=$ knot point
	$:=$ confidence ellipse
	$:=$ spline

In general

1. Matrices and vectors are underlined (e.g. A and x).
2. Matrices are denoted by upper case letters (e.g. A).
3. Vectors are denoted by in lower case letters (e.g. x).

Chapter 1
INTRODUCTION

The purpose of this investigation is to develop a smoothing algorithm applicable to noisy two-dimensional data series. The resulting algorithm incorporates the full covariance matrix depicting the accuracy of the data in its smoothing process.

Such data sets are a common occurrence in the geodetic field. They can be found in marine navigation; for example, the time series of position determinations using modern electronic devices to monitor the motion of a ship at sea. A specific example, which is later used to test the smoothing algorithm, is the Lomonosov Ridge Experiment (code-named LOREX) station navigation Doppler data set. The positioning of the LOREX ice stations in the vicinity of the North Pole was achieved using the Navy Navigation Satellite System (NNSS). Due to proximity to the pole, position determinations were greatly influenced by poor geometry and inadequate modelling of the ice motion. It was felt that an algorithm which is able to utilize all the information contained in the position fixes will greatly increase the accuracy of the predicted locations of the observing stations between position determinations.

A recomputation of all position fixes using better station velocity estimates will remove the errors caused by inadequate modelling of the ice motion. In this thesis, error models are used to account for these errors in the LOREX position fixes. A recomputation of all position fixes with better velocity estimates is outside the scope of this research.

1.1 MAIN CONTRIBUTIONS

The following are the main contributions of this thesis:

1. The development of a two-dimensional least-squares cubic spline approximation algorithm.
2. The evaluation of the performance of the spline algorithm using simulated and actual data sets.
3. The application of the spline algorithm to the navigation data sets of the three LOREX ice camps.
4. The modelling of positioning errors, caused by satellite orbital, station velocity and station height errors, through the a priori covariance matrix of the position computations.

1.2 OUTLINE OF THESIS

This thesis is divided into the following chapters.

Chapter 2 contains a brief description of the LOREX-79 expedition, the navigation equipment used and the accuracy of position determinations. This information provides a background for the discussion and assessment of the results from the processing of the navigation data sets using the developed smoothing algorithm.

Chapter 3 presents a brief overview of the scope of the investigation and details several of the options that were considered when designing the smoothing algorithm.

Chapter 4 gives a basic review of the concept of a spline and its similarities with the mechanical spline.

Chapters 5 and 6 are devoted to the formulation of the working equations of the least-squares parametric cubic spline approximation.

Chapter 7 discusses the various possible methods of adjustment; the merits and implication of each in relation to the spline algorithm.

Chapter 8 deals with the aspect of precision estimation of the least-squares estimates, the covariance law and computational accuracy.

Chapter 9 gives an overview into the various tests done to assess the performance of the spline algorithm with regard to the simulated and LOREX test data sets.

Chapter 10 discusses and evaluates the LOREX Doppler data sets and the application of the spline algorithm to the complete navigation data series of the three ice stations on LOREX. Various error models, based on the formal covariance matrix of the position determinations, are used to develop a weighting scheme suitable for high latitude positioning by NNSS. The real-time application of the spline algorithm is also addressed.

Finally, in Chapter 11 a summary of the discussions are given, conclusions drawn and recommendations made.

Chapter 2

DESCRIPTION OF LOREX-79 NAVIGATION DOPPLER DATA SET

In this chapter, a brief description of the LOREX-79 expedition together with the navigation equipment used, and the characteristics of the collected Doppler data are given. The on-site and post-processing of the data series are discussed and inadequacies noted.

2.1 LOREX DATA CHARACTERISTICS

In the spring of 1979, the Earth Physics Branch of the Federal Department of Energy, Mines and Resources in conjunction with the Polar Continental Shelf Project organised an expedition to the geographical North Pole. The Lomonosov Ridge Experiment was designed to explore the nature and origin of the major submarine mountain ridge running across the Arctic Ocean between Greenland and Siberia.

During the expedition, three camps were established on the Arctic ice. Main Camp (S0), Snowsnake (S1) and Iceman (S2) were laid out in an approximate isosceles triangle with sides of about 60 kilometres long and a base of about 100 kilometres.

Canadian Marconi 722B Transit receivers were deployed for positioning the camps. The receiver at the Main Camp was interfaced to a HP 2100 minicomputer, under the RTE II operating system with a HP 7900A Megabyte disc drive, 7-track magnetic tape, plotter and two terminal peripherals. In the off-line mode, it was linked to a CMA 749 magnetic tape cassette unit which allowed the recording of Doppler counts to a resolution of 0.01 of a Doppler count. This, due to the inherent characteristics of the navigation system, is two orders of magnitude better than the on-line tracking mode. Receivers at Snowsnake and Iceman operated unattended, in the automatic data acquisition mode. Gaps, which were later found in the collected data at these two stations, were attributed to failure of the operator to change the data cassettes when full, and signal loss at point of closest approach of the satellite because of the tracking antenna's gain pattern [Popelar et al. 1981].

The monitoring of Arctic ice drift using polar orbiting NNSS satellites has several drawbacks. Firstly, due to the high latitudes, there are many more passes than at southern latitudes and with an omni-directional antenna, severe interference problems arise. The effect of interference results in acquisition of fewer passes with the complete set of Doppler information unless the receiver is programmed to reject some passes in favour of others. Programmed response was not even possible at the Main Camp due to hardware

restrictions [Wells and Popelar 1979] and the 20 percent higher tracking efficiency at the Main Camp was attributed to manual intervention [Popelar et al. 1981].

Secondly, with polar orbiting satellites, passes at high latitudes tend to be nearly overhead. Overhead passes produce geometrically poorer cross track position fixes than non-overhead passes. Position determinations using high elevation satellites hence have very elongated error ellipses. The semi-major axis of the error ellipses are in the cross track direction of the passing satellite.

These inherent system difficulties are further complicated by the erratic behaviour of the motion of the ice platform. The ice motion changes both speed and direction, depending on the combined effects of the wind, temperature, and sea currents.

The amassed Doppler data from the three stations were processed on-site and later reprocessed in Ottawa [Popelar et al. 1981].

The satellite fix software package BIONAV [Wells and Grant 1981] was deployed on LOREX to provide position fixes for the ice stations in real time. The positions were computed in the Stereographic Coordinate System and on the International Ellipsoid. An arbitrary rejection criterion, as opposed to a statistical one, of 1000 metres on the formal standard deviations of the position determinations was used. Accepted passes were computed and stored for further processing.

2.2 LOREX DATA POST-PROCESSING

The LOREX data has been post-processed using four different methods, one of which is the subject of this thesis. The first two techniques mentioned below were used on-site at LOREX to smooth the raw fixes.

A one-dimensional least-squares cubic spline approximation (program SMOBS), using the inverse of the trace of the formal covariance matrix derived from the fix computation as weights (equation 4.3), was performed on moving sets of fixes over time periods depending on the character of the station's motion and the number of satellite fixes available. The weighting scheme used is further discussed in Section 4.2. Of a moving set of 70 passes, 50 smoothed central position fixes were accepted. The Lagrange polynomial interpolant was then used to predict the position of the station between smoothed fixes [Wells and Popelar 1979] as SMOBS does not compute the cubic coefficients needed for interpolation. The velocities and associated standard deviations of the ice stations were computed from six preceding one-hour smoothed coordinate differences. A list of positions and velocities produced by SMOBS can be found in Appendix A of Popelar et al. [1981].

In addition to the on-site cubic spline smoothing, a Kalman filter routine using covariance matrices to model measurement errors and perturbations in the ice motion, was used to sequentially process the Doppler data [Wells and Popelar 1979].

The two on-site smoothing techniques that were used had their disadvantages. The cubic spline approximation technique used weighted both coordinates equally and totally ignored the correlation between errors in the coordinates (which was above 0.9 for 80 percent of the passes). The Kalman filter algorithm could be successfully applied only if the filter could be tuned in accordance to the ice motion noise [Wells and Popelar 1979].

In an effort to improve position determinations in the post-processing of the data, a precise geodetic positioning software package (GEODOP) was extensively modified to accommodate sequential simultaneous positioning of slowly moving stations with constant velocity vectors over a three-hour time period. It uses both higher order modelling of environmental and instrumental effects to reflect the time and space correlation of model parameters during simultaneous satellite tracking from several stations and post-fitted precise satellite orbits. The mean station positions were obtained from a series of satellite position fixes, weighted by their formal covariance matrix, within the three-hour time interval. Station velocities were derived from consecutive mean positions [Popelar et al. 1981].

In this thesis, the acronym "GEODOP" will henceforth be used to denote the modified precise dynamic positioning software package. Of the four post-processing techniques,

GEODOP is the only one which does a recomputation of the individual satellite position fixes using better station velocity estimates.

Unlike the spline algorithm used on LOREX, the spline algorithm developed in this thesis (program DSPLIN) is capable of using the full covariance matrix associated with each position fix. This technique is hence able to extract all the information contained in the position determinations. In order to assess the performance of DSPLIN, the LOREX navigation data sets are used and the GEODOP solution adopted as reference standard. The agreement between DSPLIN and GEODOP smoothed values is evaluated and is shown to be better than the agreement between SMOBS and GEODOP.

Chapter 3

CONSIDERED ALTERNATIVE ALGORITHMS

In this chapter, the characteristics of a noisy data set are outlined, the area of investigation given, the alternatives discussed and the reasons for using the spline approach stated. The discussions of the considered possible alternatives for the design of the new smoothing algorithm are a minor digression from the main theme of this thesis. However, they are given here to indicate the scope and area of investigation from which the new smoothing spline algorithm evolved.

The approximating function to be developed must be able to smooth data series with the following characteristics:

1. Unequal data intervals.

The data points within the given data series are unequally spaced in either time or space.

2. Non-predictive (or non-analytic) data series.

The external factors governing or generating the data series cannot be effectively modelled or are rapidly changing in time or space.

3. Fully populated data covariance matrices.

Each data point within the data series has an associated covariance matrix depicting the two-dimensional accuracy of the observed data point.

In addition to the above, the technique must be able to provide a data series of smoothed data points with reliability estimates.

Research into the new smoothing algorithm centered around the concept of extracting existing ideas in the physical world and trying to relate or apply them as smoothing algorithms. The following were examined in this thesis.

3.1 TWO-DIMENSIONAL LEAST-SQUARES CUBIC SPLINE

The mathematical spline which "imitates" the mechanical spline has several properties conducive to its use as a smoothing device. Current development [Spath 1974; Boor 1978], of the cubic spline only allows the cubic spline to smooth data along one axis at a time and totally ignores any correlation between variables.

However, by incorporating the least-squares principle, the covariance law, and by simultaneously solving two parametric cubic splines, the new spline algorithm is able to satisfy all the stated requirements mentioned above. This concept is developed in greater detail, together with a short review of splines, in Chapter 4.

3.2 HAMILTONIAN PRINCIPLE OF LEAST ACTION

The proposed concept here is the utilization of the Lagrangian equations of motion with the Hamiltonian Principle of Least Action [Landau and Lifshitz 1976] to solve for the motion of a particle moving in a non-symmetric cluster of finite particles. Disregarding the mass of the sensing particle, the attracted particle moves according to the sum of all forces generated by the other forcing particles in that cluster [Vanicek 1973]. The interrelationship between the law of gravitational attraction and the conservation of momentum leads to the fact that both velocity and displacement of the particle are smooth functions of time. Under the kinematic approach, the generated force field can be thought of as a non-symmetric potential field and by maintaining a closed system with non-time varying elements of potential, a stationary or conservative potential or force field is said to exist.

By portraying the data series as that of the motion of the particle and the observed data points as gravity-generating mass bodies, a smooth path depicting the data series can hence be generated. By solving the equations of motion of the massless particle, the velocity and position of the particle can be obtained at any time provided that the velocity and position vectors of the particle at the beginning of the trajectory are defined.

In celestial mechanics, this is termed as the solution of a restricted n-body problem; restricted in that all attracting mass bodies are rigidly fixed and held motionless in Eculidean two-space. Further, the use of "relativistic directional masses" as the mass bodies allows the incorporation of error ellipses.

3.3 HEISENBERG PRINCIPLE OF UNCERTAINTY

The concepts of velocity and energy which stem from simple observations of common objects have been applied to certain fundamental experiments in atomic physics.

The position of an electron is known only to a certain degree of accuracy and at any time can be visualized as a wave packet in the proper position with an approximate extension.

The term "wave packet" [Heisenberg 1930] is used to denote a wave-like disturbance whose amplitude differs appreciably from zero only in a bounded region. This region, in general, is in motion and changes in shape and size. The laws of optics and that of the conservation of momentum, can be used to obtain a relationship between the uncertainty in velocity and position; the product is bounded by a certain (Planck's) constant.

This fact bears a striking resemblance to the position of a data point within a data series. The uncertainty of the

data point can only be represented by a covariance matrix, much like the wave packet. The probability of the wave packet grows larger from the last observed data point until the next observation.

Using such a representation, the motion of the data point can be represented and reliability estimates obtained for predicted points.

3.4 INTERLACING WIRE AND SLOT REPRESENTATION

A time series of two-dimensional data can be thought of as points in a geometric space defined by three orthogonal vectors. In relation to navigational data, two of the vectors represent the two-dimensional coordinate system of the position while the third is the time axis.

A sequence of time-tagged positions, for example, appears as a series of spatially suspended dots within that space. If the motion is circular, all the dots will lie on the path of a helix.

By interlacing the points with a wire of variable stiffness, points between observations can be predicted. Error ellipses are introduced by replacing the dots or holes with variable size slots. A wire so chosen in its natural state, tries to achieve minimum strain or stress within itself.

For the transformation of the wire to a mathematical tool Frenet formulae and curves are used.

3.5 SELECTION OF TECHNIQUE ADOPTED

An examination of these four proposed smoothing algorithms, revealed that the spline representation seems to be the most promising, easiest to implement, has few variables to contend with (so as not to introduce complex smoothing parameters) and from a practical application point of view satisfies all the requirements of the desired smoothing algorithm.

Chapter 4

BRIEF REVIEW OF SPLINES IN GENERAL

In this chapter, an introduction to the concept of splines is given. The transition from the mechanical spline to its mathematical form is outlined. The topic of smoothing splines contained in the present literature is addressed and differences between those and the smoothing spline algorithm used in this thesis mentioned.

4.1 INTRODUCTION

Polynomials have always played a central role in approximation theory and numerical analysis. Piecewise polynomials, however, had a very limited application due to the existence of discontinuities between polynomial functions. During the past twenty years, piecewise polynomial functions experienced tremendous theoretical advances (e.g. Boor [1978], Shumaker [1981] and Prenter [1975]). Poirer [1973] in his attempt to apply spline functions to econometric data mentions the large gap between theoretical development and practical applications of spline functions.

Currently, spline functions are being applied to smooth noisy geodetic data sets. Their use, however, has been limited to the smoothing of raw data series without obtaining accuracy estimates of either the smoothed data points or the predicted values. A brief exposé on the origin of splines allows better comprehension of the so-called spline functions..

Scheonberg [Shumaker 1981] in 1946 introduced the label "spline" when he observed similarities between piecewise polynomial interpolation and a certain mechanical device called the "spline".

A "spline" is a thin beam of some elastic material equipped with a groove and a set of weights (called either ducks or rats), with attached arms designed to fit into the grooves (see Figure 4-1).

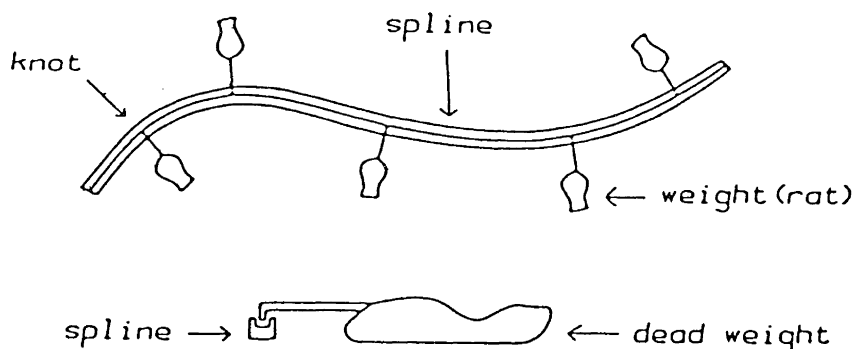


FIGURE 4-1 The Mechanical Spline

These devices are used by architects to draw smooth curves through a set of prescribed points (called in the context of this thesis, data points). To accomplish this, the flexible "spline" is bent in such a manner that it passes through all the points and is held in place by strategically located ducks. Back in the mid-1700's, Euler and the Bernoulli brothers [Shumaker 1981] discovered that the centre-line of the "spline" approximates a given mathematical function (s) which has the following properties:

1. The function (s) is a series of piecewise cubic polynomials between the first and last junction point or knot (knots being analogous to the position of the ducks on the mechanical "spline").
2. The function (s) is linear before the first and after the last knot.
3. The function (s) has continuous first and second derivatives everywhere.
4. The function (s) takes on the value of the data points (i.e. the mechanical spline is an interpolation device).

Given the location of the knots and the data points, these properties define a unique function (s) . No assumption, at this stage, is made with regard to the location of the knots amongst the data points. However it should be

noted that the knots may or may not be coincident with the position of the data points. This simple but effective analogue of the mathematical spline underlies the fundamental concept of splines in general.

4.2 THE MATHEMATICAL SPLINE

In this section, the properties of the mathematical spline are stated. Reasons for using the piecewise cubic function, along with the current limitations of splines are given. An extension of the use of splines from the current literature is made.

The mathematical spline (s) of degree k is an element of the Spline Space (S) which on a closed interval $\langle a, b \rangle$ can be written as:

$$s_k \in S_k \subset [P_k \cap C^n \langle a, b \rangle] \quad - (4.1)$$

where P_k := Polynomial Space containing k th degree polynomials; a subspace of the total Polynomial Space,

$C^n \langle a, b \rangle$:= Space of n th differentially continuous functions on the closed interval $\langle a, b \rangle$,

and $n \leq k - 1$.

Any function (s) so defined on a set of points (u_j, v_j) , $j = 1, \dots, m$ will hence have the following properties:

1. It is continuous at u_1, u_2, \dots, u_m and
with $s(u_j) = v_j$.

2. The first $k-1$ derivatives of the spline functions, (i.e. $s'(u), s''(u), \dots, s^{(k-1)}(u)$) exist and are continuous within the closed interval $\langle a, b \rangle$ on which the spline function is defined.

It becomes apparent that the mathematical spline defined in Section 4.1 is of the form:

$$s_3 \in S_{3,t} \subset [p_{3,t} \cap C^2 \langle a, b \rangle] \quad - (4.2)$$

with $t_j, j = 1, \dots, m$ being the knot sequence.

Cubic splines as in (4.2) are the most popular splines for two reasons. The first is that the human eye has increasing difficulty in detecting jumps in the derivatives of a function as the order of the derivative increases. Discontinuities in the first and second derivatives can be detected, but the eye has great difficulty in detecting jumps in derivatives of order greater than two. Hence a function with only second order derivative continuity will appear smooth to the human eye. The second reason is that there exist distinct disadvantages in using higher degree polynomial functions. The higher the degree, the greater is the evaluation cost of the parameters defining the spline. In addition, individual oscillations of the polynomials generally increase with the degree. Hence the cubic spline combines the advantages of smaller oscillations, modest evaluation cost and second derivative continuity.

The simple one-dimensional interpolating cubic spline, in the context of this research, has several major defects:

1. At least one of the variables has to increase monotonically.
2. It is confined to point estimation between knots or data points.
3. It does not allow for the incorporation of differently weighted data points.
4. No precision estimation of predicted points between data points is possible.

To overcome the first problem, the spline is computed against a third variable (t) which has the property of being always monotonically increasing. For a given set of points (x,y) , the parametric spline [Spath 1974] is computed on data sets (x,t) and (y,t) ; with t monotonically increasing and is related functionally or otherwise to the data points (x,y) . A discussion of possible types of variable (t) can be found in Spath [1974]: page 60.

No assumptions have yet been made about the number of knots with respect to a given set of data points. When the number of knots is equal to the number of data points, the spline interpolates between the data points. The transition (which is further discussed in Chapter 5) from an interpolating to an approximating spline is through the incorporation of additional data points in the solution of the parameters defining the spline function. However,

additional information is required if a unique approximating spline function is to exist. This additional information takes the form of a weighting scheme amongst the data points; some of which are of an arbitrary nature (e.g. Spath [1974]: page 106) whilst others, being more rigorous (e.g. Boor [1978]: page 235) rely on the minimisation of a specified variational function.

Wells and Popelar [1979] on the LOREX expedition utilized, in near real-time, parametric cubic splines minimising the differences between smoothed and observed positions to smooth the satellite positioning data (x,y). The cubic spline, mentioned earlier in Section 2.2, was computed first in x against time and then in y against time, using the inverse of the trace of the formal covariance matrix obtained from the satellite fix computations, as weights for both splines, i.e.

$$w_i := 1/(\sigma_1^2 + \sigma_2^2)^{1/2} \quad - (4.3)$$

where i := computed fix number,

w_i := designated weight for the i th computed coordinates,

σ_1^2 and σ_2^2 := diagonal elements of the formal covariance matrix associated with the i th computed position.

The formal covariance matrix associated with each fix is of the form

$$\begin{bmatrix} \sigma_1^2 & \sigma_{12} \\ \sigma_{12} & \sigma_2^2 \end{bmatrix}$$

and it portrays the two-dimensional precision of the computed coordinates. The variances of the individual coordinates are denoted by σ_1^2 and σ_2^2 , and the correlation (or covariance) between the two determined coordinates by σ_{12} .

The weighting scheme used on LOREX was rather arbitrary as an operator-specified "coefficient of roughness" was used to scale the assigned weights computed via equation (4.3) to achieve different degrees of smoothness. The high correlation between the two position coordinates was totally ignored. In addition no precision estimates for the individual predicted points between observed positions were available.

The spline algorithm developed in this thesis has been primarily designed to overcome these deficiencies of previous smoothing splines. The full covariance matrices of the data points are utilized in the simultaneous computation of two parametric cubic splines against a third variable, time. Through the method of least squares, it is possible to obtain least-squares estimates and an associated covariance matrix for the parameters defining the spline. The covariance law is also used to derive precision estimates for the predicted data points.

Chapter 5

DEVELOPMENT OF THE PARAMETRIC CUBIC SPLINE

In this chapter, the aspect of base functions for the spline is addressed, the transition from the simple cubic spline to the parametric cubic spline is described and the working equations are given.

Using the concepts embodied in Chapter 4, the cubic spline (s) is hence defined on a set of points (x_i, y_i, t_i) , $i = 1, \dots, m$ for which $s_x(t_i) = x_i$ and $s_y(t_i) = y_i$, and is a composite function with $2(m-1)$ cubic polynomials. Further, the function (s) is twice differentiable with respect to the variable (t), for $t \in \langle t_0, t_m \rangle$.

5.1 DEFINITION OF BASE FUNCTIONS

The precise definition of the base functions ϕ_ℓ , $\ell = 1, \dots, 4$ in the piecewise polynomial function

$$s(t) := \sum_{\ell=1}^4 \alpha_\ell \phi_\ell(t)$$

of the cubic spline has yet to be mentioned. In actuality, there are numerous possible definitions and alternatives. The so-called "generalised cubic splines" [Spath 1974: page

124] utilizes complicated base functions. The two conditions [Spath 1974: page 58] that the base functions of the cubic spline have to satisfy are:

1. The resulting polynomial is a cubic function.
2. The transformation between coefficients and knot vectors must exist (i.e. the equations in Section 5.2 can be formulated).

The use of more complex bases than those given below complicates the formulation and increases computational cost. This is in addition to the fact that smoother splines are obtained from the usual cubic spline than other more complex cubic splines without constraints [Spath 1974]. Hence in this research, a simple set of base functions are used (i.e. $1, \Delta t, (\Delta t)^2$ and $(\Delta t)^3$: Δt being the time interval between knots).

5.2 PARAMETRIC CUBIC SPLINE

On a given set of knots (x_j, y_j, t_j) , $j = 1, \dots, m$ the j th piecewise cubic polynomial is thus defined:

$$s_{xj}(t) := a_{j1} + \sum_{\ell=2}^4 a_{j\ell} (t-t_j)^{\ell-1}$$

$$s_{yj}(t) := b_{j1} + \sum_{\ell=2}^4 b_{j\ell} (t-t_j)^{\ell-1}$$

- (5.1)

with $s_{xj}(t_j) = x_j$

and $s_{yj}(t_j) = y_j$

and $t_j \leq t \leq t_{j+1}$

Note that $a_{j\ell}$ and $b_{j\ell}$ are the elements of the coefficient vectors $(\underline{a}_j, \underline{b}_j)$ of the two cubic polynomials of the spline.

The functional relationship between the given knots and the cubic coefficients, i.e. the boundary values, can be expressed as follows:

$$x_j := s_{xj}(t_j) = a_{j1} \quad - (5.2a)$$

$$y_j := s_{yj}(t_j) = b_{j1} \quad - (5.2b)$$

$$x_{j+1} := s_{xj}(t_{j+1}) = a_{j1} + \sum_{\ell=2}^4 a_{j\ell} (t_{j+1} - t_j)^{\ell-1} \quad - (5.2c)$$

$$y_{j+1} := s_{yj}(t_{j+1}) = b_{j1} + \sum_{\ell=2}^4 b_{j\ell} (t_{j+1} - t_j)^{\ell-1} \quad - (5.2d)$$

$$x'_j := s'_{xj}(t_j) = a_{j2} \quad - (5.2e)$$

$$y'_j := s'_{yj}(t_j) = b_{j2} \quad - (5.2f)$$

$$x'_{j+1} := s'_{xj}(t_{j+1}) = a_{j2} + \sum_{\ell=3}^4 (\ell-1)a_{j\ell} (t_{j+1} - t_j)^{\ell-2} \quad - (5.2g)$$

$$y'_{j+1} := s'_{yj}(t_{j+1}) = b_{j2} + \sum_{\ell=3}^4 (\ell-1)b_{j\ell} (t_{j+1} - t_j)^{\ell-2} \quad - (5.2h)$$

$$x''_j := s''_{xj} = 2a_{j3} \quad - (5.2i)$$

$$y''_j := s''_{yj} = 2b_{j3} \quad - (5.2j)$$

$$x''_{j+1} := s''_{xj} = 2a_{j3} + 6a_{j4}(t_{j+1} - t_j) \quad - (5.2k)$$

$$y''_{j+1} := s''_{yj} = 2b_{j3} + 6b_{j4}(t_{j+1} - t_j) \quad - (5.2l)$$

There is a choice of expressions with regard to the explicit form of the coefficient vectors \underline{a} and \underline{b} . They can be expressed either in terms of their functional values (i.e. equations 5.2a to 5.2d) and their first derivatives (i.e. equations 5.2e to 5.2h) or their functional values (i.e. equations 5.2a to 5.2d) and their second derivatives (i.e. equations 5.2e to 5.2l) [Spath 1974; Boor 1978].

Parameters of functional values and first derivatives are used here to represent the knots on the assumption that the positions and velocities, taking navigational data as an example, are easier to visualize than positions and accelerations.

Inverting equations 5.2a to 5.2h,

$$a_{j1} = x_j \quad - (5.3a)$$

$$a_{j2} = x'_j \quad - (5.3b)$$

$$a_{j3} = 3(x_{j+1} - x_j)/\Delta t_j^2 - (2x'_j + x'_{j+1})/\Delta t_j \quad - (5.3c)$$

$$a_{j4} = [-2(x_{j+1} - x_j)/\Delta t_j + x'_j + x'_{j+1}]/\Delta t_j^2 \quad - (5.3d)$$

$$b_{j1} = y_j \quad - (5.3e)$$

$$b_{j2} = y'_j \quad - (5.3f)$$

$$b_{j3} = 3(y_{j+1} - y_j)/\Delta t_j^2 - (2y'_j + y'_{j+1})/\Delta t_j \quad - (5.3g)$$

$$b_{j4} = [-2(y_{j+1} - y_j)/\Delta t_j + y'_j + y'_{j+1}]/\Delta t_j^2 \quad - (5.3h)$$

with $\Delta t_j := t_{j+1} - t_j$

Hence there exist a total of eight elements, four in each of the two coefficient vectors, \underline{a}_j and \underline{b}_j , for each interval $\langle t_j, t_{j+1} \rangle$ defining the cubics.

To ensure that adjacent piecewise cubics are continuous, constraint relationships are enforced. Considering the junction point between the j th and $(j+1)$ th interval, second derivative continuity is achieved by the following equations:

From equations 5.2i to 5.2l,

$$6a_{j4} \Delta t_j + 2a_{j3} = 2a_{j+1,3}$$

and
$$6b_{j4} \Delta t_j + 2b_{j3} = 2b_{j+1,3}$$

- (5.4)

Substituting the respective coefficients for their functional values and derivatives, the following relationships are obtained [Spath 1974: page 46]:

$$\begin{aligned} (1/\Delta t_j)x'_j + 2(1/\Delta t_{j+1} + 1/\Delta t_j)x'_{j+1} + (1/\Delta t_{j+1})x'_{j+2} \\ = 3(x_{j+1}-x_j)/\Delta t_j^2 + 3(x_{j+2}-x_{j+1})/\Delta t_{j+1}^2 \end{aligned}$$

and similarly,

$$\begin{aligned} (1/\Delta t_j)y'_j + 2(1/\Delta t_{j+1} + 1/\Delta t_j)y'_{j+1} + (1/\Delta t_{j+1})y'_{j+2} \\ = 3(y_{j+1}-y_j)/\Delta t_j^2 + 3(y_{j+2}-y_{j+1})/\Delta t_{j+1}^2 \end{aligned}$$

- (5.5)

The working equations developed up to the present chapter are the usual parametric cubic spline equations and they can be used as an interpolating function for any given set of data points.

For m points, there are $2(m-1)$ equations with $2m$ first derivative unknowns. Further information are required to make the set of equations non-singular. These take the form of "boundary" (or "end") conditions. They specify the form which the outer knots will take with respect to themselves or other inner knots.

The choice and type of end conditions affects the performance of the spline. The effect, however, diminishes towards the centre of the data span. For a relatively large data series, a large proportion of the spline remains invariant to the type of boundary conditions chosen.

The transition from the parametric interpolating cubic spline to an approximating spline is discussed in the following chapter.

Chapter 6

LEAST-SQUARES CUBIC SPLINE APPROXIMATION

In this chapter, the cubic spline is transformed to an approximation tool by the incorporation of additional data points between knots. The equations representing an additional point are developed.

Consider an "extra" data point (x^0, y^0) at time t^0 within the j th piecewise cubic interval. Since the point lies on the cubic,

$$\begin{aligned}
 x^0 &:= s_{xj}(t^0) = a_{j1} + \sum_{\ell=2}^4 a_{j\ell} (t^0 - t_j)^{\ell-1} \\
 \text{and } y^0 &:= s_{yj}(t^0) = b_{j1} + \sum_{\ell=2}^4 b_{j\ell} (t^0 - t_j)^{\ell-1}
 \end{aligned}
 \tag{6.1}$$

with $t_j \leq t^0 \leq t_{j+1}$

By substituting the explicit values of the coefficients in terms of the position of the knots (equations 5.3) and first derivatives, the equations (6.1) are transformed to

$$\begin{aligned}
 & [1 + \overline{\Delta t}^2(2\overline{\Delta t}-3)]x_j + \Delta t^0(1-\overline{\Delta t})^2 x_j' \\
 & - \overline{\Delta t}^2(2\overline{\Delta t}-3)x_{j+1} - \Delta t^0 \overline{\Delta t}(1-\overline{\Delta t})x_{j+1}' \\
 & - x^0 = 0
 \end{aligned}$$

$$\begin{aligned}
\text{and} \quad & [1 + \overline{\Delta t}^2(2\overline{\Delta t}-3)]y_j + \Delta t^0(1-\overline{\Delta t})^2y'_j \\
& - \overline{\Delta t}^2(2\overline{\Delta t}-3)y_{j+1} - \Delta t^0\overline{\Delta t}(1-\overline{\Delta t})y'_{j+1} \\
& - y^0 = 0 \qquad \qquad \qquad - (6.2)
\end{aligned}$$

$$\text{with } \overline{\Delta t} := \Delta t^0/\Delta t_j$$

$$\Delta t^0 := t^0 - t_j$$

$$\text{and } \Delta t_j := t_{j+1} - t_j$$

Using equations (6.2) (which are termed as observation equations) and those enforcing second derivative continuity (equations 5.4 - termed as constraint equations), the parameters of the least-squares spline can now be determined.

In the transformation from an interpolating to an approximating spline, the value of the knots themselves are treated as unknowns and instead of 2 m first derivative unknowns, the solution vector is expanded to include the functional value of the knots, making a total of 4 m unknowns; m being the number of knots.

There exist several methods of solving this type of least-squares problem with added constraints. The merits of each of the three techniques will be discussed in the following chapter.

Chapter 7

LEAST-SQUARES ADJUSTMENT

In this chapter, three methods of performing a least-squares adjustment with added constraints are evaluated. These are the unified approach, least-squares adjustment through the elimination of constraints, and the method of least squares with constraints. The explicit equations of the latter technique are given.

A least-squares adjustment is performed to derive the best estimates for the unknown parameters. The development of the least-squares method of solution is via the Lagrange method with the covariance law being applied to obtain precision estimates of the computed parameters [Wells and Krakiwsky 1971].

Let the unknown parameters be represented by the vector \underline{x} , and the observed data points by the vector \underline{l} . The two mathematical models that have to be simultaneously satisfied are:

1. The observation (or primary) model (equations 6.1),

$$\underline{f}_1(\underline{x}, \underline{l}) = \underline{0}.$$

2. The constraint (or secondary) model (equations 5.4),

$$\underline{f}_2(\underline{x}) = \underline{0}.$$

There exist several approaches to solving combined models of this nature; the unified approach, the solution via the elimination of constraints, and the functionally constrained least-squares technique.

7.1 UNIFIED APPROACH

With the unified approach [Mikhail 1976], the unknown parameters are also regarded as "observations" or pseudo-observations and the solution here is by the summation of normal equations from the two models above. The constraint pseudo-observables are differently weighted against the observations. By varying the weights for the constraint pseudo-observables, various degrees of satisfaction of the constraint equations are achieved. This seemingly easy treatment has several severe pitfalls [Lawson and Hanson 1974: page 149].

To ensure that the constraint equations are adequately satisfied, heavier weights (i.e. heavier in relation to those of the observations) are placed on the constraint pseudo-observables. However, the constraint equations are, by themselves, singular and the implementation of large weights causes the combined set of normal equations to be ill-conditioned.

Ill-conditioned solutions are undesirable as a loss in precision occurs when computing the inverse and later the

solution vector. One of the prerequisites of the smoothing algorithm is the ability to provide reliability estimates for the estimated parameters (Chapter 3). The assignment of arbitrarily large weights on the constraint pseudo-observables affects the a posteriori covariance matrix for the parameters. The "correct" ratios between the input covariances linked together by a common a priori variance factor presents a difficulty to any one using this method as there exists no physical or geometrical criteria for selecting these ratios.

This technique was used here to verify the feasibility of the new spline algorithm. However it was later discarded as it could not meet the requirements of providing precision estimates for the parameters and hence predicted points (as specified in Chapter 3).

7.2 SOLUTION VIA THE ELIMINATION OF CONSTRAINTS

The constraint equations can be used to solve for, functionally, as many parameters as there are constraints [Mikhail 1976: page 217]. These parameters are then eliminated from the observation model. Hence the total number of unknown parameters is reduced. The remaining parameters are solved for directly by least-squares adjustment. The eliminated parameters are later computed by back substitution.

As this is a rigorous technique, formal covariance matrices are derived for all estimated parameters. A development of this method of solution is included in Appendix I.

The two primary advantages of this method are:

1. a reduced set of unknown parameters are present in the least-squares solution, and
2. the constraint equations are removed from the least-squares solution.

However to successfully apply this method of least-squares estimation, the constraint equations have to be made non-singular; as shown in Appendix I. As mentioned in Chapter 5, the constraint equations can be made non-singular by specifying the end conditions of the spline. The question of developing an algorithm to select the independent parameters, a difficulty expressed by Mikhail [1976]: page 217, does not exist as it will always be the first derivatives that are eliminated.

The predefinition of the end conditions poses as a minor drawback in the use of this technique. The merits of such a step is questionable in light of the fact that, for large data series, it will be required to "join pieces" of splines together. This is due to the length of the data span used for each spline computation being limited by the user's computer memory capacity. The capability of passing on the junction (or knot) vector values is hence desirable if the

data series is to be continuous at the joints. However, with this method of least squares, the end conditions have to be predefined within the algorithm and remain unaltered. To generate a continuous smoothed data series, an overlap of data points between adjacent splines within a data series is required. This uses the property that the effect of the end knot condition diminishes towards the centre of the spline (Section 5.2).

7.3 METHOD OF LEAST SQUARES WITH CONSTRAINTS

Finally, there is a method of least squares with added constraints between unknown parameters [Wells and Krakiwsky 1971: page 142].

The constraints are imbedded into the variational function and strictly (or absolutely) enforced. Primary drawbacks are of a computational nature. For m knots there are two matrices of sizes $4m$ and $2(m-2)$ to be inverted. In addition, the observation model rather than the constraint model must be non-singular (the reverse of that required by the technique described in Section 7.2). In practical terms, this means that there will be a lower limit on the number of data points that must be contained in each cubic interval.

As the spline algorithm is used here as an approximation tool, adequate redundancy to meet this lower limit will be

the usual case. This condition can hence be easily adhered to or algorithmically checked and enforced (e.g. by subroutine CHECK in Appendix VII).

7.3.1 Derivation of the Functionally Constrained Model

In this section, a brief development of the method of least squares used in the algorithm is described and the working equations are given.

There are, as mentioned earlier in this chapter, two mathematical models present in the adjustment:

the observation model,

$$\underline{f}_1(\underline{x}, \underline{l}) = \underline{0}$$

and the constraint model,

$$\underline{f}_2(\underline{x}) = \underline{0}$$

- (7.1)

with \underline{x} vector representing the value and first derivative unknowns of the knots,
 \underline{l} vector containing the observed data points,

and
$$\underline{x} = \underline{x}^0 + \underline{\delta}$$

$$\underline{l} = \underline{l}^0 + \underline{v} .$$

The observation vector, \underline{l}^0 , has a full weight matrix, $\underline{P} := \sigma_0^2 \underline{\Sigma} \underline{l}^0$ ($\underline{\Sigma} \underline{l}^0$ being the a priori covariance matrix of the observations).

Using Taylor's expansion, equations (7.1) are expanded about the initial approximation, \underline{x}^0 and the observed values, \underline{l}^0 ,

i.e.

$$\underline{f}_1(\underline{x}, \underline{l}) \doteq \underline{f}_1(\underline{x}^0, \underline{l}^0) + \frac{\partial \underline{f}_1}{\partial \underline{x}} \bigg|_{\underline{x}^0, \underline{l}^0} \underline{\delta} + \frac{\partial \underline{f}_1}{\partial \underline{l}} \bigg|_{\underline{x}^0, \underline{l}^0} \underline{v} = \underline{0}$$

and

$$\underline{f}_2(\underline{x}) \doteq \underline{f}_2(\underline{x}^0) + \frac{\partial \underline{f}_2}{\partial \underline{x}} \bigg|_{\underline{x}^0} \underline{\delta} = \underline{0}$$

- (7.2)

where $\underline{f}_1(\underline{x}^0, \underline{l}^0)$ and $\underline{f}_2(\underline{x}^0)$ are the misclosure vectors.

Rewriting,

$$\underline{w}_1 + \underline{A}_1 \underline{\delta} + \underline{Bv} = \underline{0}$$

$$\underline{w}_2 + \underline{A}_2 \underline{\delta} = \underline{0}$$

where $\underline{w}_1 := \underline{f}_1(\underline{x}^0, \underline{l}^0)$

$$\underline{w}_2 := \underline{f}_2(\underline{x}^0)$$

- (7.3)

and the design matrices,

$$\underline{A}_1 := \frac{\partial \underline{f}_1}{\partial \underline{x}} \bigg|_{\underline{x}^0, \underline{l}^0}, \quad \underline{A}_2 := \frac{\partial \underline{f}_2}{\partial \underline{x}} \bigg|_{\underline{x}^0} \quad \text{and} \quad \underline{B} := \frac{\partial \underline{f}_1}{\partial \underline{l}} \bigg|_{\underline{x}^0, \underline{l}^0}$$

In hyper-matrix notation,

$$\begin{bmatrix} \underline{w}_1 \\ \underline{w}_2 \end{bmatrix} + \begin{bmatrix} \underline{A}_1 \\ \underline{A}_2 \end{bmatrix} \underline{\delta} + \begin{bmatrix} \underline{B} & \underline{0} \\ \underline{0} & \underline{0} \end{bmatrix} \underline{v} = \underline{0}$$

- (7.4)

(Equation (7.4) is equivalent to the partitioning of the design matrix \underline{A} , and the misclosure vector \underline{w} , in the direct least-squares model of $\underline{A}\underline{\delta} + \underline{Bv} + \underline{w} = \underline{0}$).

The least-squares solution is then derived by minimising the variational function ϕ , where

$$\phi := \underline{\hat{v}}^T \underline{P} \underline{\hat{v}} + \underline{\hat{k}}_1^T (\underline{w}_1 + \underline{A}_1 \underline{\hat{\delta}} + \underline{Bv}) + \underline{\hat{k}}_2^T (\underline{w}_2 + \underline{A}_2 \underline{\hat{\delta}}) \quad - (7.5)$$

with $\underline{\hat{k}}_1$ and $\underline{\hat{k}}_2$ being the estimates for the Lagrange multipliers. (The '^' symbol denotes least-squares estimates of their true values).

$$\text{For minima, } \frac{\partial \phi}{\partial \underline{\hat{v}}} = \frac{\partial \phi}{\partial \underline{\hat{\delta}}} = 0.$$

$$\text{or } \underline{P} \underline{\hat{v}} + \underline{B}^T \underline{\hat{k}}_1 = \underline{0}$$

$$\text{and } \underline{A}_1^T \underline{\hat{k}}_1 + \underline{A}_2^T \underline{\hat{k}}_2 = \underline{0}$$

- (7.6)

Combining equations (7.4) and (7.6), the set of normal equations is thus formulated.

$$\begin{bmatrix} \underline{P} & \underline{B}^T & \underline{0} & \underline{0} \\ \underline{B} & \underline{0} & \underline{A}_1 & \underline{0} \\ \underline{0} & \underline{A}_1^T & \underline{0} & \underline{A}_2^T \\ \underline{0} & \underline{0} & \underline{A}_2 & \underline{0} \end{bmatrix} \begin{bmatrix} \underline{\hat{v}} \\ \underline{\hat{k}}_1 \\ \underline{\hat{\delta}} \\ \underline{\hat{k}}_2 \end{bmatrix} + \begin{bmatrix} \underline{0} \\ \underline{w}_1 \\ \underline{0} \\ \underline{w}_2 \end{bmatrix} = \underline{0}$$

- (7.7)

By the process of elimination of variables, followed by back substitution of functionally solved parameters, the following explicit expressions are derived.

$$\begin{aligned}
\hat{\underline{\delta}} &= - (\underline{A}_1^T \underline{M}^{-1} \underline{A}_1)^{-1} (\underline{A}_2^T \hat{\underline{k}}_2 + \underline{A}_1^T \underline{M}^{-1} \underline{w}_1) \\
\hat{\underline{k}}_2 &= (\underline{A}_2 (\underline{A}_1^T \underline{M}^{-1} \underline{A}_1)^{-1} \underline{A}_2^T)^{-1} [\underline{w}_2 - \underline{A}_2 (\underline{A}_1^T \underline{M}^{-1} \underline{A}_1)^{-1} \underline{A}_1^T \underline{M}^{-1} \underline{w}_1] \\
\hat{\underline{k}}_1 &= \underline{M}^{-1} (\underline{A}_1 \hat{\underline{\delta}} + \underline{w}_1) \\
\hat{\underline{v}} &= - \underline{P}^{-1} \underline{B}^T \hat{\underline{k}}_1 \\
\hat{\sigma}_0 &= \underline{v}^T \underline{P} \underline{v} / \gamma
\end{aligned}$$

where $\underline{M} = \underline{B} \underline{P}^{-1} \underline{B}^T$

and $\gamma = \text{degrees of freedom.} \quad - (7.8)$

The compatibility between the spline model and the observed data points can be evaluated through the Chi-squared (χ^2) statistical test on the a posteriori variance factor ($\hat{\sigma}_0^2$). The a priori variance factor (σ_0^2) of the spline model is set to unity (i.e. the weight matrix $\underline{P} := \underline{\Sigma}_{\underline{x}}^{-1}$). The validity of the hypothesis that both variance factors are compatible with each other can be tested using the knowledge that the statistic

$$y := \gamma \hat{\sigma}_0^2 / \sigma_0^2 \quad (\text{with } \gamma \text{ degrees of freedom})$$

has a $\chi^2(\xi; \gamma)$ probability density distribution [Vanicek and Krakiwsky 1982]. Incompatibility exists between the a posteriori variance factor ($\hat{\sigma}_0^2$) and a priori variance factor (σ_0^2) (i.e. the Chi-squared test fails) when the assumed model for the observations is incorrect or when the a priori covariance matrix of the observations is in error [Vanicek and Krakiwsky 1982: page 237].

7.3.2 Simplification of Functionally Constrained Model

Two basic facts regarding the spline model (equation 7.1) that can be taken advantage of are:

1. the model is linear, and
2. the model is parametric (i.e. $\underline{B} = -\underline{I}$, with \underline{I} being the identity matrix).

As the model is linear, no iterations are required. The incorporation of an a priori solution vector (subroutine APRORI in Appendix VII) is seen as just a method of increasing the numerical accuracy of the solution vector.

By being a parametric model, the equations (7.8) given for the general case are thus reduced to

$$\begin{aligned}\hat{\underline{\delta}} &= - (\underline{A}_1^T \underline{P} \underline{A}_1)^{-1} (\underline{A}_2^T \hat{\underline{k}}_2 + \underline{A}_1^T \underline{P} \underline{w}_1) \\ \hat{\underline{k}}_2 &= [\underline{A}_2 (\underline{A}_1^T \underline{P} \underline{A}_1)^{-1} \underline{A}_2^T]^{-1} [\underline{w}_2 - \underline{A}_2 (\underline{A}_1^T \underline{P} \underline{A}_1)^{-1} \underline{A}_1^T \underline{P} \underline{w}_1] \\ \hat{\underline{v}} &= - (\underline{A}_1 \hat{\underline{\delta}} + \underline{w}_1) \\ \hat{\sigma} &= \underline{\hat{v}}^T \underline{\hat{P}} \underline{\hat{v}} / \gamma\end{aligned}$$

- (7.9)

Chapter 8

PRECISION ESTIMATION

In this chapter, the covariance law is described, an expression for the covariance matrix for the least-squares estimates is given and the computational accuracy of the algorithm is addressed.

Precision estimation of the least-squares estimates and all other subsequently derived quantities are obtained by using the covariance law.

8.1 COVARIANCE LAW

The covariance law, which is also called the law of covariances and propagation of covariances [Wells and Krakiwsky 1971: page 20], is stated as follows:

Given a variate \underline{y} linearly related to another variate \underline{x} by the equation

$$\underline{y} = \underline{G}\underline{x} \text{ , } \underline{G} \text{ being the transformation matrix from } \underline{x} \text{ to } \underline{y}$$

and with

$$\begin{aligned} E[\underline{y}] &= E[\underline{G}\underline{x}] \\ &= \underline{G}E[\underline{x}] \text{ , } E \text{ being the expectation operator.} \end{aligned}$$

- (8.1)

The covariance matrix of \underline{y} (i.e. $\underline{\Sigma}_y$), given the covariance matrix of \underline{x} (i.e. $\underline{\Sigma}_x$), is hence derived as follows:

$$\begin{aligned}
 \underline{\Sigma}_y &= E[(\underline{y} - E[\underline{y}])(\underline{y} - E[\underline{y}])^T] \\
 &= E[(\underline{Gx} - \underline{G}E[\underline{x}])(\underline{Gx} - \underline{G}E[\underline{x}])^T] \\
 &= E[\underline{G}(\underline{x} - E[\underline{x}])(\underline{x} - E[\underline{x}])^T \underline{G}] \\
 &= \underline{G}E[(\underline{x} - E[\underline{x}])(\underline{x} - E[\underline{x}])^T] \underline{G} \\
 &= \underline{G} \underline{\Sigma}_x \underline{G}^T
 \end{aligned}$$

- (8.2)

The propagation of variances and covariances with linear functions is independent of the density functions and is valid for any probability distribution [Mikhail 1976: page 78].

Incidentally, the \underline{G} matrix essentially represents the Jacobian of \underline{y} with respect to \underline{x} , i.e.

$$\underline{\Sigma}_y = \underline{J}_{y,x} \underline{\Sigma}_x \underline{J}_{y,x}^T$$

- (8.3)

with $\underline{J}_{y,x} := \frac{\partial \underline{y}}{\partial \underline{x}}$

8.2 PRECISION OF LEAST-SQUARES ESTIMATES

Using the above covariance law (equation 8.3) and equations (7.9), the a posteriori covariance matrix of the unknown solution vector($\hat{\underline{\delta}}$) is of the form:

$$\underline{\Sigma}_{\hat{\underline{\delta}}} = \underline{N}^{-1} (\underline{I} - \underline{A}_2^T \underline{M}^{-1} \underline{A}_2 \underline{N}^{-1}) \quad - (8.4)$$

where $\underline{N} = \underline{A}_1^T \underline{P} \underline{A}_1$

and $\underline{M} = \underline{A}_2 \underline{N}^{-1} \underline{A}_2^T$

8.3 PRECISION OF COMPUTATIONS

The spline algorithm approaches instability under either of the following conditions:

1. the number of data points in the knot intervals is insufficient to define the spline (Section 7.3), or
2. the observed data points within an interval have large variances (or very low weights).

Computational accuracy is degraded when either of the above occurs. Both conditions cause the normal equation matrix \underline{N} , of the observation model \underline{f}_1 to be ill-conditioned. If the violations are severe enough, the matrix becomes singular. Between singularity and a well-conditioned matrix, there lies many shades of ill-conditioning, some of

which are not detected in the calculations, but give apparently good results through round-off.

In an effort to detect such "in-betweens" the program DSPLIN utilizes two different techniques. Firstly, condition numbers (via subroutine COND in Appendix VII) are computed for all inverses computed in DSPLIN and secondly, a check on the internal computational accuracy is performed (in subroutine LS in Appendix VII). Equations (II-4 and II-2) used by routines COND and LS in Appendix VII are described in Appendix II.

As a preventive measure, a count (by subroutine CHECK) of the number of data points in each knot interval is made prior to computations and superfluous knots dropped if necessary.

The aspect of numerical computational accuracy and the detection of precision loss in computing the least-squares estimates is further addressed in Appendix II.

Chapter 9

DISCUSSION AND EVALUATION OF THE SPLINE ALGORITHM

In this chapter, the various areas of investigation into the performance of the spline algorithm are discussed. Selected results of the processing of the simulated and LOREX data sets are presented.

The following are the areas investigated:

- a) Distribution of data points within a data series.
- b) Selection of knots.
- c) Completeness of spline model.
- d) Boundary (outer) knots.
- e) Joining two separate adjacent splines.

9.1 DISTRIBUTION OF DATA POINTS

The simulated data set (Appendix IV), is created, amongst other reasons, to evaluate the spline algorithm under the following distributions of data points within a data series:

1. Equal distribution of points along a curve.
2. Dense distribution of points along a straight line.

3. Irregular distribution of points along a straight line.
4. Sparse distribution of points along straight line.
5. No data points along a curve.

The simulated data points were generated at equal time intervals by equation IV-1. Of the 50 simulated data points, 21 were chosen as the simulated data set. The selection of the points is such that all the above distributions appeared in subsets of the simulated data series.

From the multitude of tests that were carried out (Table 9-1 forms but a small sample), no detrimental effects on the spline were observed with any of the above mentioned data point distributions.

9.2 SELECTION OF KNOTS

In this section, the topic of knot selection is addressed. The design constraints of the curve fitting algorithm are given. Performance of the various possible knot selection schemes are discussed and conclusions drawn.

The computation of the spline, given the location of the knots (e.g. through the specification of the third variable time, in navigation data sets), has been discussed in the Chapters 5 and 6. The number and location of the knots

TABLE 9-1a Results from the DSPLIN Program Using Simulated Data

TEST NO.	KNOT SELECTION SCHEME USED	RUN NO.	NO. OF KNOTS	R.M.S. RESIDUALS	VARIANCE FACTOR	CHI. SQ. TEST*	ADDITIONAL INFORMATION (SEE BELOW)		REMARKS
							Knot Times ¹	Curve Fitting Options ²	
1	Equal interval	1	3	30.07	24.24	FAIL			*Two of the knots have been dropped by CHECK routine. i.e. only 8 knots were used.
		2	5	7.94	1.69	PASS			
		3	10 ⁺	5.57	1.00	PASS			
2	Visual inspection	1	3	20.42	10.57	FAIL	0,38,98		
		2	5	6.03	0.96	PASS	0,8,43,78,98		
3	Curve fitting routine (with residual error bar tests at α % level as the rejection criteria	1	7	5.89	1.00	PASS	0,17,27,39,56,45,98	(Parameter No.) (1 2 3 4 5 6 7) 6 100 10 2 1 0 0	$\alpha = 50\%$
		2	7	5.66	0.96	PASS	0,17,27,39,63,80,5,98	6 100 10 2 0 0 0	$\alpha = 50\%$
		3	6	5.20	0.76	PASS	0,22,34,56,71,98	6 100 10 2 1 0 0	$\alpha = 90\%$
4	Curve fitting routine (with the apos. variance factor at α % confidence level as the rejection criteria).	1	4	7.04	1.29	PASS	0,47,72,5,98	(Parameter No.) (1 2 3 4 5 6 7) 6 1 10 10 2 0 1	$\alpha = 99\%$
		2	5	7.21	1.39	PASS	0,25,47,80,98	6 1 10 10 2 1 0	$\alpha = 50\%$
		3	6	5.46	0.84	PASS	0,22,29,47,84,5,98	6 1 10 10 2 1 1	$\alpha = 38\%$

* at the 99% confidence level

[1] Knot Times - These are the times of the knots chosen to represent the simulated data series. A complete listing of the times and location of the input positions of the data points is given in Appendix IV.

[2] Curve Fitting

Options - These are the parameters used with the curve fitting algorithm (Subroutine FIT in Appendix VII). A condensed description of the set of parameters (or options) is given in the following Table 9-1b.

TABLE 9-1b

DESCRIPTION OF THE PARAMETERS (OR OPTIONS) OF THE
CURVE FITTING ALGORITHM (FIT)

Parameter Number	Description
1	: Minimum number of data points contained in the first cubic polynomial.
2	: Location of the designated knot times: 1 : midway between two data point times. 0 : coincident with the data point time.
3	: Number of points, in terms of a percentage of the current interval, to be placed in the extended interval (see Figure 9-1).
4	: Weighting factor(X) for the former slope vector based on the estimated covariance matrix, i.e. (weight matrix) ⁻¹ := formal covariance matrix * (10/X) < 1 : unweighted, i.e. X=0. 10 : formal covariance matrix, i.e. X=1. 10> : formal covariance matrix to be divided by (10/X).
5	: Minimum number of data points per interval.
6	: Inclusion of data points in the extended interval in the rejection tests.
7	: Minimum number of data points in the extended interval.
The last three parameters deal with the level of output desired from the subroutine FIT.	
8	: All information requested, e.g. current knot vector, residuals, a posteriori variance factor and status of curve fitting.
9	: Print computed knot vectors only.
10	: Print formal or estimated covariance matrix of computed knot vector.

Note: Generally, '1' denotes 'yes' and '0' denotes 'no'

influence the resulting splined (smoothed) values. At one extreme, a lower number of knots decreases the computational load and heavily smooths the data set. At the other extreme, the spline approaches the interpolation of all the data points; including the noise in them.

This difficulty is present in all smoothing algorithms. The desired degree of smoothness of the resulting curve must be determined by external evidence; this is more of an art than a science.

Four approaches to the problem of knot selection are incorporated (through subroutine SELKNT in Appendix VII) in the spline algorithm.

They are:

1. equal time intervals (i.e. equal time span per cubic interval),
2. equal point intervals (i.e. equal number of points per cubic interval),
3. knots chosen by visual inspection, and
4. knots chosen via a "trend evaluating" algorithm.

The first and second knot selection schemes are easy to implement and the spline model can be considered as "single number criterion" type of smoothing algorithm (i.e. different degrees of smoothing are achieved by varying only one parameter).

With unequally spaced or irregular data sets, a reduction in the number of knots is achieved by strategically locating

each knot within the data span. This can be done either by visual inspection or through some predefined trend evaluating (or curve fitting) algorithm.

Basically, what is needed is a process to determine the length of time within a data span in which the data series can be aptly represented by a cubic curve.

With reference to the LOREX navigation data sets, the choice of the minimum time interval between knots can be obtained by evaluating the length of the response time of the ice platform to the maximum possible force that can act on the ice sheet. Unfortunately, due to the complexity of the ice sheet, wind stress effects or that of undercurrents, a single figure cannot be easily obtained. In addition, if the ice is subjected to a force less than the maximum, it may be more appropriate to smooth over a longer time span.

A plausible alternative is the implementation of an algorithm designed specifically to automatically select "optimum" knot locations based on some predefined criteria. For the design of the trend evaluating routine, numerous papers (e.g. Ellis and McLain [1977], Ichida and Kiyono [1977] and Chung [1980]) on curve fitting have been drawn upon to create the "weighted one pass (left to right) local cubic polynomial" curve fitting algorithm (subroutine FIT in Appendix VII).

Several considerations must be taken into account in designing such an algorithm. Firstly, the spline function

cannot be computed solely using local data, i.e. it is of a global nature [Ellis and McLain 1977]. An alternative has to be found which still uses the attractive properties of both piecewise cubics and the least-squares norm as the basis for the curve fitting approximation.

Ichida and Kiyono [1977] through eigenvalue analysis (based on simple assumptions) and Chung [1980] using more complex error techniques, demonstrated that the C^2 functions, (i.e. space containing all polynomials with second derivative continuity), cannot be used as they exhibit inherent instabilities. The authors, Ichida and Kiyono, and Chung, mentioned above, used C^1 functions and the extended interval concept to resolve the numerical instabilities in the curve fitting procedure.

The "extended interval" concept (Figure 9-1) entails extending the current interval, Δt , of the j th piecewise function by $\delta \Delta t$ to incorporate additional observed data points in the computation of the right end knot vector (i.e. the $(j+1)$ th knot vector in Figure 9-1). The position and slope of the right end knot is hence adjusted to allow for the next curve segment [Chung 1980]. Very briefly, the non-inclusion of future data through the extended interval concept results in instabilities because of the amplification of propagation and truncation errors [Chung 1980].

A curve fitting algorithm with variable controlling parameters (or options - Table 9-1b) has been developed

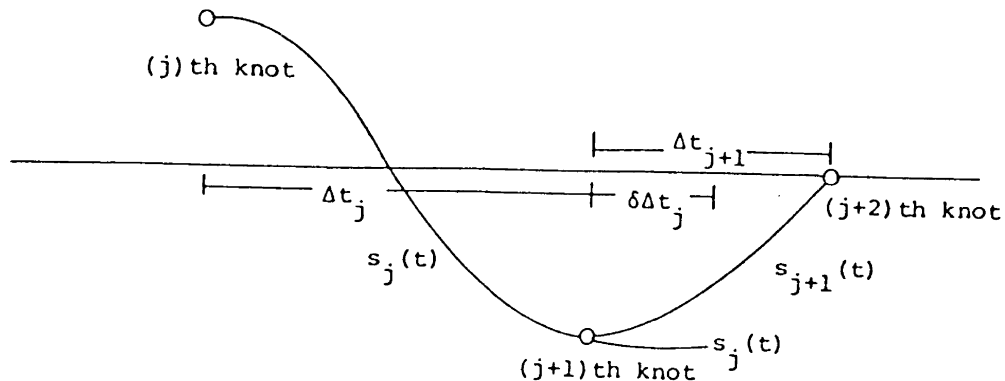


FIGURE 9-1 Extended Interval Concept in Curve Fitting

(subroutine FIT in Appendix VII). It utilizes both weighted knot and slope information from the previous interval to simultaneously compute two least-squares cubic polynomials, x against t and y against t (see Section 5.2, equation 5.3), in the current and extended intervals, and iteratively extends both intervals until the chosen error tolerances are exceeded.

Hence for the Δt_j interval, the two least-squares cubic polynomial coefficients are computed using data points from the interval $\Delta t_j + \delta\Delta t_j$. The extension, $\delta\Delta t_j$, is taken as a fixed percentage of the interval Δt_j . Both intervals are increased until the chosen error tolerances are exceeded or when the end of the data series is reached. These error tolerances can be either simple error bar tests on the residuals (i.e. the distance between smoothed and observed data points) or the Chi-squared statistical test on the a posteriori variance factor of each subsequent fit (Section 7.3.1).

The performance of the four knot selection schemes were evaluated using both the simulated and LOREX data sets. Due to the different characteristics of the simulated and LOREX test data sets, each is discussed in turn.

9.2.1 Knot Selection Algorithm Using Simulated Data

The following are the general conclusions for the simulated data set:

1. All knot selection schemes, with an adequate density of knots, are applicable (see Table 9-1).
2. Equal interval knot schemes, as a rule, do not always give the best distribution of knots. However, with a sufficient density of knots, the underlying motion or curve can be aptly fitted (see Table 9-1, Test No. 2).
3. Visual knot selection, which at times do lead to better knot distributions (Table 9-1, Test No. 2) than equal interval knot schemes, are difficult to implement.
4. The curve fitting algorithm (Table 9-1, Test No. 3 and Test No. 4) gives the best results; best in terms of lowest number of knots and with an equivalent variance factor (i.e. compare results of Test No. 3, Run No. 3 with that of Test No. 4, Run No. 2 or Run No. 3).

5. The use of the Chi-squared statistical test on the a posteriori variance factor in each of the subsequently fitted curves by the curve fitting routine (FIT) as the rejection criterion seems remarkably better than the simple error bar residual (or outlier) tests (i.e. result of Table 9-1, Test No. 3 is better than Test No. 4).
6. The interplay between the 10 option parameters (Table 9-1b) on the curve fitting routine requires further investigation and at this point no guidelines to the use of the curve fitting algorithm can be given.

9.2.2 Knot Selection Algorithm using LOREX Test Data Sets

Different knot selection schemes are used for the LOREX data sets (Table 9-2, Tests Nos. 2, 3 and 4). The curve fitting algorithm could not optimally locate the knots in the LOREX data sets. The two possible reasons for this are:

1. incorrect interplay between the parameters on the fitting routine, or
2. presence of outliers (i.e. badly determined data points) in the observed data sets.

Different combinations of the parameters of the curve fitting routine were attempted and results indicated the second reason to be the most probable cause.

Although visual inspection of Figures V-1 to V-9 in Appendix V of the LOREX test data sets suggest the presence

of outliers, examination of the statistics of the recorded passes revealed no apparent reason for the discrepancies in the computed positions. In an effort to detect outliers, a linear filter routine was devised (subroutine FILTER in Appendix VII). The routine fits a straight line, via the method of of least-squares, to a subset of the data series and shifting the location of the subset in increments until the total data series is sequenced. Interpretation of the results which take the form of a time series of ratios of the residuals to its input standard deviations proved difficult. Its use was later discontinued.

Due to the great variability in terms of noise on the test data sets, the visual knot selection scheme was not used. For the two remaining knot selection schemes, no significant differences between them were detected. Equal points per interval knots (Table 9-2, Test No. 4) performed just as well as equal time interval knots (Table 9-2, Test No. 2 and Test No. 3).

For the purposes of investigating the completeness of the spline model and the inadequacies of the formal covariance matrices of the position fixes, the equal time span per cubic interval knot selection scheme was used. For each of the three test data sets, the knot time intervals were chosen at one-third, one-fifth, one-tenth and one-twentieth of the total time span of the test data series used (e.g. if the test data time span was 72 hours, then the knot time

TABLE 9-2 Results of the various test runs by DISPLIN on the 3 LOREX test data sets under different conditions.

TEST NO.	RUN NO.	NO. OF KNOTS	R.M.S. ERROR (m)			VARIANCE FACTOR			CHI-SQ. TEST			D.O. F.			COMMENTS CONDITIONS OF RUN
			TEST DATA SET NO.			TEST DATA SET NO.			TEST SET NO.			TEST SET NO.			
			1	2	3	1	2	3	1	2	3	1	2	3	
1	1	3	429.70	1,068.31	908.82	1,819.91	5,290.20	110.87	F	F	F	194	194	194	Formal covariance matrices from position fixes are used as weights.
	2	5	387.85	692.63	909.55	482.69	389.73	97.44	F	F	F	190	190	190	
	3	10	385.30	579.32	912.82	289.55	89.39	64.64	F	F	F	180	180	180	
	4	20	402.70	588.47	911.61	155.44	49.10	55.27	F	F	F	160	160	160	
2	1	3	411.10	1,039.88	821.15	5.29	78.65	2.39	F	F	F	194	194	192	Minimum semi-minor axis (B) of 35 m enforced. Altitude and velocity errors modelled.
	2	5	380.38	657.13	819.10	1.70	5.51	2.17	F	F	F	190	190	188	
	3	10	381.42	584.23	121.00	1.24	2.32	1.59	P	F	F	180	180	178	
	4	20	385.92	588.89	820.66	1.03	1.37	1.61	P	F	F	160	160	158	
3	1	8	386.19		817.29	1.35		1.82	F		F	190		188	Minimum B = 35 m. Alt and velocity errors modelled. Knot times at 1/2 day (12 hrs) and 1/4 day intervals.
	2	8	379.60		818.11	1.26		1.61	P		F	184		182	
	3	4		658.09			10.69			F	F		192		
	4	7		618.32			3.96			F			186		
4	1	3	409.89	1,083.64	821.17	4.12	92.78	2.40	F	F	F	194	194	192	Equal no. of point intervals. Minimum B = 35 m. Alt and velocity errors modelled. Pts per interval = [50,25,11,5] pts.
	2	5	381.30	704.31	819.67	1.41	9.64	2.17	F	F	F	190	190	188	
	3	10	383.96	581.77	821.00	1.05	2.12	1.50	P	F	F	180	180	178	
	4	21	386.88	584.16	817.42	0.93	1.56	1.64	P	F	F	158	158	156	

TABLE 9-2 (Continued)

TEST NO.	RUN NO.	NO. OF KNOTS	R.M.S. ERROR (m)			VARIANCE FACTOR			CHI-SQ. TEST			D.O. F.			COMMENTS AND CONDITIONS OF RUN
			TEST DATA SET NO.			TEST DATA SET NO.			TEST SET NO.			TEST SET NO.			
			1	2	3	1	2	3	1	2	3	1	2	3	
5	1	3	416.55	1,094.30	911.52	57.31	1,472.74	35.41	F	F	F	194	194	194	A minimum of 30 m std deviation is imposed on all formal error ellipses of position fixes.
	2	5	380.15	662.83	910.28	22.50	111.34	27.17	F	F	F	190	190	190	
	3	10	387.48	581.60	911.40	12.25	30.37	16.25	F	F	F	180	180	180	
	4	20	386.77	586.81	918.19	9.25	19.34	14.95	F	F	F	160	160	160	
6	1	3			820.49			33.67			F			192	Investigating the effect of the deletion of pt. 37 (bad pt.) in Test Data Set 3. All parameters are as in Test No. 5.
	2	5			818.46			27.17			F			188	
	3	10			820.67			16.13			F			176	
	4	20			823.81			14.84			F			158	

intervals would be set at 24, 14.4, 7.2 and 3.6 hours respectively). Three knots represent the absolute minimum number of knots one can apply to any data set. The resulting data set is heavily smoothed. Twenty knots, on the other hand, ensures a sufficient density of knots to aptly portray any of the LOREX test data sets regardless of knot placements.

9.3 COMPLETENESS OF THE SPLINE MODEL

The completeness of the spline model relates directly to the choice of the number of knots for each data span. The results, in Table 9-1 and Table 9-2, show that the root mean square error (rms) and the a posteriori variance factor are effective in determining whether a sufficient number of knots have been used. When the model has an inadequate knot density, an increase in the number of knots significantly reduces the value of the root mean square of the differences between smoothed and observed positions. This improvement in the rms diminishes as the number of knots continue to rise (Table 9-1, Test No. 1). The failure of the Chi-squared statistical test (Section 7.3.1) on the variance factor can be attributed to either:

1. an incorrect or incomplete model, or
2. an incorrect a priori covariance matrix for the observed data set [Vanicek and Krakiwsky 1982: page 237].

Under a "steady state" in the rms (i.e. no appreciable change in rms follows any increase in the number of knots, e.g. Table 9-2, Test No. 1, test data set No. 3, Run nos. 1 to 3) the latter reason is given for its failure to pass the statistical Chi-squared test.

Deletion of a badly determined position fix (e.g. point 37 in test data set three was computed using severely unbalanced Dopplers about the point of closest approach) affects the rms more than the variance factor (see Table 9-2, Test Nos. 5 and 6). This suggests that the "erroneous" fix is correctly weighted within the data span.

It should be noted that the Chi-squared statistical test is only a global indication of knot sufficiency (Section 7.3.1). Knot selection at the local levels can be evaluated through the analysis of a time series of standardised residuals (i.e. r_x and r_y). The standardised residuals are defined as follows:

$$r_x := (E_p - E_s) / \sigma_{Ep}$$

and

$$r_y := (N_p - N_s) / \sigma_{Np}$$

where p - subscript denoting observed position coordinates
(E for eastings and N for northings),

σ - formal standard deviations associated with each
observed position coordinate,

and s - subscript denoting smoothed position coordinates
produced by the spline (E for eastings and
N for northings).

9.4 BOUNDARY (OR OUTER) KNOTS

Two boundary knot vectors, along with their a priori covariance matrices, are read together with the observed data points, into the least-squares process. For a single separate spline computation, the outer data points are usually chosen as knots.

Weighting the end knot positions as heavily as the outer data points is found to bias the final location of the outer knots; more so when the extreme points have small formal covariance matrices and are unrepresentative of the true precision of the points. In light of this, low weights are recommended in the absence of information about the end knot vectors.

9.5 SPLICING SPLINES

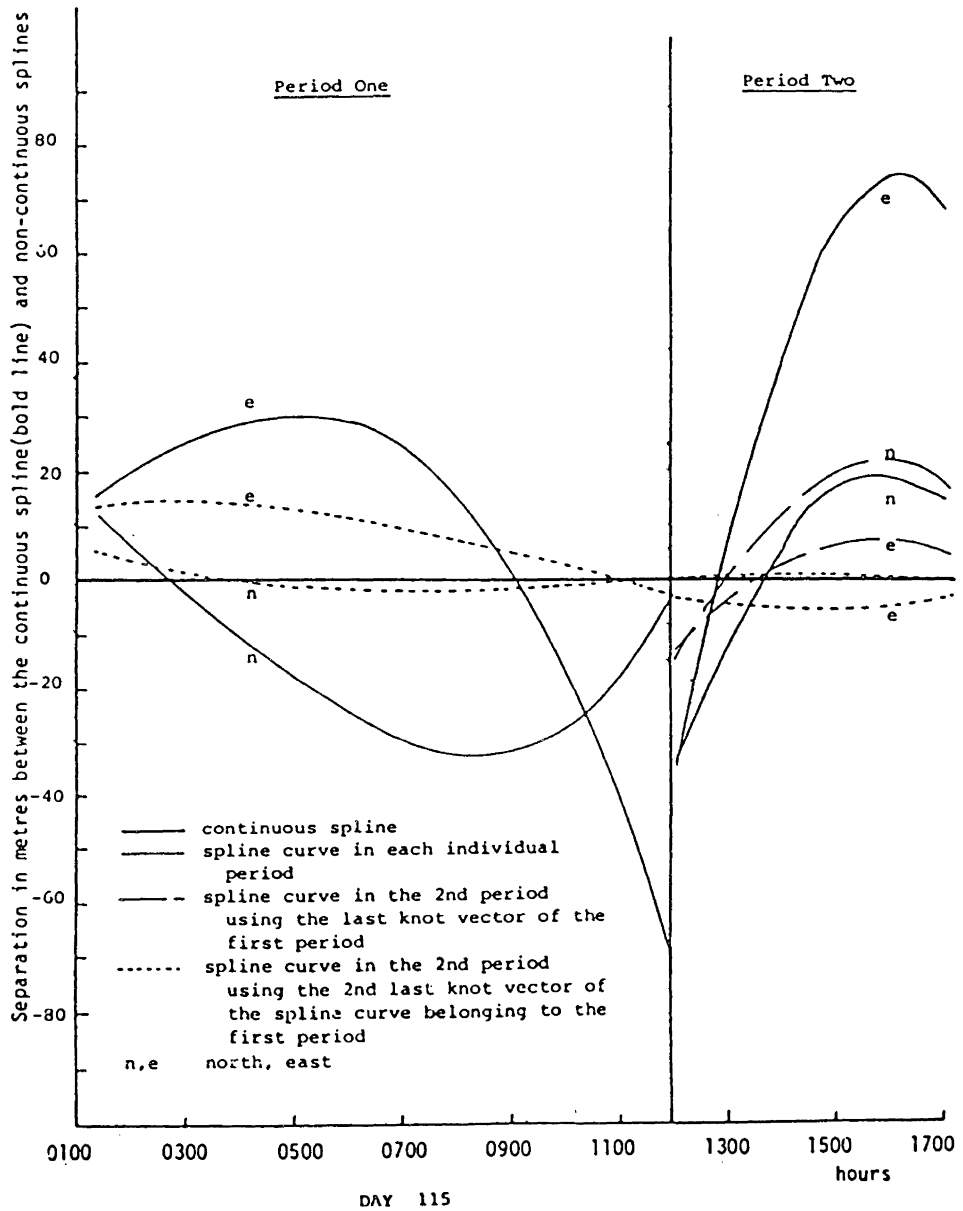
The primary purpose of the inclusion of outer knot vectors into the program is to facilitate the joining of splines from separate adjacent data spans. This is desirable when dealing with very large data series. The minimum data point overlap between adjacent splines is investigated by comparing two separate but adjacent splines computed under different conditions against a continuous spline over the whole period.

The experiments are conducted only with LOREX test data set one (Appendix V). Test data set one (which consist of position fixes for station S0 from day 113 hr 14 to day 116 hr 19) is subdivided into two periods. Period one is from day 113 hr 14 to day 115 hr 12 and period two is from day 115 hr 12 to day 116 hr 19.

The following are the splines computed using DSPLIN:

1. A continuous spline over the whole period (i.e. from day 113 hr 14 to day 116 hr 19). In Figure 9-2, the continuous spline is represented by the straight bold line.
2. Separate and unspliced splines for period one (i.e. from day 113 hr 14 to day 115 hr 12) and period two (i.e. from day 115 hr 12 to day 116 hr 19). These splines are represented by curved unbroken lines in Figure 9-2.
3. Second spline in period two computed with the estimated end knot vector and its covariance matrix, from the first spline in period one, as its beginning knot vector. This is represented by the long dashed lines in Figure 9-2.
4. Second spline is computed using the second last estimated knot vector from the first spline together with a common overlap of data points (i.e. the spline is computed using data points from the period day 115 hr 0 to day 116 hr 19; with day 115 hr 0 being the

FIGURE 9-2 Comparisons between separate and continuous splines. The effect of supplying a beginning knot vector to the second spline is clearly illustrated by the plot below.



location of the second last knot vector of the first spline). This is portrayed in Figure 9-2 by the short dashed lines.

Referring to Figure 9-2, the use of the end knot vector (and its a posteriori covariance matrix) of the first spline as the beginning knot vector of the second spline, allows the latter spline to 'settle down' faster. The discrepancy between the second spline and the continuous spline, in the first knot interval, diminishes further when, instead of the last knot vector, the second last knot vector of the former spline, along with a common overlap of data points, is used.

Apparently the second spline, with a weighted outer knot vector, demands a one knot interval overlap to damp out the oscillations in its front segment. In light of this, all adjacent splines should contain at least two common knot intervals and points, with the first splined values read up to the second last knot and the second set of values starting from the second knot (illustrated in Figure 9-3).

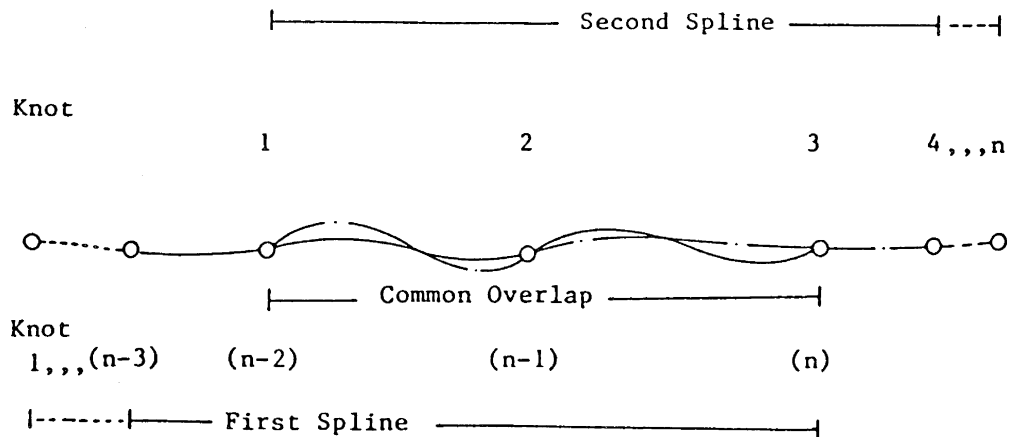


FIGURE 9-3 Minimum Overlap Between Splines

Chapter 10

DISCUSSION, EVALUATION AND APPLICATION OF THE SPLINE ALGORITHM TO THE LOREX DATA SETS

In this chapter, the orbital separation between the NNSS satellites during the period of the expedition are given, the processing sequence of the LOREX data sets are outlined, the error models used to modify the formal covariance matrix of the position fixes are developed, the real-time application of the spline algorithm is discussed, results of the comparisons between DSPLIN and GEODOP, and SMOBS and GEODOP are given, and the results from the processing of the three LOREX data sets from the ice stations are given and the difficulties investigated.

The general outline of the processing of the three LOREX data sets is given in Figure 10-1.

10.1 SEPARATION BETWEEN TRANSIT SATELLITE ORBITS

The three LOREX test data sets (Appendix V) were visually examined prior to the processing to determine if there exists any periodic degradation, as indicated by a larger scatter of position fixes about the mean, within the data series. Visual inspection of the plots of the test data

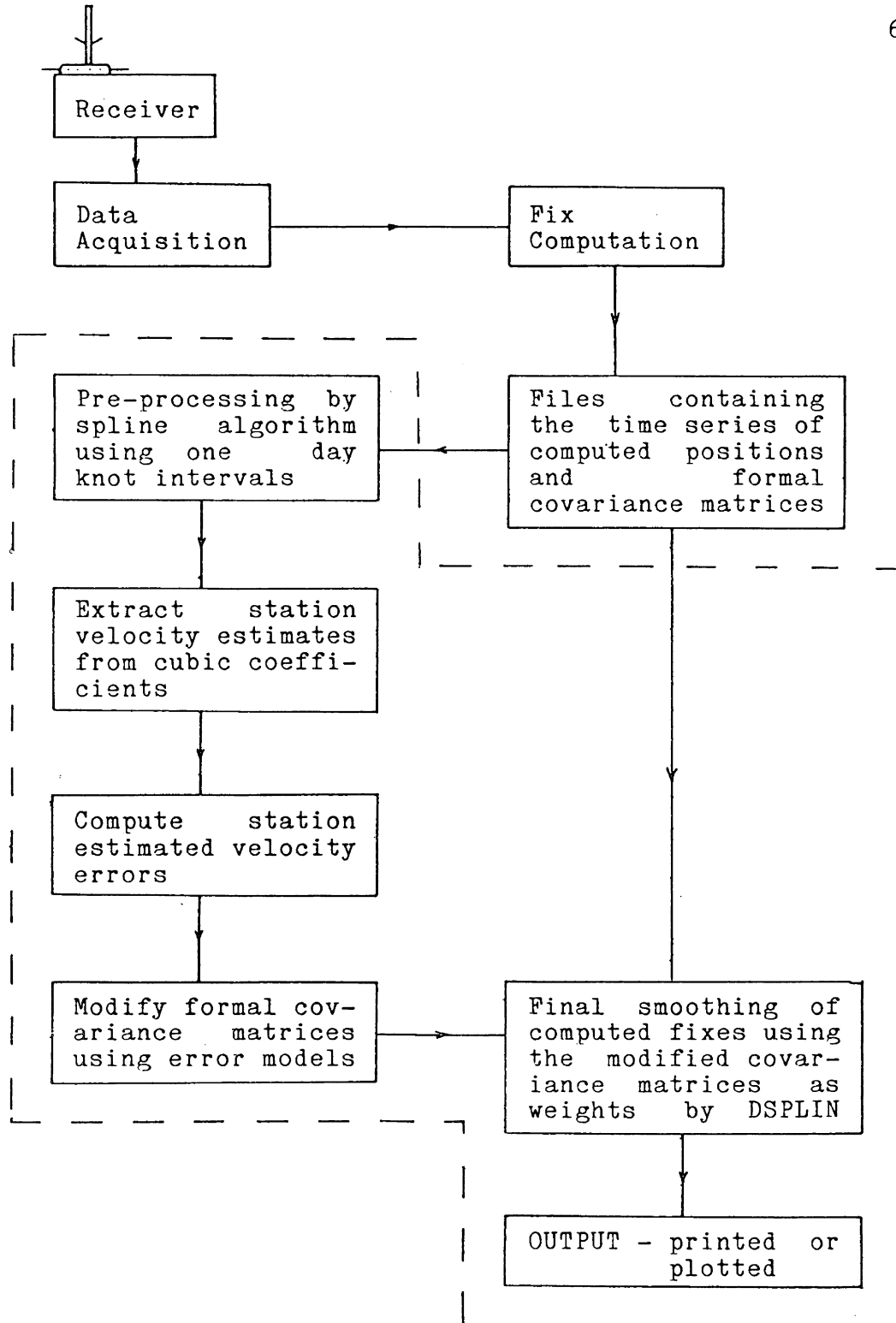


FIGURE 10-1 LOREX Satellite Data Processing Flow-chart. Enclosed within the broken line is the processing procedure used in this thesis.

sets reveals an apparent periodic degradation at 12 hour intervals, i.e. at 0 and 1200 hours each day (see Figures V-1 to V-9). This could have been caused by the orbital configuration of the Transit satellites during the period of the expedition. Figure 10-2, drawn from the orbit parameters of the operating satellites published by USNO [1979], shows the orbit of the satellites to be within a 90 degree quadrant. The closeness of the orbital planes and direction of motion of the satellites may have contributed to the observed periodic degradation.

10.2 STATION VELOCITY ESTIMATES

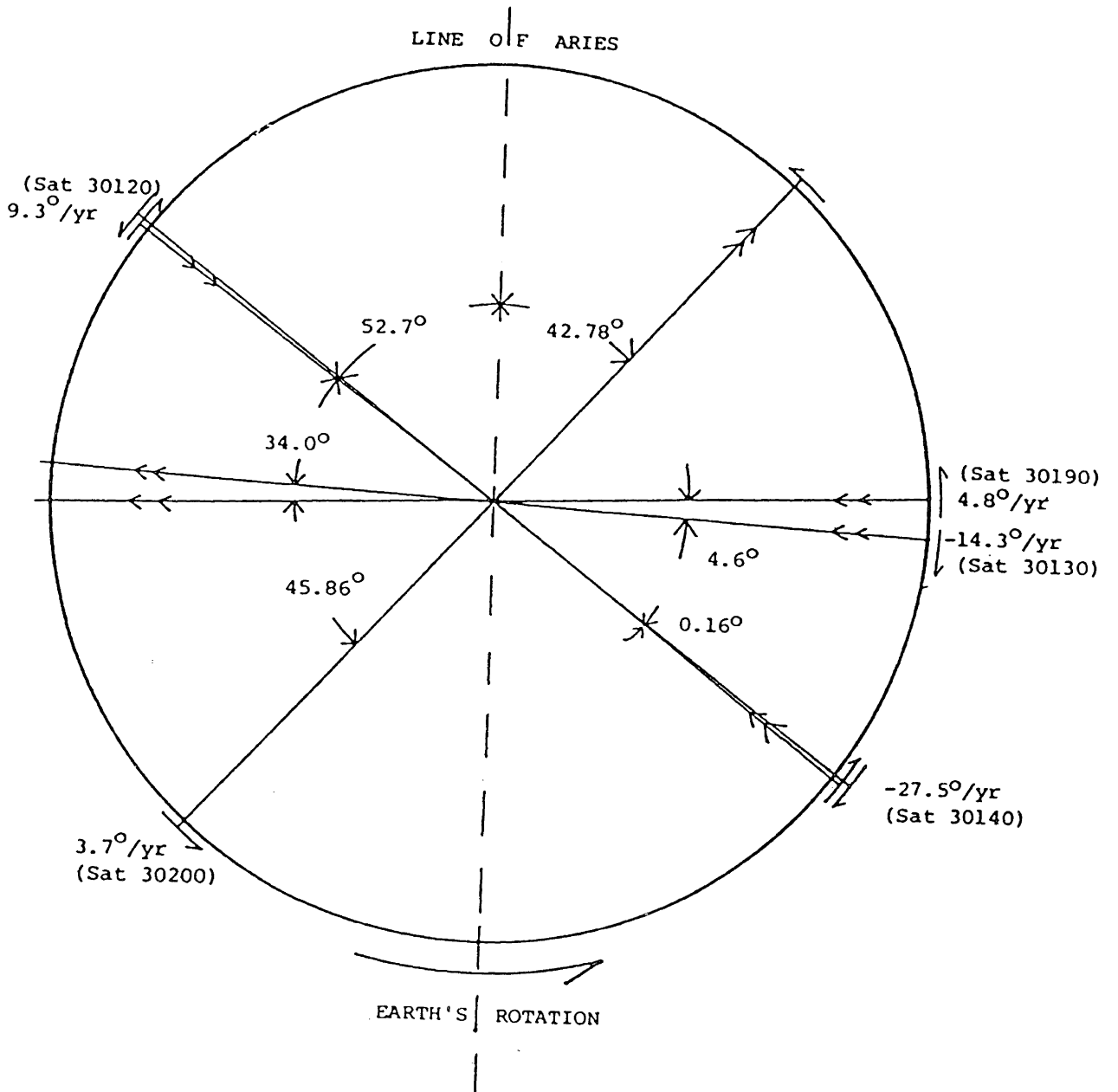
For each of the three test data sets there exist three sets of velocity vectors:

1. Real-time predicted speeds and azimuths.

These are the speeds and azimuths used in the real-time computation of the position fixes.

2. Pre-processed splined speeds and azimuths.

The spline algorithm is used to generate a set of smoothed velocities and azimuths for the stations. To extract the long term trends in the motion of the station, the spline is computed using one day knot intervals over the full data series.



NORTH POLE VIEW

FIGURE 10-2 ORBITAL SEPARATION OF 5 OPERATIONAL TRANSIT SATELLITES
ON MAY 1ST 1979

3. Final splined velocities and azimuths.

These are the final set of speeds and azimuths produced by program DSPLIN incorporating all the modifications described in this chapter.

The error in the estimated velocity of the receiver, as will be described in Section 10.3.2, is the difference between final splined velocities and real-time predicted values. An approximate velocity error is the difference between the pre-processed splined values and the real-time predicted velocities. In this thesis, however, the real-time predicted velocity estimates are assumed to be nonexistent and the receiver velocity error is that computed by the pre-processing spline. The real-time predicted velocity estimates could not be easily extracted from the existing Doppler data.

10.3 A PRIORI COVARIANCE MATRICES

The spline algorithm requires that the a priori covariance matrix adequately reflect the accuracy of the position determinations. The formal covariance matrices obtained from the fix computations appears incorrect from the results of the Chi-squared statistical tests (Table 9-2, Test No. 1). In this section, a description and justification of the procedures used to modify the formal

covariances of the computed position fixes are given. The results of each modification to the a priori covariances are evaluated.

Hoar [1982] and Stansell [1978] stated that a single pass point positioning accuracy for a stationary receiver is in the vicinity of 37 metres (at one sigma level) and between 27 to 37 metres rms respectively. The imposition of a minimum of 20 metres (Table 10-1, Test No. 1 and Figure V-1a) or 30 metres (Table 9-5, Test No. 5) on the standard deviations of the passes (i.e. all fixes with a standard deviation of less than the minimum are scaled up equally in eastings and northings) results in a dramatic drop in the magnitude of the variance factor. This further supports the hypothesis that the a priori covariance matrices, resulting from the fix computation (based on the residuals of the Doppler observations) are unrepresentative of the accuracy of the position determinations. The effect of errors in the satellite coordinates and those due to receiver velocity errors are not represented in these formal covariance matrices.

10.3.1 Modelling Orbital Errors

Wells [1974] mentioned that the broadcast predicted satellite orbits have, approximately, 26, 11 and 5 metres standard deviations in the along, radial and cross track components respectively. The uncertainty in the computed

positions can be no smaller than the uncertainties in the position of the satellite. A value of 30 metres, based on the approximate precision of the along track position of the satellite, was chosen as the minimum allowable semi-minor axis for the error ellipse of the fixes. In order to assess the impact of setting this constraint on the formal covariance matrices of the position fixes, this figure was increased to 35 metres and the test runs (done under the 30 metres minimum semi-minor axis) repeated. Formal error ellipses which had semi-minor axes of less than the minimum were scaled up accordingly. The scale factors thus range from 1 to 30 (or 35). The imposition of a minimum of one metre on the semi-minor axis of the formal error ellipse prior to scaling limits the applied scale factor to within the said range. The scaled error ellipses are then translated via equations (VI-5) developed in Appendix VI to their equivalent standard deviations and covariances (subroutine ELLSIG in Appendix VII).

Test No. 2 and Test No. 6 (Table 10-1) performed under the above mentioned conditions show an improvement in the variance factor; with test data set one passing the statistical Chi-squared test. Test data sets two and three, however, still fail to pass the Chi-squared test even with the maximum number of knots. This suggests the presence of yet unmodelled errors (Section 9.3).

TABLE 10-1 Results of the various test runs by DSPLIN on the 3 LOREX
Test Data Sets under different conditions.

TEST NO.	RUN NO.	NO. OF KNOTS	R.M.S. ERROR (METRES)			VARIANCE FACTOR			CHI-SQ. TEST			D.O. F.			COMMENTS AND CONDITIONS OF RUN
			TEST DATA SET NO.			TEST DATA SET NO.			TEST SET NO.			TEST SET NO.			
			1	2	3	1	2	3	1	2	3	1	2	3	
1	1	3	415.30	408.27	911.64	103.65	2,204.77	48.21	F	F	F	194	194	194	A minimum of 20 m std.deviation is imposed on all formal errors of position fixes.
	2	5	379.79	668.01	910.60	40.73	147.29	38.73	F	F	F	190	190	190	
	3	10	387.38	582.25	914.76	21.06	43.65	23.13	F	F	F	180	180	180	
	4	20	385.90	587.24	918.17	15.05	25.11	20.64	F	F	F	160	160	160	
2	1	3	409.47	1,016.33	821.55	5.51	138.92	3.12	F	F	F	194	194	192	A minimum semi-minor axis (B) of 30 m is enforced on all formal error ellipses.
	2	5	379.87	647.99	819.21	2.09	9.69	2.82	F	F	F	190	190	188	
	3	10	383.05	582.44	820.96	1.56	3.69	2.05	F	F	F	180	180	178	
	4	20	386.49	585.40	820.77	1.21	2.40	2.06	F	F	F	160	160	158	
3	1	3	409.49	1,015.70	821.15	4.05	102.84	2.39	F	F	F	194	194	192	A minimum semi-minor axis (B) of 35 m is enforced on all formal error ellipses.
	2	5	379.88	648.21	819.11	1.54	7.21	2.17	F	F	F	190	190	188	
	3	10	383.06	582.34	821.00	1.15	2.74	1.59	F	F	F	180	180	178	
	4	20	386.45	585.52	820.67	0.89	1.79	1.61	P	F	F	160	160	158	
4	1	3	409.42	1,050.31	821.25	5.50	96.12	3.12	F	F	F	194	194	192	A minimum B of 30 m is enforced; with altitude, X-track and along track velocity errors modelled.
	2	5	379.84	658.64	819.21	2.09	6.77	2.82	F	F	F	190	190	188	
	3	10	383.08	584.67	820.96	1.55	2.83	2.05	F	F	F	180	180	178	
	4	20	386.50	589.42	820.76	1.21	1.67	2.06	F	F	F	160	160	158	

TABLE 10-1 (Continued)

TEST NO.	RUN NO.	NO. OF KNOTS	R.M.S. ERROR (m)			VARIANCE FACTOR			CHI-SQ. TEST			D.O. F.			COMMENTS AND CONDITIONS OF RUN
			TEST DATA SET NO.			TEST DATA SET NO.			TEST SET NO.			TEST SET NO.			
			1	2	3	1	2	3	1	2	3	1	2	3	
5	1	3	410.26	1,050.32	821.43	6.06	95.97	2.39	F	F	F	194	194	192	Minimum B = 30 m. Alt and velocity errors modelled. If satellite elev. > 88°, semi-major axis (A) is set to 3 km.
	2	5	380.08	658.73	819.43	2.17	6.69	2.08	F	F	F	190	190	188	
	3	10	383.37	584.86	821.43	1.57	2.76	1.24	F	F	P	180	180	178	
	4	20	386.54	589.88	822.14	1.19	1.59	1.17	F	F	P	160	160	158	
6	1	3	410.77	1,039.94	821.35	4.58	78.53	1.80	F	F	F	194	194	192	As in the above but with minimum B = 35 m.
	2	5	380.21	657.25	819.34	1.61	5.45	0.57	F	F	F	190	190	188	
	3	10	383.46	584.44	821.49	1.16	2.27	0.95	P	F	P	180	180	178	
	4	20	386.60	589.33	822.11	0.87	1.30	0.89	P	P	P	160	160	158	

10.3.2 Modelling Station Velocity Errors

Stansell [1978] gives the two possible components of a Transit fix error as being the inherent system errors (e.g. orbit and propagation errors) and errors caused by unknown receiver velocity during a satellite pass. The effect of such a velocity error remains as a complex function of satellite pass geometry and the structure of the error in velocity. The magnitude of velocity-caused errors is portrayed graphically in Figures 10-3 and 10-4. Under normal Transit use, the maximum satellite elevation acceptable for a fix computation is limited by this error.

However, in the vicinity of the North Pole, almost all passes have high elevation angles and unknown velocity-caused errors have hence to be contended with and accounted for in the a priori covariance matrix of the computed positions. The procedure used in an attempt to better model the influence of velocity errors, by modifying the a priori covariance matrix, is described below.

It is assumed that all Transit satellites have a 90 degree orbit inclination. This introduces a small error into the computed elevation angle. Using USNO [1979] data (April and July 1979), it can be shown that the maximum error caused by this assumption is within one to three degrees for all satellites except Satellite No. 30140. For Satellite No. 30140, due to its much larger departure from a 90 degree orbital plane inclination, the maximum possible error on the computed elevation angle is about five degrees.

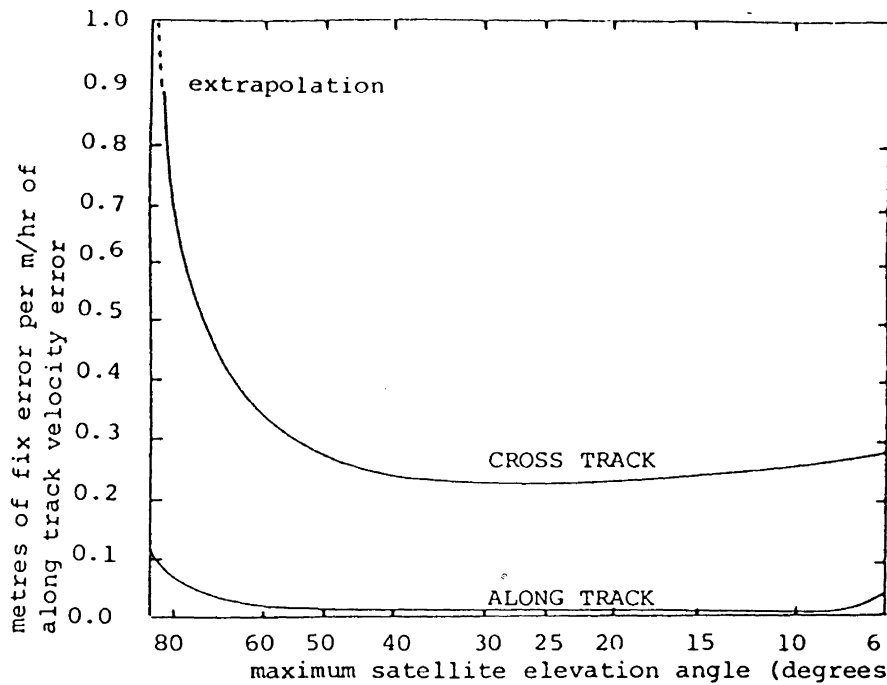


FIGURE 10-3 Sensitivity of satellite fix to a one metre per hour error in velocity in the along-track direction.

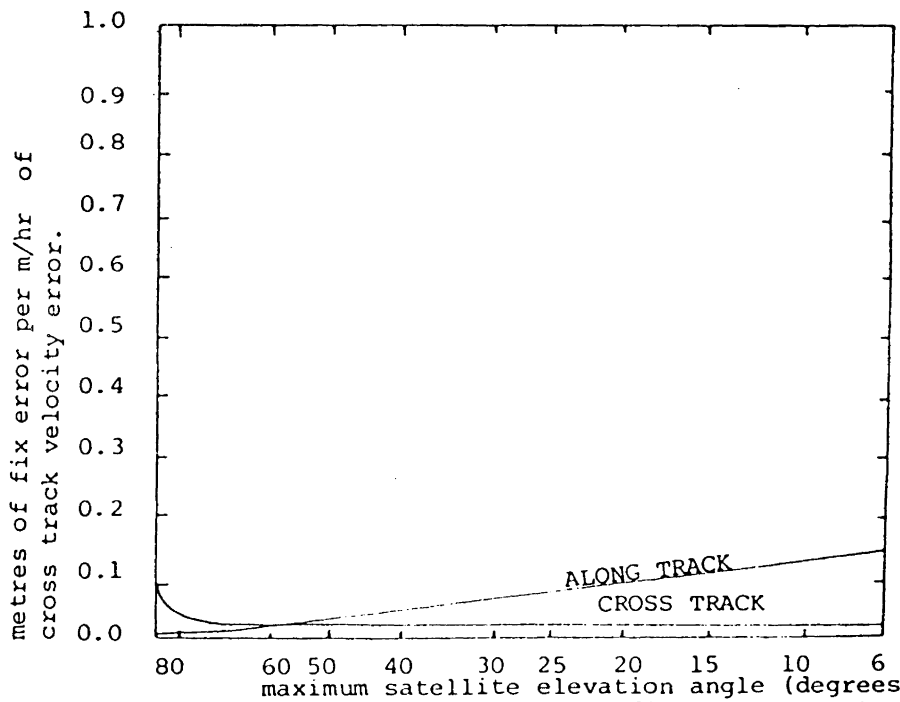


FIGURE 10-4 Sensitivity of satellite fix to a one metre per hour error in velocity in the cross-track direction.

The elevation angle for each fix is computed using the algorithm described in Appendix III. The direction of motion of the satellite at the time of closest approach (correct to within a few degrees) is derived from the formal error ellipse of the computed position. The semi-minor axis of the error ellipse lies in the along track direction of the passing satellite because the position fix is more precisely determined in the along track direction of the satellite than in the cross track direction.

The position fixes used in the test runs were computed on LOREX in real-time using predicted velocity vectors. Errors in the values of the predicted velocity vector (Figures 10-3 and 10-4) propagate into the computed position determinations.

At this point, the analytical expression underlying the curves in Figures 10-3 and 10-4 could be derived and used. However a simpler procedure is adopted here. The curves shown in Figures 10-3 and 10-4 are approximated by step functions and extrapolated towards the 90 degree elevation angle (as described in Table 10-2). The fact that the extrapolated figures might prove inadequate cannot be ignored. However, can a reliable estimate of the cross track position be estimated with satellites having elevation angles of greater than 88 degrees (termed here as "high elevation" satellites)? A move towards answering this question is made by treating all passes with a maximum

TABLE 10-2
STEP FUNCTIONS APPROXIMATING THE FIX ERROR DUE TO
VELOCITY AND HEIGHT ERRORS.

The following are the step functions used in approximating the Figures 10-3, 10-4 and 10-5, divided into cross track and along track directions of the observed satellite.

I) Cross Track Error Components

Satellite elevation angle (e in degrees)	Fix error in metres
a) Errors due to an estimated velocity north error (Vn)	
e < 75	0.45*Vn
75 < e <= 80	0.56*Vn
80 < e <= 84	0.62*Vn
84 < e <= 85	1.00*Vn
85 < e <= 88	1.20*Vn
e >= 88	1.50*Vn
b) Errors due to an estimated velocity east error (Ve)	
e < 80	0.03*Ve
80 < e <= 85	0.05*Ve
85 < e <= 87	0.09*Ve
e >= 87	0.12*Ve
c) Errors due to an estimated height error (H)	
e < 75	3.30*H
75 < e <= 80	4.20*H
80 < e <= 83	5.60*H
83 < e <= 85	7.20*H
85 < e <= 86	10.00*H
e >= 86	15.00*H

II) Along Track Error Components

Satellite elevation angle (e in degrees)	Fix error in metres
a) Errors due to an estimated velocity north error (Vn)	
e < 75	0.03*Vn
75 < e < 80	0.04*Vn
80 < e < 83	0.08*Vn
83 < e < 85	0.09*Vn
85 < e < 87	0.10*Vn
e > 87	0.13*Vn
b) Errors due to an estimate velocity east error (Ve)	
e < 80	0.02*Ve
80 < e < 85	0.15*Ve
e > 85	0.10*Ve
c) Errors due to an estimate height error (H)	
e < 75	0.25*H
75 < e < 80	0.35*H
80 < e < 85	0.50*H
85 < e < 87	0.75*H
e > 87	1.00*H

The root sum square (rss) fix errors, in both cross track and along track directions, are defined as being the square root of the sum of squares of the computed fix errors from the three error sources described above. For example,

$$\text{rss}(\text{cross track}) := \sqrt{a^2 + b^2 + c^2}$$

where a, b and c are the estimated fix errors computed using the step functions Ia, Ib and Ic respectively.

[Reference: Stansell 1978: pages 72, 73 and 68]

satellite elevation angle of greater than 88 degrees as line fixes (or position fixes with very elongated ellipses). The term "line fix" is used to denote a computed position with a formal error ellipse having a semi-major axis of greater than 3000 metres.

10.3.3 Modelling Height Errors

Also considered are the errors in the computed position due to an error in the assumed station height. When using high elevation satellites (as defined in Section 10.3.2), height errors, as shown in Figure 10-5, can cause a substantial error in the computed position. Popelar et al. [1981] in their post-processing of the LOREX navigation data sets arrived at an average figure of around eight metres for the station ellipsoidal heights.

This is different from the assumed height of the stations used in the fix computations on LOREX by 12 metres.

10.3.4 Combined Effects on the Formal Covariance Matrix

Using the above information, the contribution from each of the error sources, described in Section 10.3.1, 10.3.2 and 10.3.3, are evaluated. The resulting root sum square error (rss) (obtained from the position errors due to velocity and height errors - Table 10-2), divided into along and cross track components, replaced the semi-minor and semi-major axes of the formal error ellipse from the fix

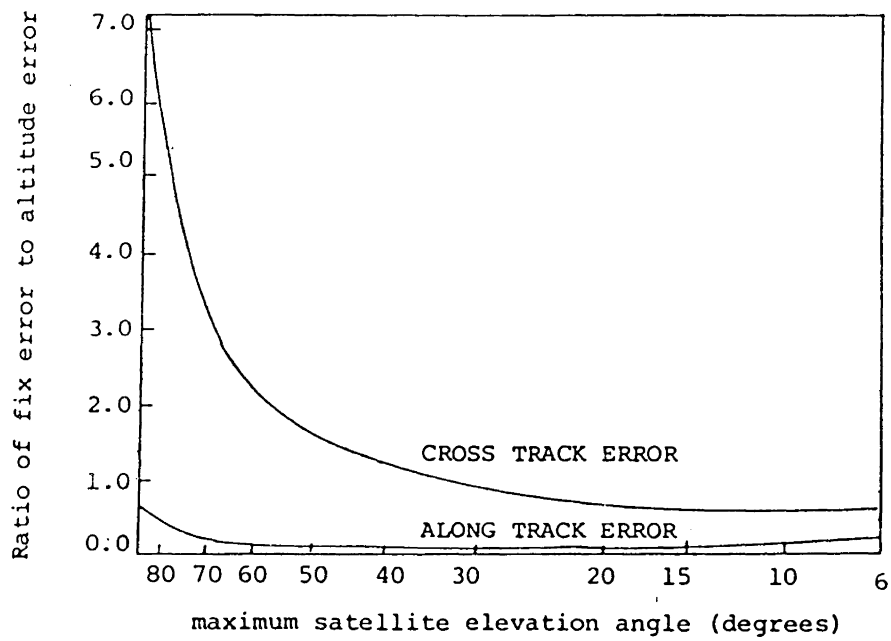


FIGURE 10-5 Sensitivity of satellite fix to station altitude estimate error

computation (subroutine ERRORS in Appendix VII) whenever these were below the rss figures. Test No. 4 of Table 10-1 used this modification to achieve a further improvement in the variance factor. The maximum effect, as expected, is shown by the test data set describing the fastest motion of station (i.e. test data set two).

To evaluate the effect of treating position fixes computed from high elevation satellites as line fixes (defined in 10.3.2), all position fixes computed with high elevation satellites had the semi-major axis of their error ellipses set to 3000 metres. The outcome of this experiment (Table 10-1, Test Runs Nos. 5 and 6) agrees with the notion that the cross track position determinations using high elevation satellites are extremely poor. The improvement in the variance factor increases as the station get nearer to the pole. This can be expected as test data set three has more position fixes with high elevation satellites (55 percent of test data points) than test data set two (14 percent) or test data set one (7 percent). In addition, the examination of the predicted covariance matrices for the smoothed points (in test data set three) revealed an average drop around 22 percent in the variances of the position coordinates (the actual figures range from -14 percent to 25 percent).

Since the spline model for all the three test data sets passes the Chi-squared tests when the revised a priori

covariance matrices is used (Table 10-1, Test No. 6), these revised matrices can be assumed to aptly reflect the accuracy of the observed position fixes. For the spline algorithm and indeed any weighted smoothing technique, this condition must be fulfilled.

The time series of predicted positions for each of the three test data sets (Table 10-1, Test No.6) are given in Figures 10-6 to 10-14.

10.4 REAL-TIME APPLICATION

The near real-time application of the algorithm developed in this thesis would involve the processing of the observed data series in consecutive data spans. As described in Section 9.5, a minimum overlap of two knot intervals is required to ensure continuity. The estimated second last knot vector of the former spline, along with its covariance matrix, is used as the weighted a priori beginning knot vector for the latter spline.

The processing of the Doppler data from the three ice camps on the LOREX-79 expedition proceeded in a manner similiar to that described above. Real-time position determinations using the Transit satellite system over variable time spans (depending on the motion of the station and the resulting number of knots) are used by DSPLIN to produce smoothed estimated paths of the drifting ice

FIGURE 10-6 SMOOTHED THREE HOUR POSITIONS WITH ESTIMATED ERROR
ERROR ELLIPSES AT THE 99% CONFIDENCE LEVEL
TEST DATA SET ONE

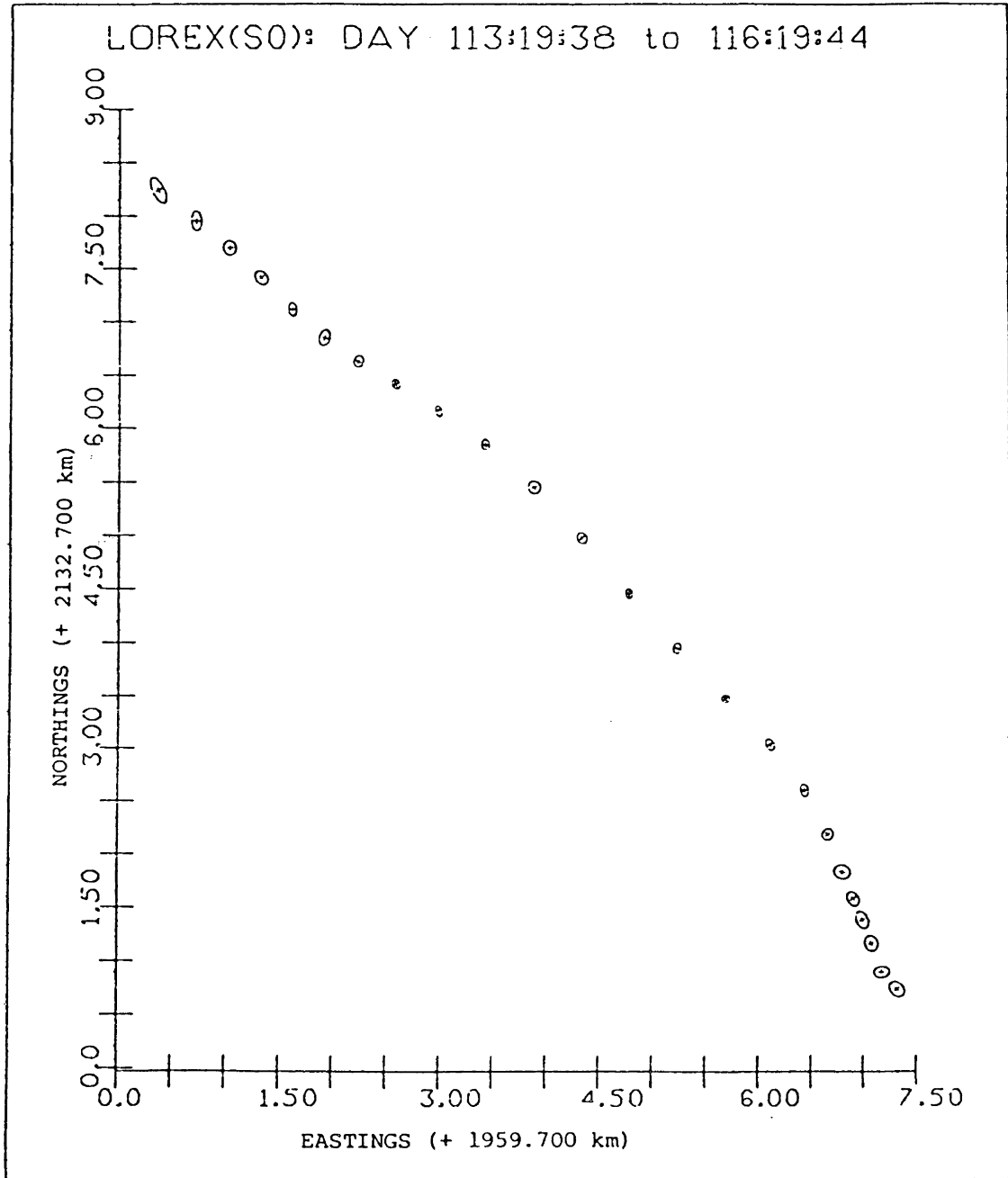


FIGURE 10-7 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET ONE

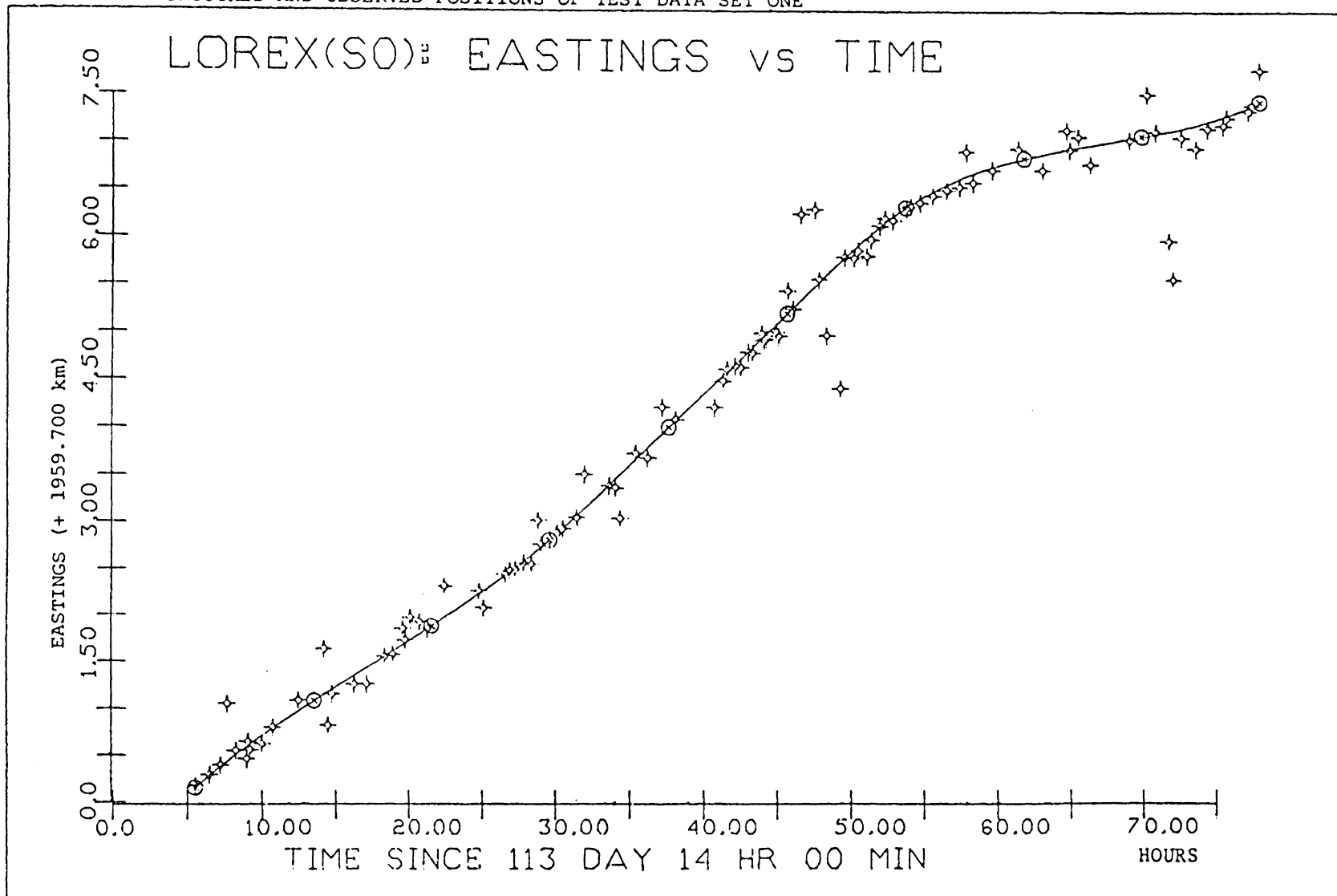


FIGURE 10-8 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET ONE

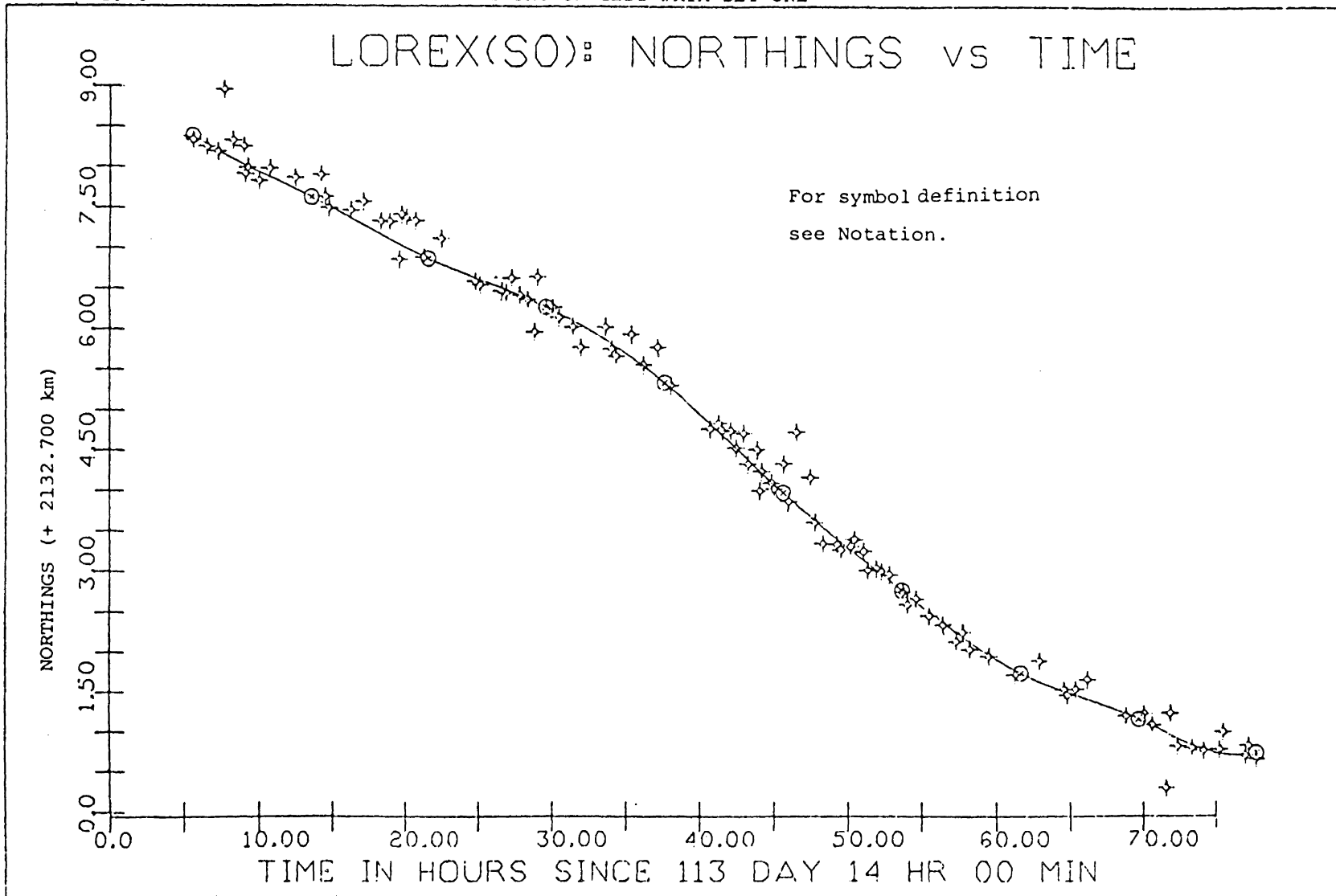


FIGURE 10-9 SMOOTHED THREE HOUR POSITIONS WITH ESTIMATED ERROR

ELLIPSES AT THE 99 % CONFIDENCE LEVEL

TEST DATA SET TWO

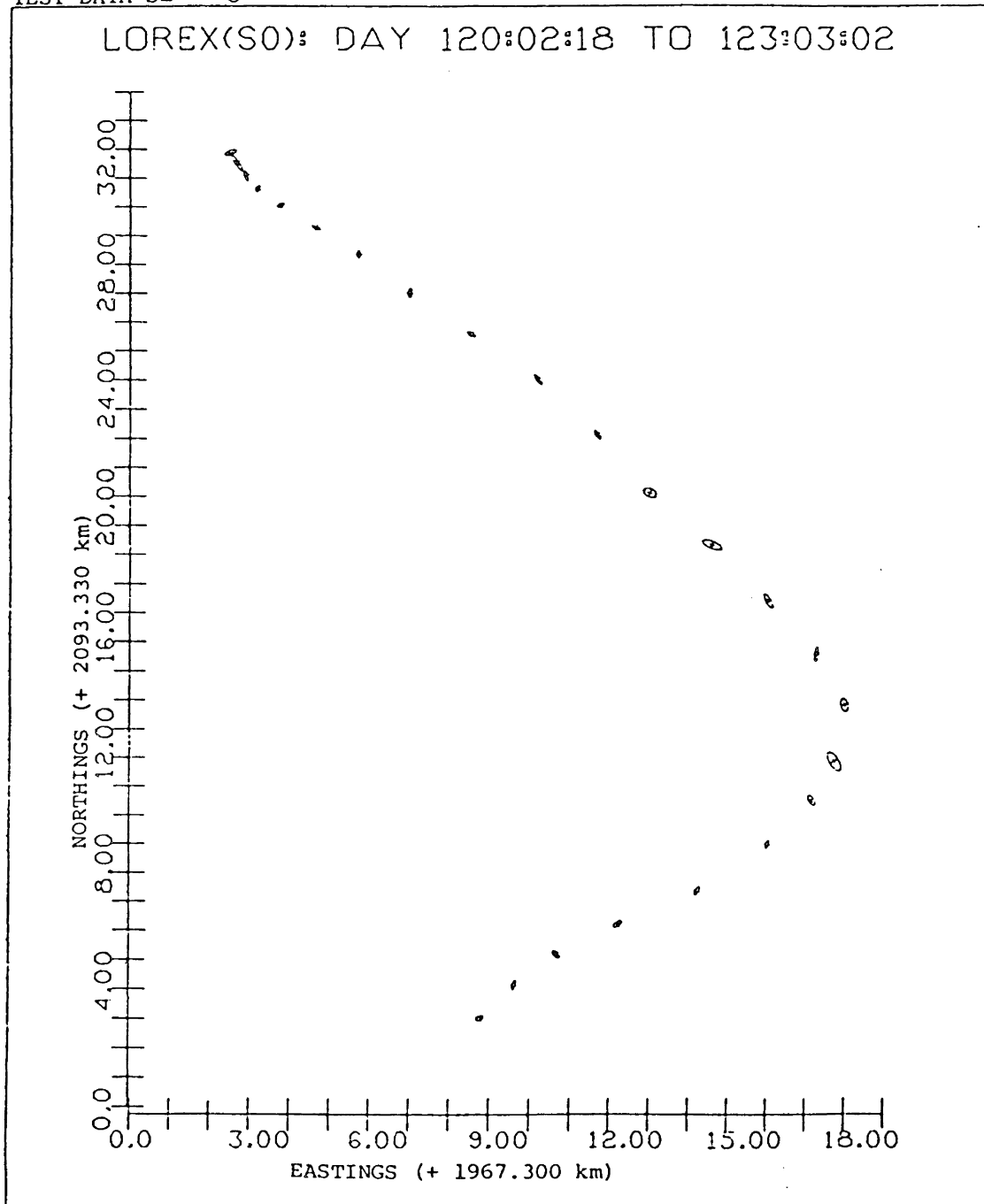


FIGURE 10-10 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET TWO

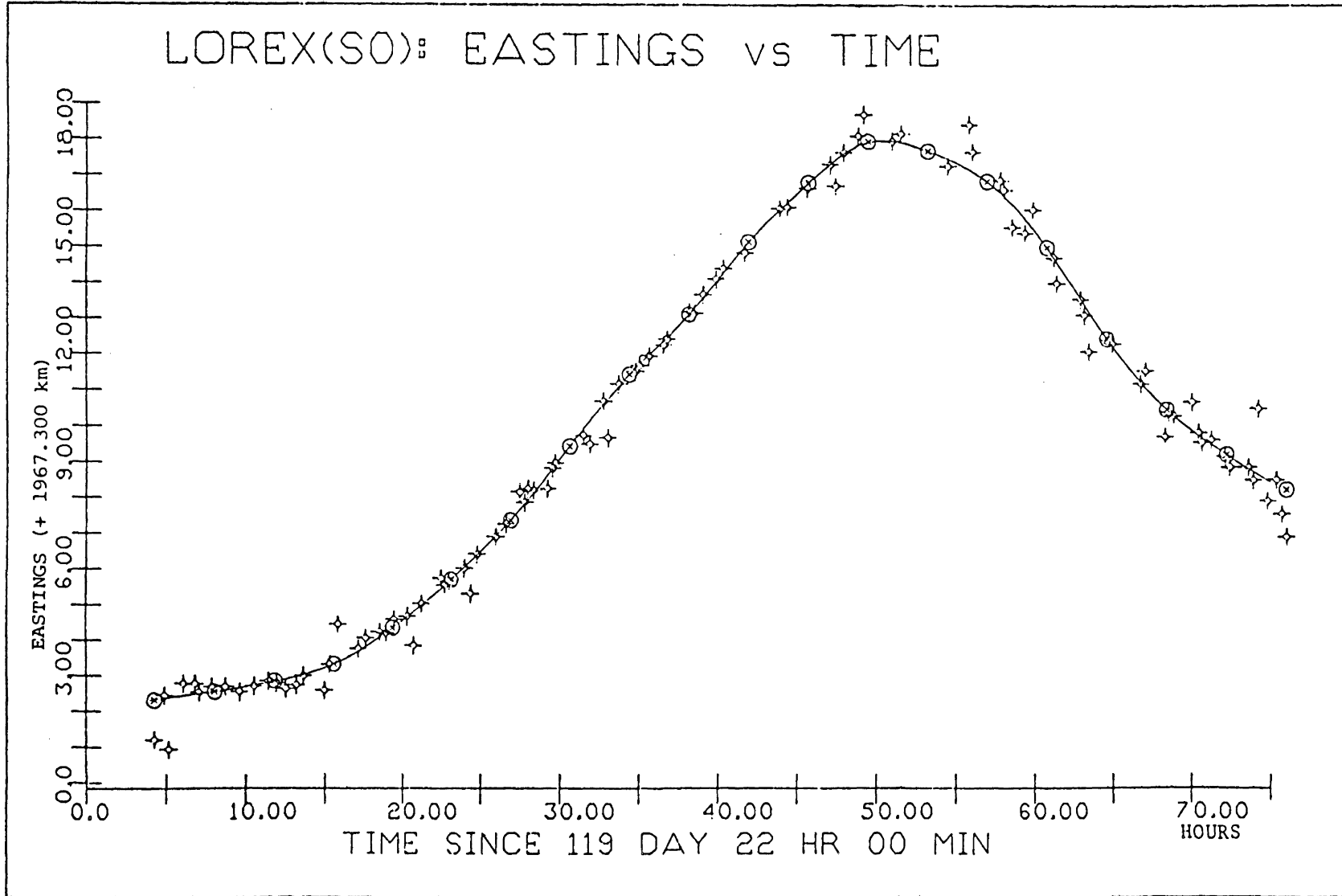


FIGURE 10-11 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET TWO

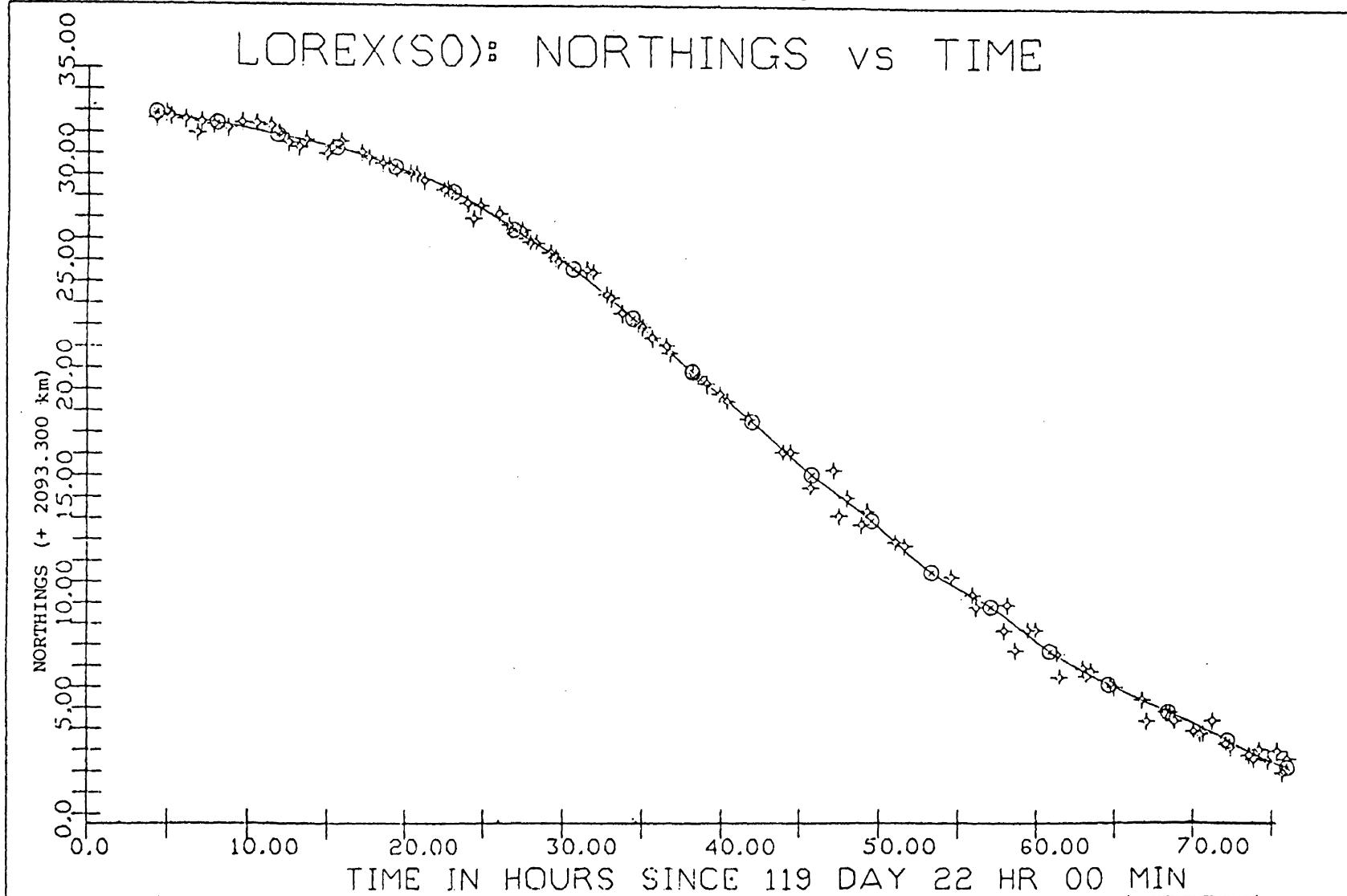


FIGURE 10-12 SMOOTHED THREE HOUR POSITIONS WITH ESTIMATED ERROR
ELLIPSES AT THE 99 % CONFIDENCE LEVEL

TEST DATA SET THREE

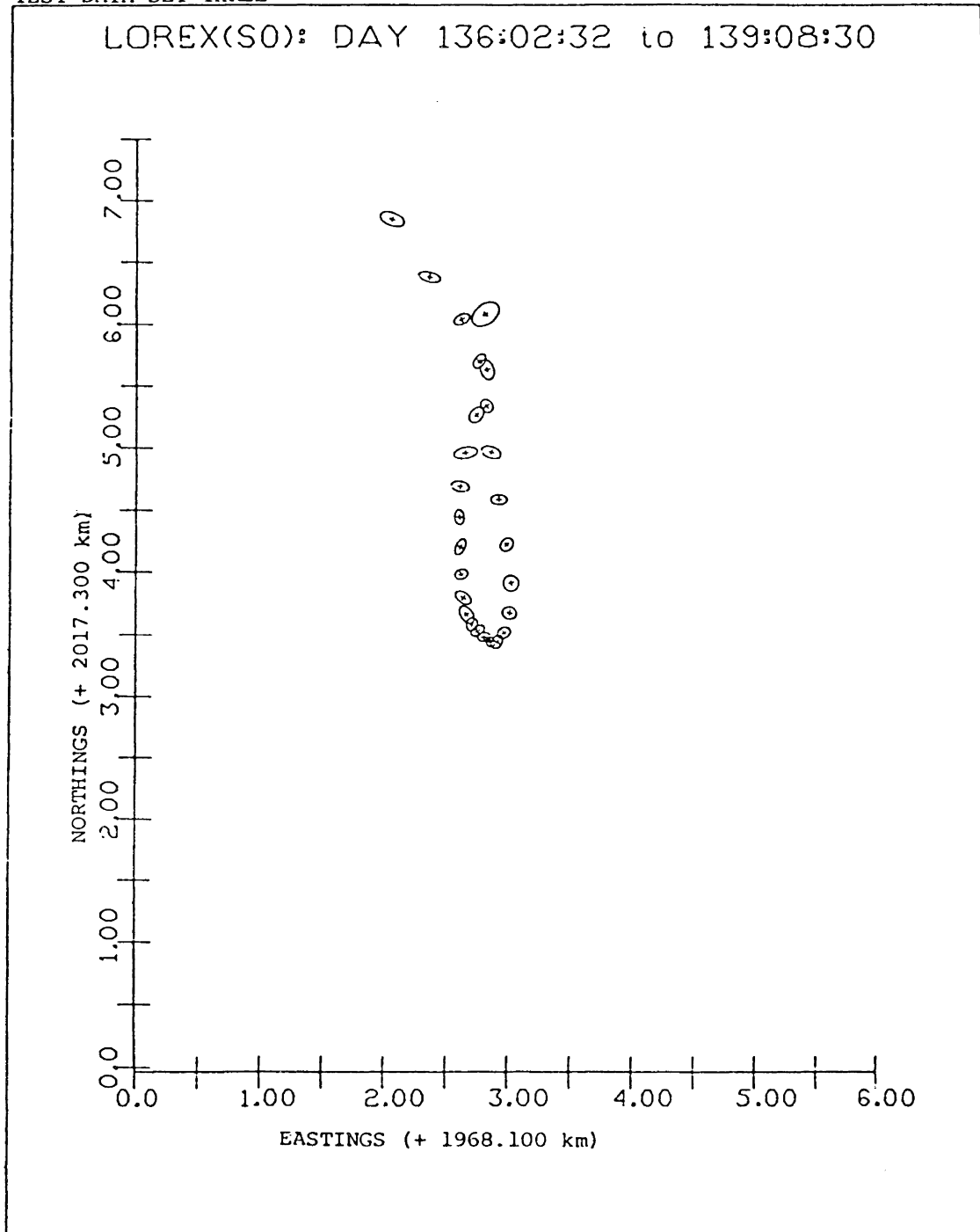


FIGURE 10-13 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET THREE

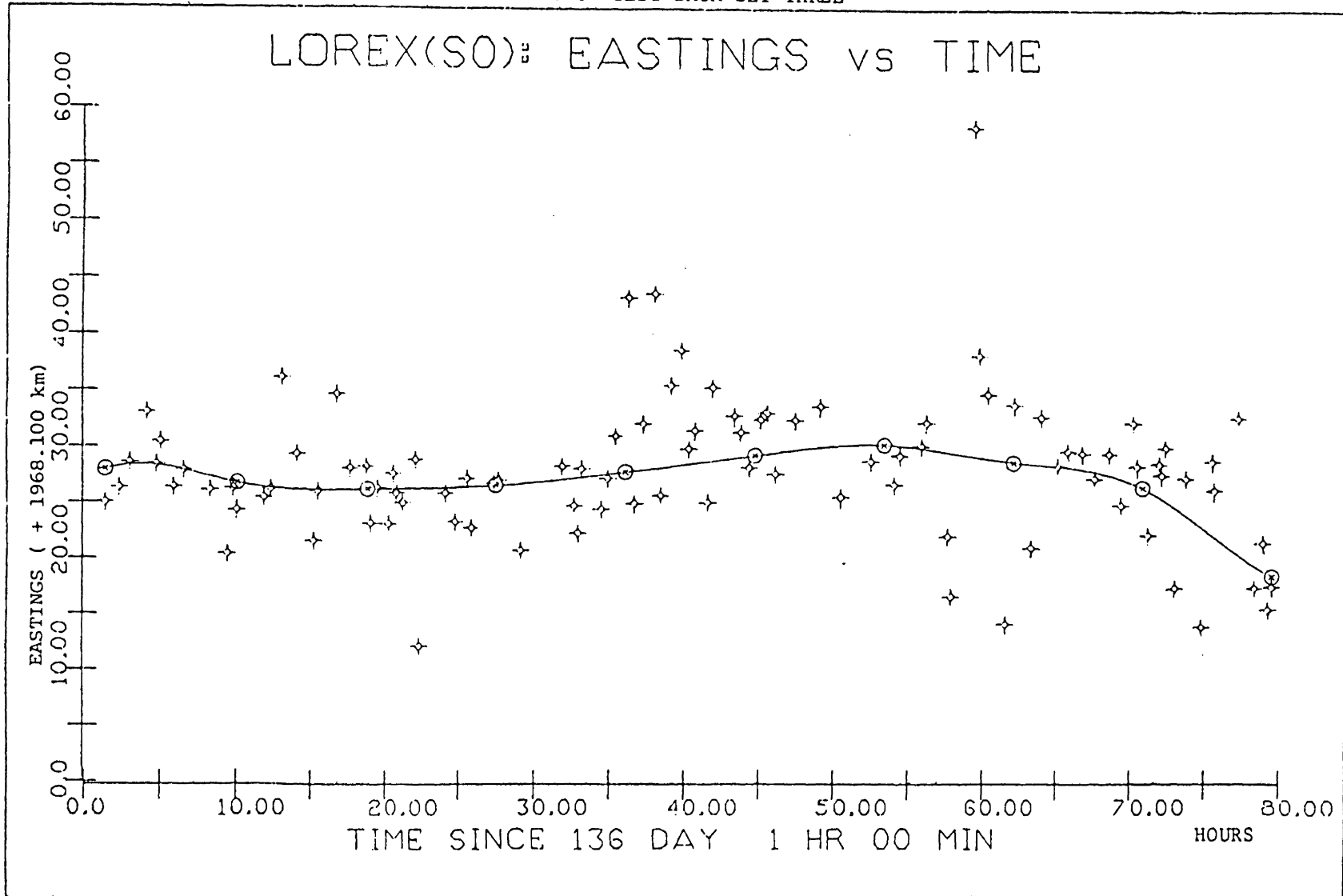
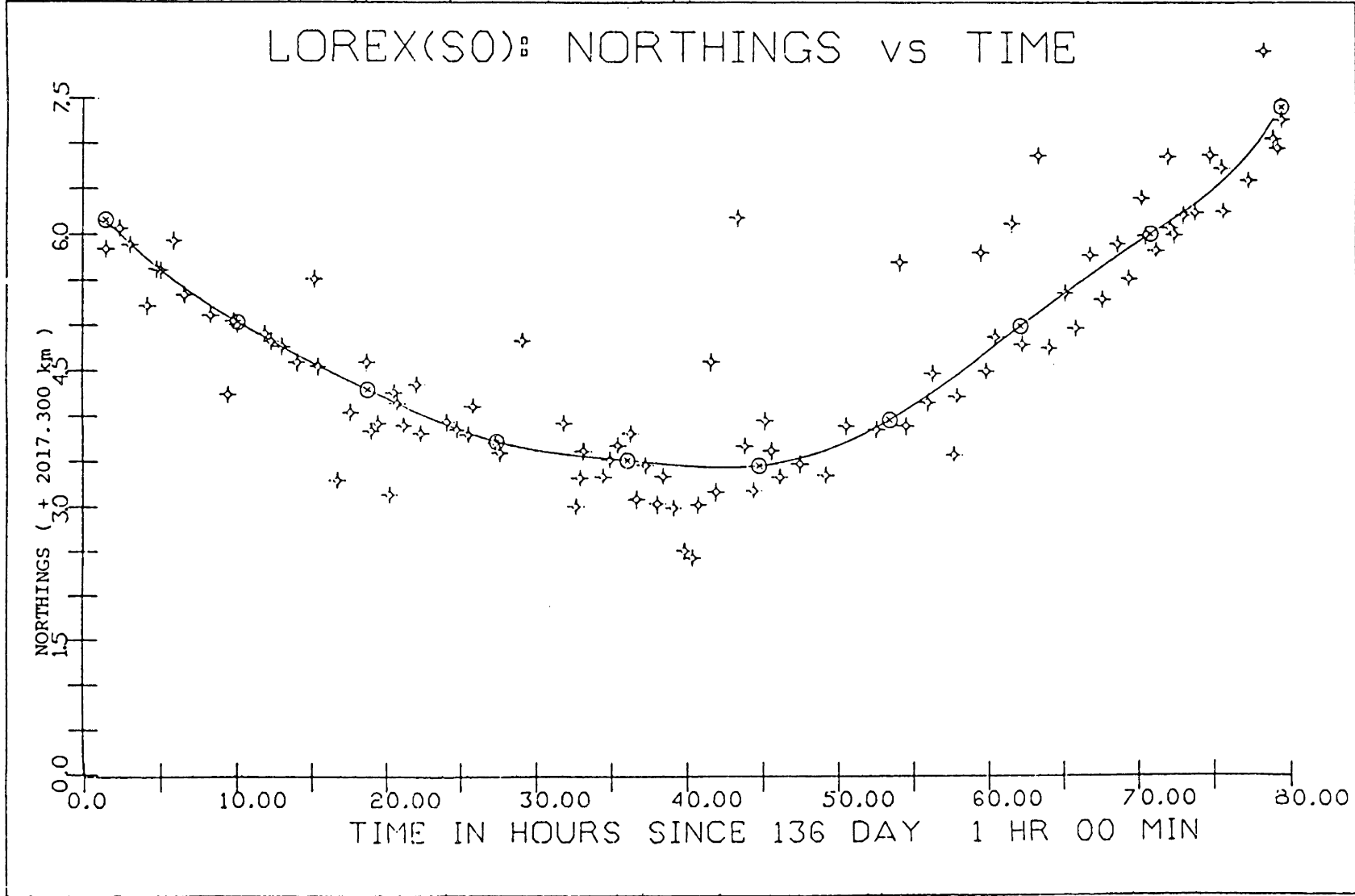


FIGURE 10-14 SMOOTHED AND OBSERVED POSITIONS OF TEST DATA SET THREE



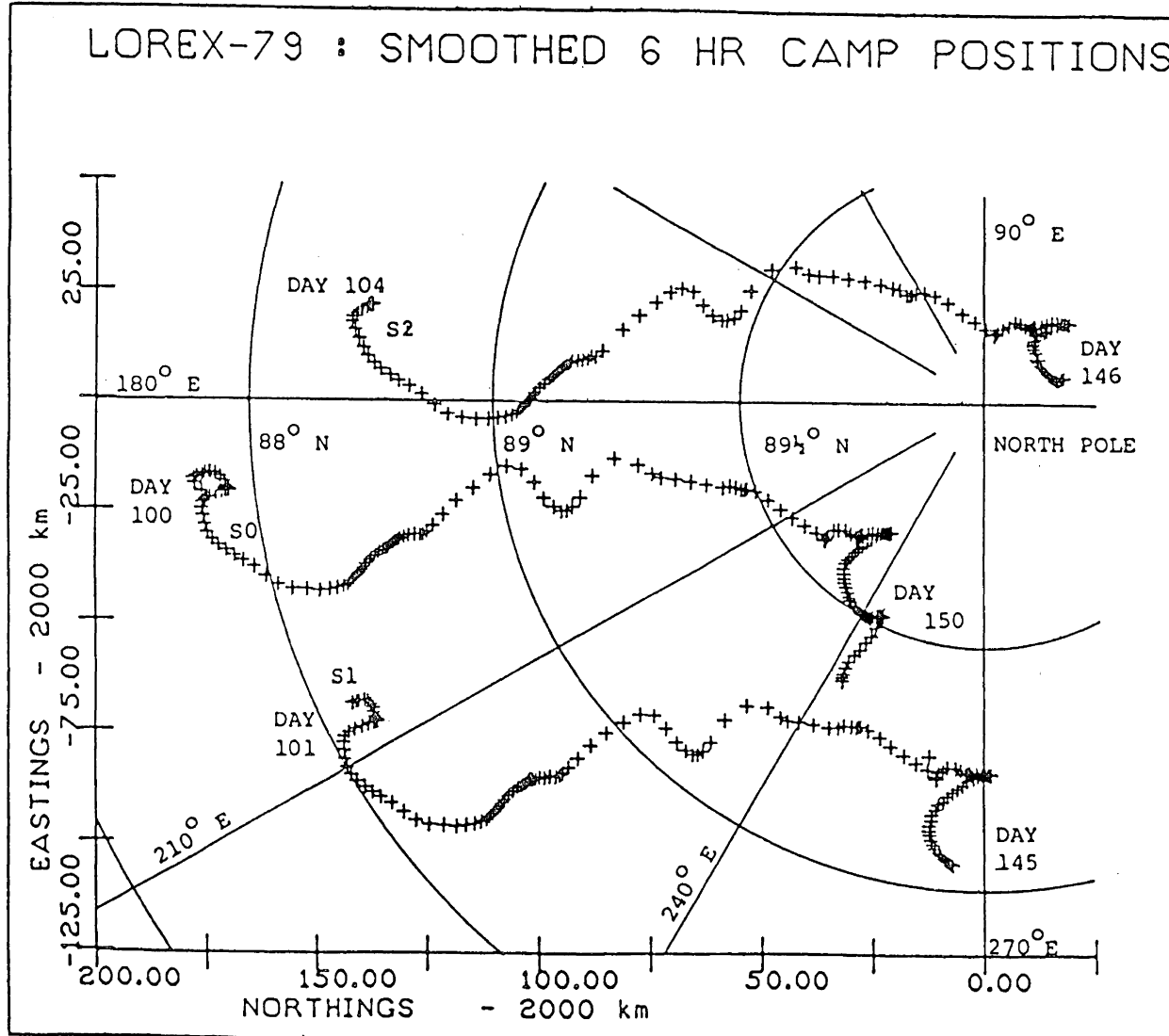
stations. The length of the data series of positions used in the computation of each spline is dependent upon the maximum number of knots that the computer program can handle at any one time. Implications of increasing the upper limit of the number of knots is discussed in Section 10.5.

10.5 PROCESSING OF LOREX-79 DOPPLER POSITIONING DATA

In this section, the complete processing of the positioning data series from the three camps on the LOREX expedition using DSPLIN is described and discussed.

The series of computed real-time position determinations, using the Transit system, for the camps are used as input to the spline algorithm (Figure 10-1) to generate smooth paths for the stations during the period of the expedition (Figure 10-15). The smoothed velocity vectors of the three stations are extracted from the estimated knot vectors of the spline (Figures 10-16 to 10-19). Each of the station's navigation data series is divided into several subsets as there exists a limit to the number of knots the computer program can handle for any given series. Currently, DSPLIN (Appendix VII) has an upper limit of 32 knots. Increasing the maximum number of knots within the program is not desirable as it increases both the random access memory array storage requirements of the program and the execution time in computing the much larger inverses.

FIGURE 10 - 15



LOREX Station Velocity Plots

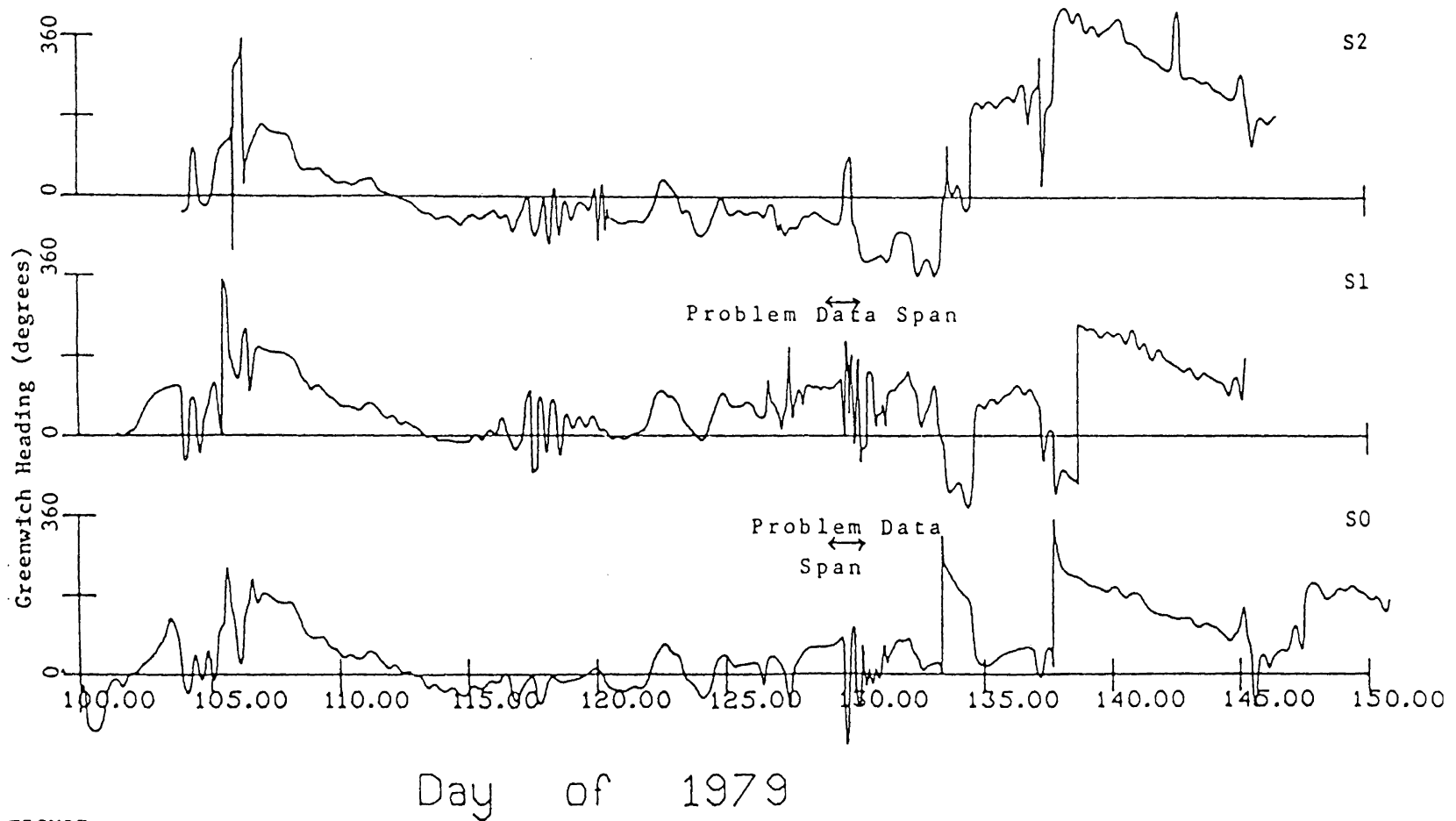


FIGURE 10-16

LOREX Station Velocity Plots

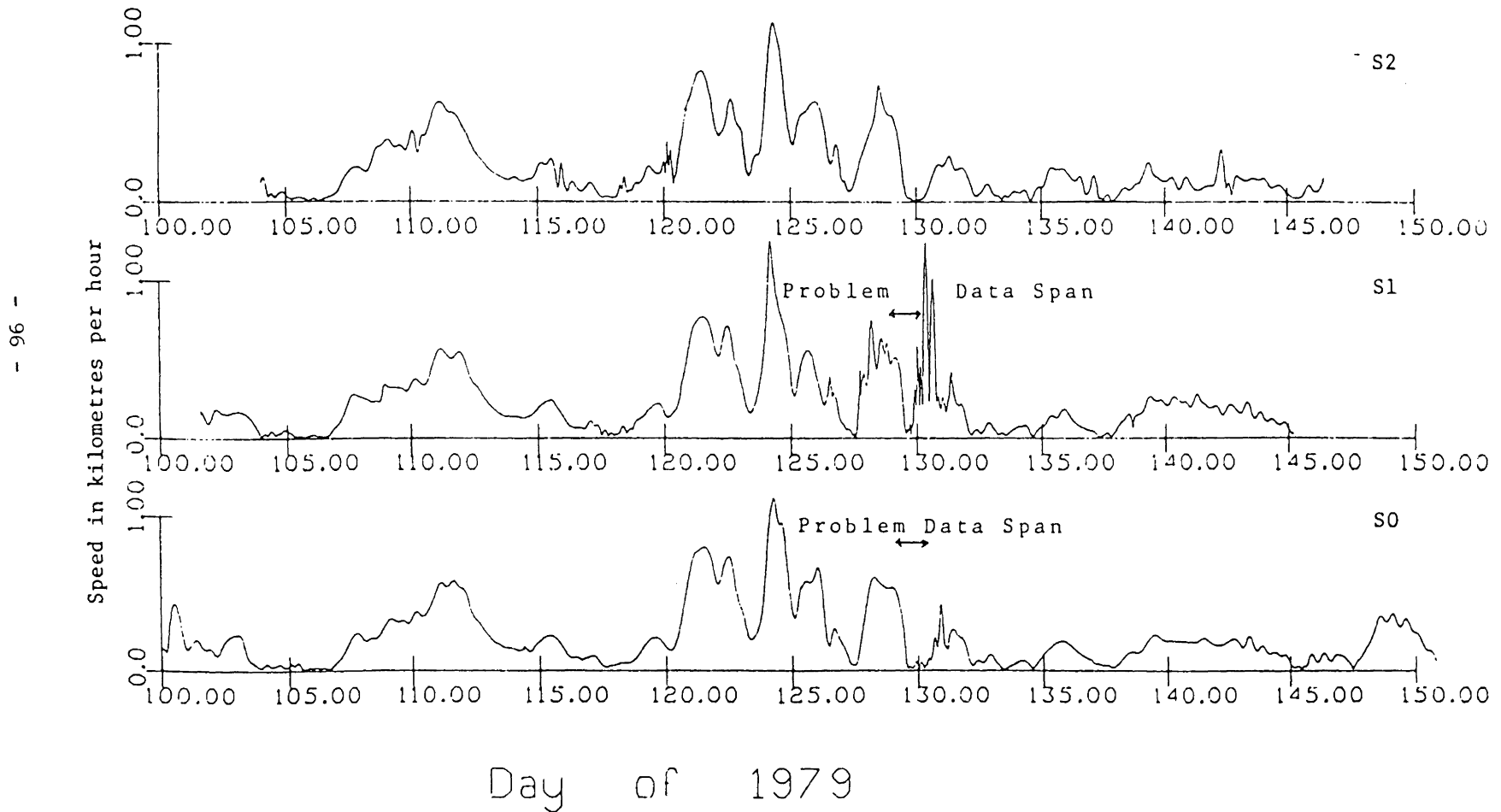
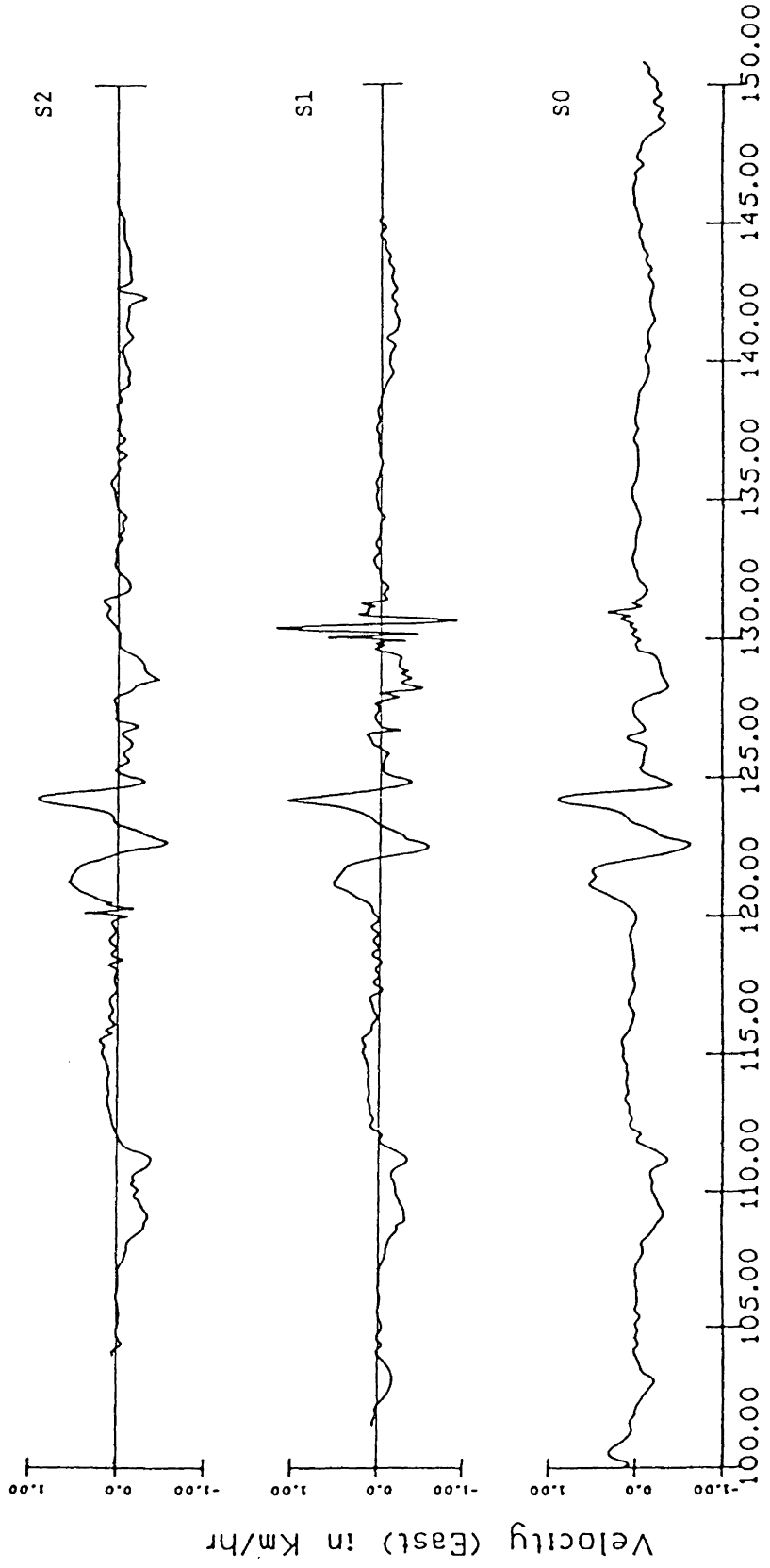


FIGURE 10-17

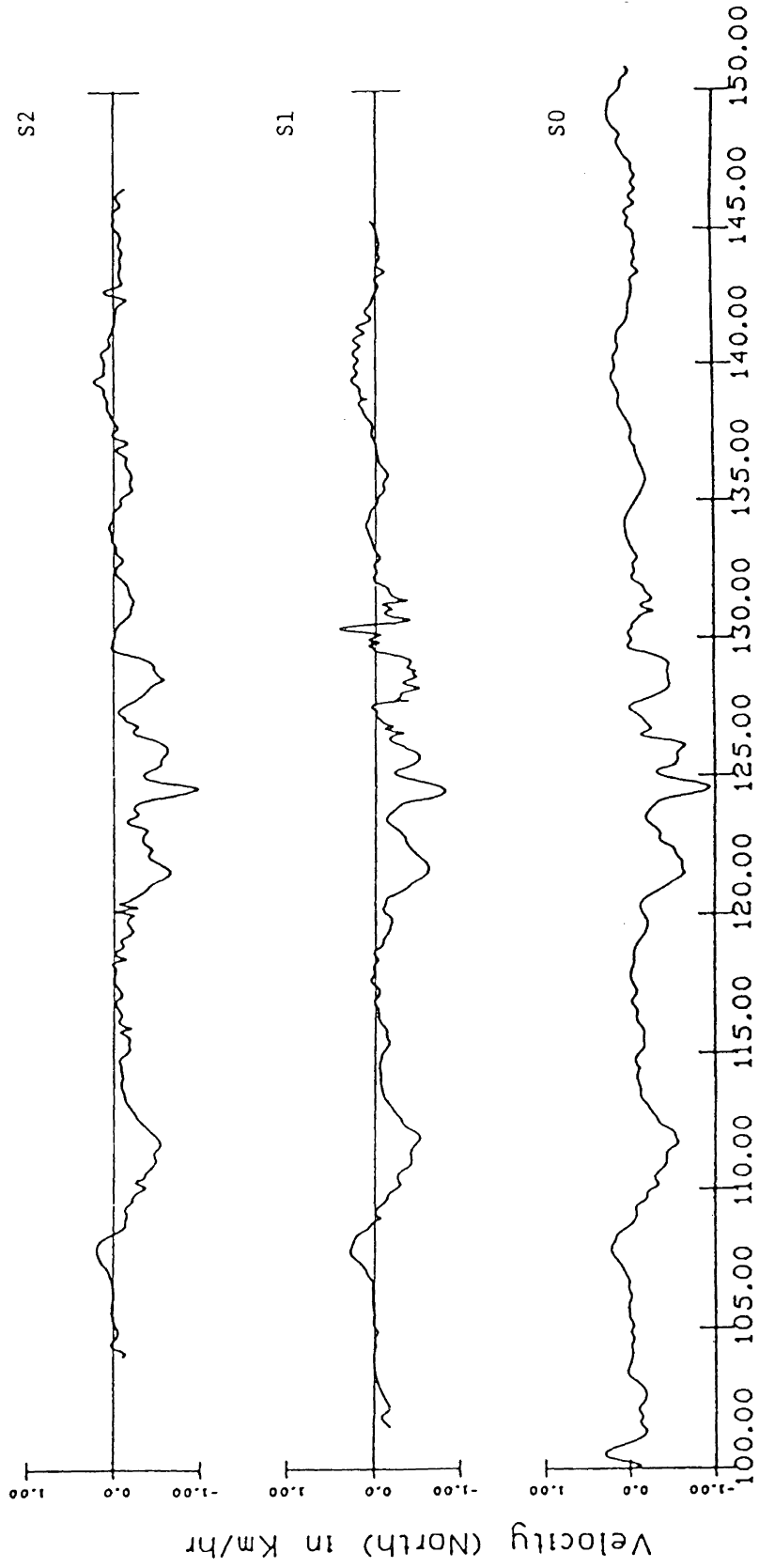
LOREX Station Velocity Plots



Day of 1979

FIGURE 10-18

LOREX Station Velocity Plots



Day of 1979

FIGURE 10-19

The LOREX Doppler positioning data sets for ice camps S0, S1 and S2 were divided into 9, 8 and 7 subsets respectively.

10.5.1 Problem Data Spans

All subsequent splined subsets, with the exception of two, have a posteriori variance factors which pass the Chi-squared statistical test (Section 7.3.1). The exceptions occur in the LOREX data series from station S0 and station S1, and are both around the same time period (i.e. between day 129 to day 131). This phenomenon is absent in the data series from station S2, possibly due to the much lower sampling period of position fixes at station S2.

One of the subsets, as identified above, a data span in the data series from station S0, was subjected to a number of tests in an effort to determine the reason for the failure of the spline model (computed from the data contained in the subset of the data series) to pass the Chi-squared test. The following were investigated:

1. Error in the value of the minimum semi-minor axis of the error ellipses adopted. The selected value of 35 metres (see Section 10.3.1) was gradually increased and the subset model passed the test when a value of 80 metres was reached. The value of 80 metres as the minimum value for the semi-minor axis of the error ellipses greatly reduces the assigned accuracy of all position determinations; including good position fixes.

2. Error in either the value of the cutoff angle for the elevation (i.e. 88 degrees - Table 10-1) of the satellite in the treatment of the position fix as that of a line fix (as defined in Section 10.3.2) or the assigned value of the semi-major axis of the elongated error ellipse constituting a line fix. Results show that changes in the value of the cutoff elevation angle (from 88 to 85 degrees) or the assigned cross track error (increased from 3000 m to 5000 m) did not make any significant change in the a posteriori variance factor.

From the results above, the following are the conclusions drawn about the inability of the a posteriori variance factor of the two data subsets to pass the Chi-squared statistical test.

Firstly, the sampling period, the average time between position fixes, may be inadequate to define the motion of the ice platform during periods of rapid ice movements. Secondly, the fact that here, the effect of velocity-caused errors in the computed positions are modelled simply by expanding the a priori covariance matrix. This may have two defects: inadequacy of the error models to expand the covariance matrices, and the problem that the velocity-caused errors (which are essentially position biases) are modelled as a random effect. The observation period for

each satellite pass is about 18 minutes. During this period, any variation in speed and direction of the motion of the receiver will affect the observed Doppler counts and the resulting position computations. The effect of short term variations in speed and direction on the position determinations have not been investigated and can be safely neglected because changes in the velocity vector of the receivers on LOREX, due to the inertia of the ice sheet, would be negligible over the short 18 minute interval.

Predicted speeds and directions, constant over a certain period of time, were used in computing the position fixes. Figure 10-20, which compares the real-time predicted velocity vectors with the final smoothed values from DSPLIN, highlights the errors that can exist in the estimated real-time velocity vectors used in the fix computation. A reduction of these errors would have been possible through a pre-processing algorithm which produces better velocity vector estimates (as illustrated in Figure 10-1 with the spline being used as the pre-processing algorithm) for the recomputation of the position fixes.

The final smoothed path of the three ice stations are portrayed in Figure 10-15. Figures 10-16 to 10-19 give the smoothed velocity vectors of the three ice stations for the duration of the expedition. The differences between the smoothed positions, velocities and directions produced by the spline algorithm and those obtained using GEODOP (see Section 2.2) are given in the following section.

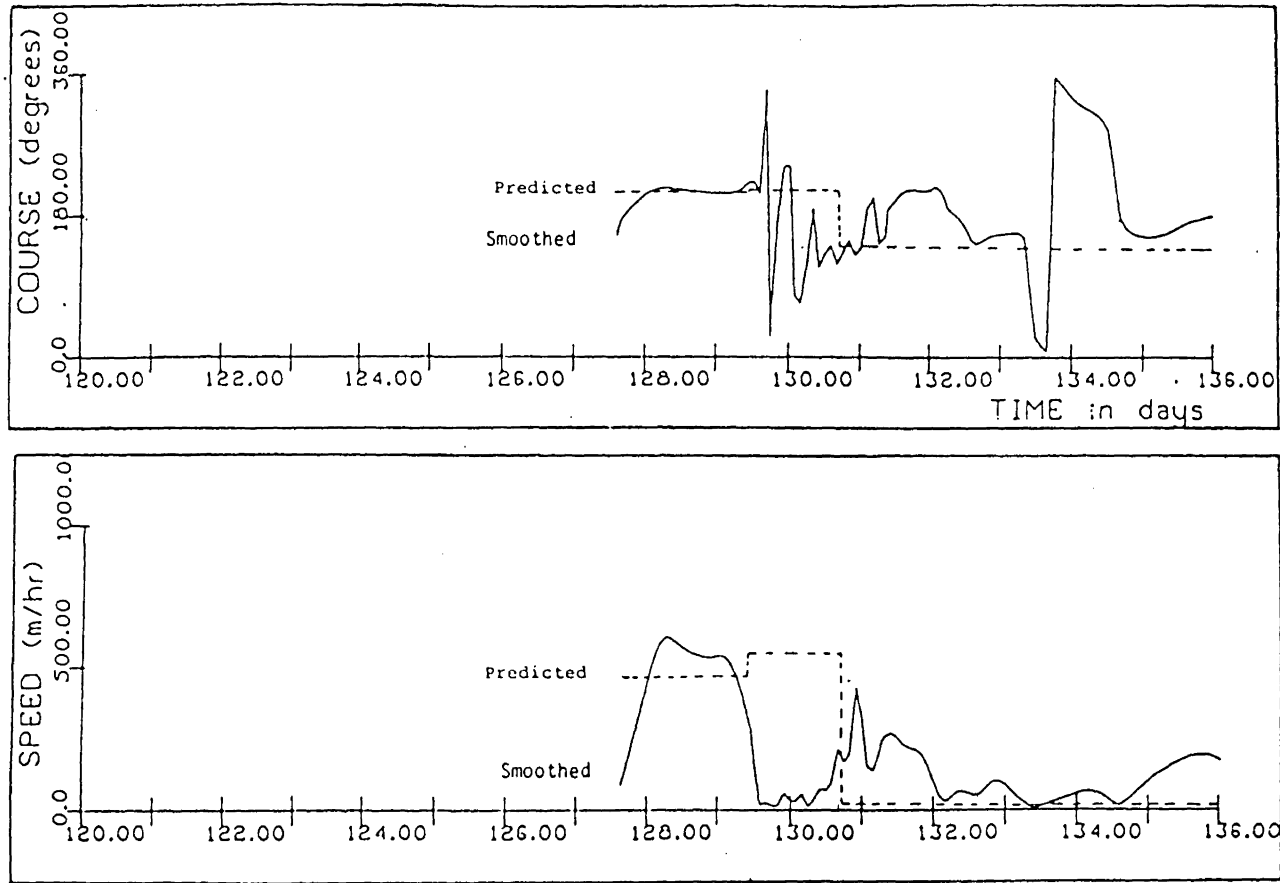


FIGURE 10-20 The real-time predicted and smoothed velocity vectors for station S0.

10.6 COMPARISON WITH OTHER TECHNIQUES

In this section, the six-hour smoothed positions and velocities for the three ice camps produced by DSPLIN, SMOBS and GEODOP are compared. A brief description of SMOBS and GEODOP can be found in Section 2.2. The procedure followed for LOREX data processing by DSPLIN is given in Figure 10-1.

The position and velocity information produced by GEODOP, computed from better orbital and environmental models and recomputed position fixes based on precise satellite orbits in the multi-station three-dimensional adjustment mode (see Section 2.2), are taken as the reference standard for the comparisons. The comparison between DSPLIN and GEODOP was made to determine the following:

1. Accuracy of the recovered positions and velocities.
2. Consistency of recovered positions and velocities with time.
3. Consistency of estimated precision of position and velocity estimates with accuracy.

Differences between SMOBS and GEODOP are also evaluated and compared with DSPLIN versus GEODOP differences. The following are computed in the comparison between the technique and the adopted reference (GEODOP).

1. Position deviations (i.e. Δr_i).

$$\Delta r_i := [(\vartheta_i^R - \vartheta_i)^2 + (\lambda_i^R - \lambda_i)^2]^{1/2} \quad - (10-1)$$

2. Velocity deviations (i.e. Δv_i).

$$\Delta v_i := [(v_{Ni}^R - v_{Ni})^2 + (v_{Ei}^R - v_{Ei})^2]^{1/2} \quad - (10-2)$$

where ϑ, λ := geodetic latitude and longitude E,
 v_N, v_E := velocity north and velocity east,
 i := data point number,
 and R := reference standard.

3. Standard deviations of position ($\sigma_{\Delta r_i}$) and velocity ($\sigma_{\Delta v_i}$)

differences computed using the covariance law

(Section 8.1), i.e.

$$\sigma_{\Delta r_i}^2 := [\Delta \vartheta_i^2 (\sigma_{\vartheta_i}^2 + \sigma_{\vartheta_i}^{R2}) + 2\Delta \vartheta_i \Delta \lambda_i (\sigma_{\vartheta_i \lambda_i} + \sigma_{\vartheta_i \lambda_i}^R) + \Delta \lambda_i^2 (\sigma_{\lambda_i}^2 + \sigma_{\lambda_i}^{R2})] / \Delta r_i^2$$

$$\sigma_{\Delta v_i}^2 := [\Delta v_{Ni}^2 (\sigma_{vNi}^2 + \sigma_{vNi}^{R2}) + 2\Delta v_{Ei} v_{Ni} (\sigma_{vNE_i} + \sigma_{vNE_i}^R) + \Delta v_{Ei}^2 (\sigma_{vEi}^2 + \sigma_{vEi}^{R2})] / \Delta v_i^2$$

- (10-3)

where $\Delta \vartheta, \Delta \lambda$:= differences in latitude and longitude,
 $\sigma_{\vartheta}, \sigma_{\lambda}$:= std. deviations of position coordinates,
 $\sigma_{\vartheta \lambda}$:= covariance between coordinates,

$\Delta v_N, \Delta v_E$:= differences in velocity north and east,
 σ_{vN}, σ_{vE} := std. deviations of velocity north and east,
 σ_{vNE} := covariance between velocity components.

4. Standardised deviations of positions and velocities.

$$\tilde{\Delta r}_i := \Delta r_i / \sigma_{\Delta r_i}$$

$$\tilde{\Delta v}_i := \Delta v_i / \sigma_{\Delta v_i} \quad - (10-4)$$

Ideally, all the above parameters (defined by equations 10-1 to 10-4) should be computed and plotted against time to evaluate their consistency in time. However, as shown in Table 10-3, much of the required data is absent. This is partly due to the technique itself (e.g. SMOBS does not have individual precision estimates for mean positions), and partly by the omission of information in the program outputs (e.g. the correlation coefficients in GEODOP positions are not printed).

The following comparisons were those that could be readily done with the available information.

1. Computation of absolute position and velocity differences.

These differences are computed in both comparisons, i.e. DSPLIN versus GEODOP and SMOBS versus GEODOP. The set of differences (or deviations) are plotted against time (Figures 10-21 and 10-22). The cumulative distributions, obtained from reordering the position and velocity deviations (equations 10.1 and 10.2), are also plotted (Figure 10-23).

TABLE 10-3

SUMMARY OF POSITION AND VELOCITY INFORMATION
PRODUCED BY GEODOP, SMOBS AND DSPLIN

I) Position Estimates

Program Name	Latitude or Northing	Longitude or Easting	Standard Deviations and covariances		
			σ_1	σ_2	σ_{12}
GEODOP	Both	Both	σ_{lat}	σ_{long}	No
SMOBS	Northing	Easting	No	No	No
DSPLIN	Northing	Easting	σ_N	σ_E	σ_{NE}

II) Velocity Estimates

Program Name	Speed	Direction	Standard Deviations and covariances		
			σ_1	σ_2	σ_{12}
GEODOP	Yes	Yes	No	No	No
SMOBS	Yes	Yes	σ_{ve}	σ_{vn}	No
DSPLIN	Yes	Yes	σ_{ve}	σ_{vn}	σ_{ven}

where ve - Velocity East
and vn - Velocity North

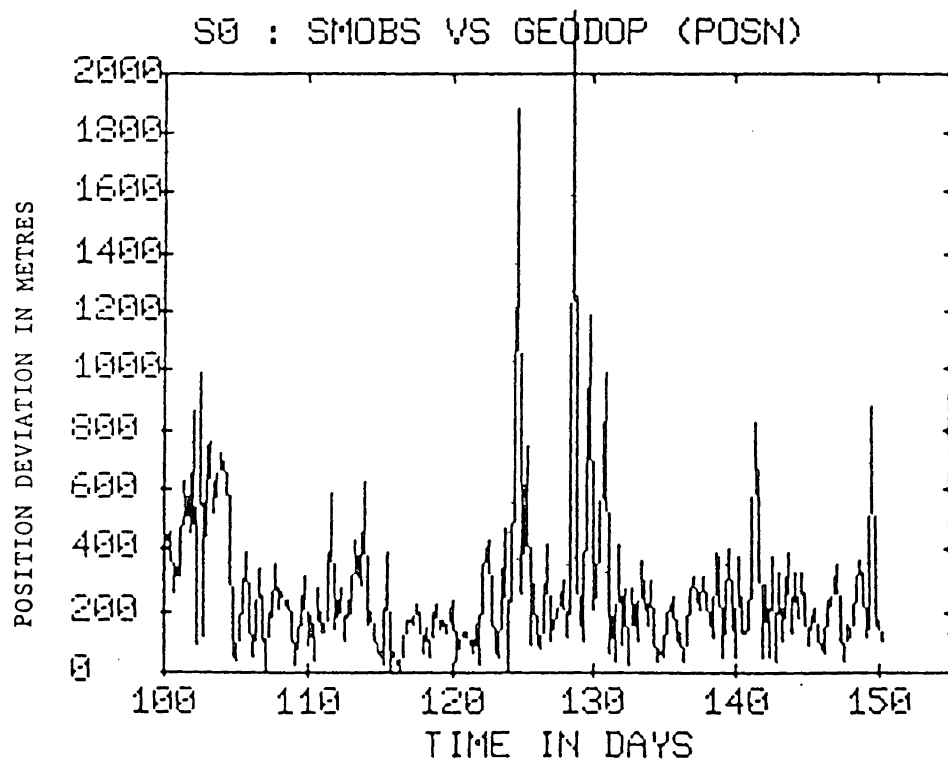
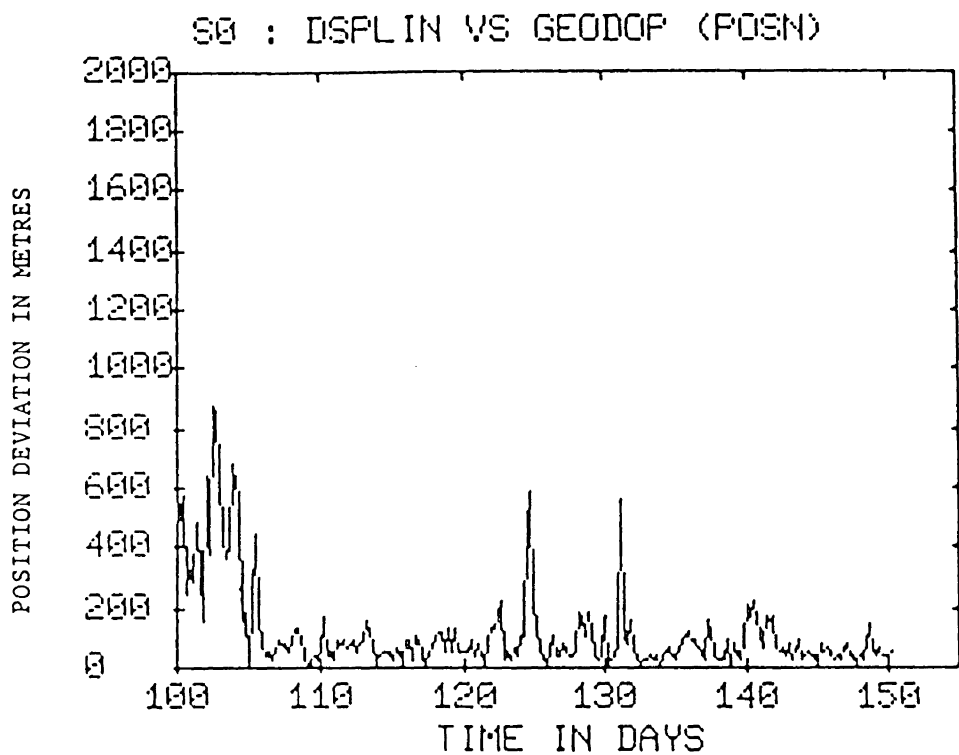


FIGURE 10-21 Time Series of Position Differences

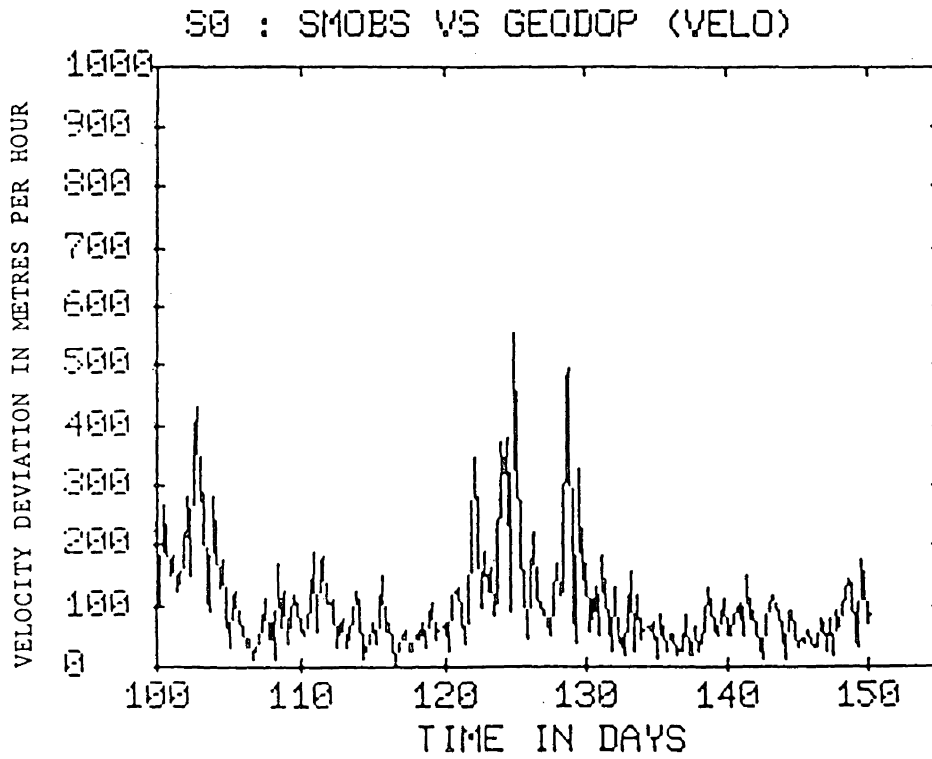
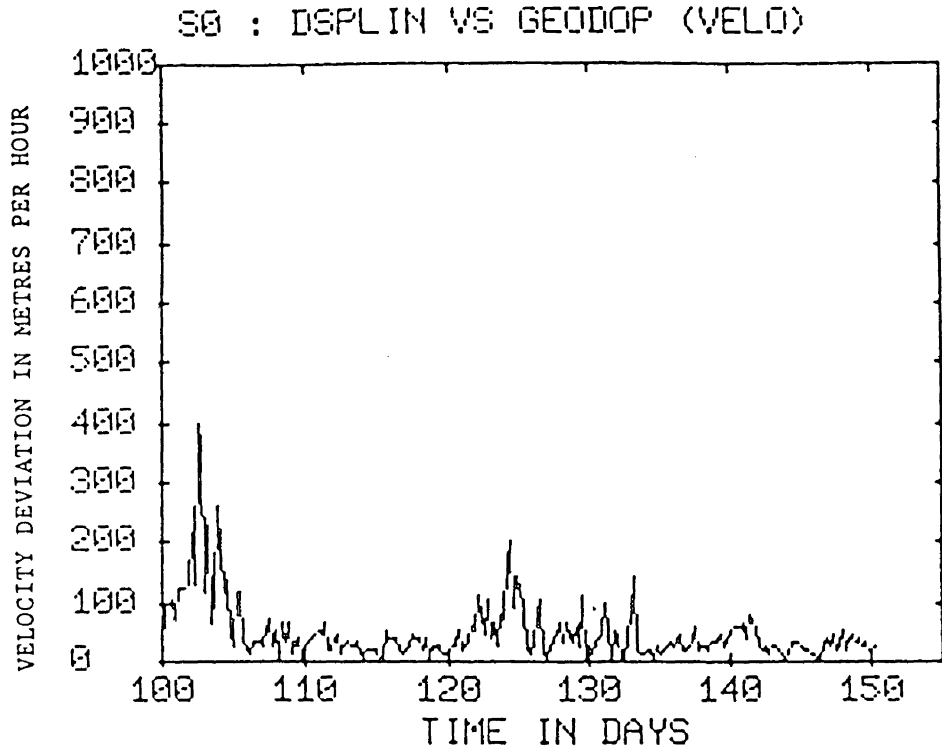


FIGURE 10-22 Time Series of Velocity Differences

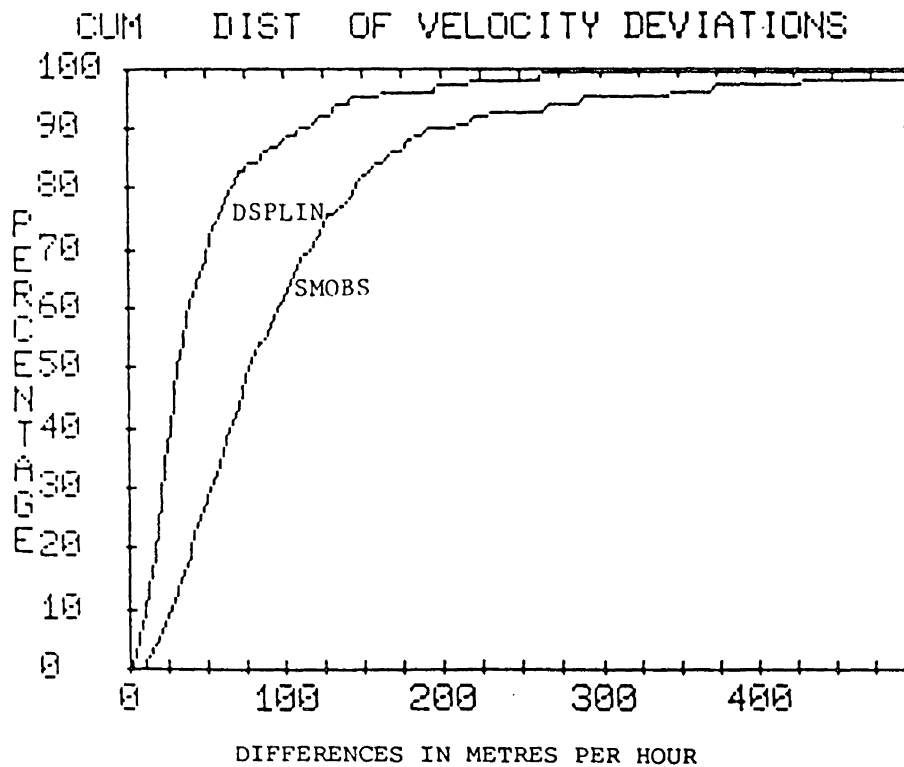
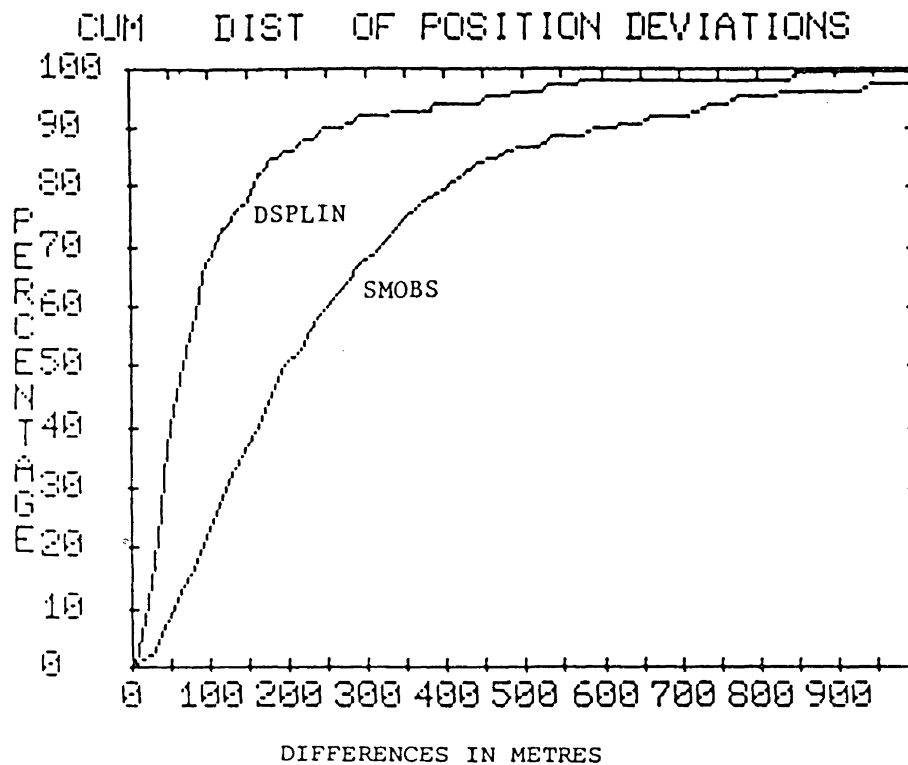


FIGURE 10-23 Cumulative Distribution of Position and Velocity Deviations

2. Computation of standardised position deviations.

This is only possible in the comparison between DSPLIN and GEODOP, and even so, the assumption that the coordinates produced by GEODOP are uncorrelated (Table 10-3) had to be made (Figure 10-24).

520 positions and velocities from S0, S1 and S2, common to the smoothed LOREX data series produced by GEODOP, SMOBS and DSPLIN, were chosen for the comparisons. The resulting root mean square of the position and velocity differences are 194 metres and 70 metres per hour, respectively from the DSPLIN versus GEODOP comparison, and 437 metres and 144 metres per hour, respectively from the SMOBS versus GEODOP comparison. Hence DSPLIN position and velocity estimates are 56 and 47 percent better than SMOBS. The time series plots of position and velocity deviations (Figure 10-21 and 10-22) show the improvement for station S0 graphically. This improvement in position and velocity estimation is again demonstrated by the cumulative distribution plots of the position and velocity deviations (Figure 10-23). The coincidence in the peaks of position and velocity deviations in Figure 10-21 and 10-22 can be explained by the fact that both DSPLIN and SMOBS use the same computed position data series and hence were influenced by the same "bad" data points. The effect of an erroneous data point however, is more pronounced with SMOBS. As demonstrated in Figure 10-21 and 10-22, smoothed position errors propagate into smoothed

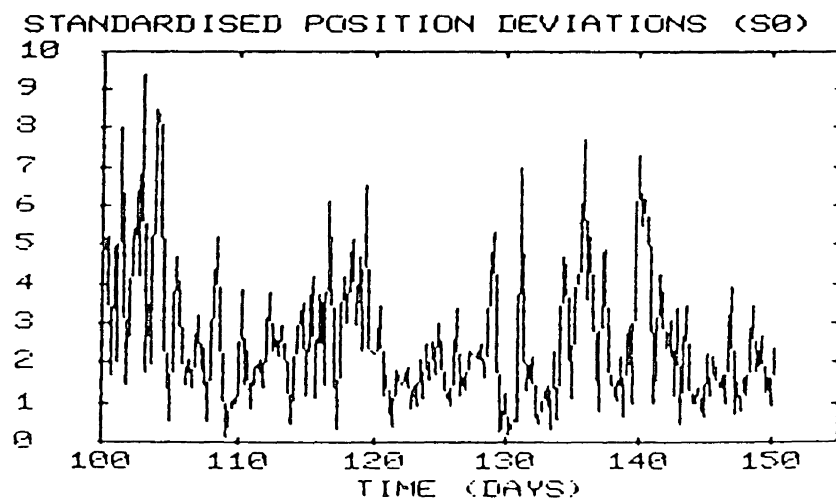
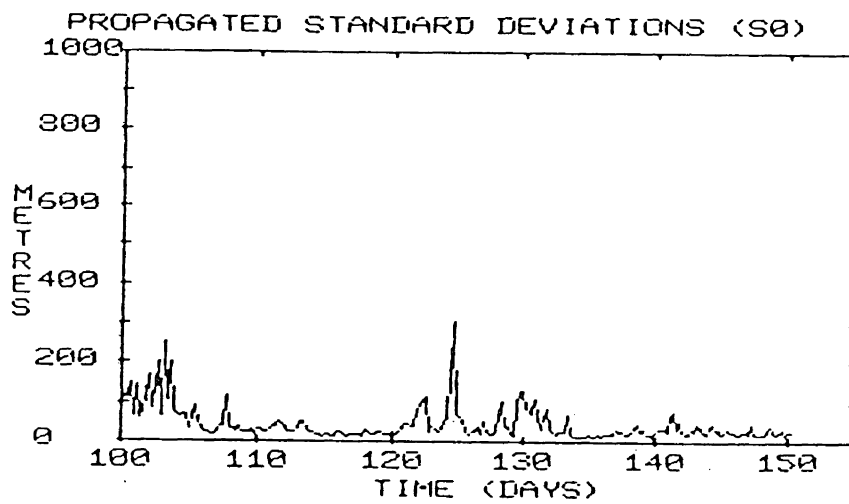
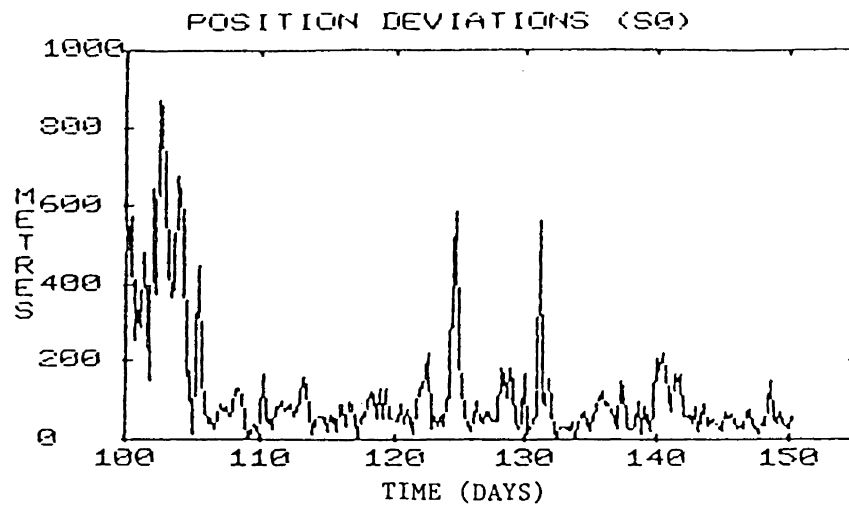


FIGURE 10-24 Time Series of Position Deviations, Propagated Standard Deviations and Standardised Position Deviations.

velocity errors. A larger discrepancy between positions produced by SMOBS or DSPLIN against GEODOP is observed to occur between day 100 and day 105. The reason for this discrepancy is not apparent. One plausible cause could be oscillator instabilities in the satellite receivers as they were all cold started upon arrival on LOREX.

As to the assessment of the consistency of the precision estimates, the ratio of the deviation to its propagated standard deviation is ideally equal to one. The plots of the time series of position deviations (equation 10-1), propagated standard deviations (equation 10-3) and standardised position deviations (equation 10-4) for station SO are given in Figure 10-24. Examination of Figure 10-24 reveals that the precision estimates (accepting GEODOP as being true) are not consistent in time with the accuracy. Generally, the position deviations are correlated with the propagated standard deviations. There are several places where they are different. The larger discrepancies between day 100 to day 105 are not adequately accounted for by the standard deviations. Consistency in the precision estimates occurs only between day 120 to day 130. The motion of the station during this period is characterized by high velocities and larger velocity changes (Figure 10-17). The highest absolute velocities reached by the three stations are recorded in this time period. Maximum velocity east (Figure 10-18) and velocity north (Figure 10-19) of the three stations also occur during this time period.

The inconsistencies are caused by the covariance matrix associated with each position being optimistic. This optimism may exist in either GEODOP or DSPLIN values. The contribution of the neglected correlation between GEODOP smoothed coordinates to the periods of inconsistency cannot be evaluated.

The overall conclusion that can be drawn is that DSPLIN (with GEODOP as reference standard) produces more accurate position and velocity estimates which are consistent with time than SMOBS and that the precision estimates are inconsistent in time with the derived measures of accuracy.

Chapter 11

CONCLUSIONS AND RECOMMENDATIONS

In this chapter, the contributions of this thesis are summarized. Conclusions and recommendations are made on smoothing with the developed spline algorithm, application of the spline algorithm to the LOREX navigation data sets and the treatment of high latitude position fixes using NNSS.

11.1 TWO-DIMENSIONAL LEAST-SQUARES CUBIC SPLINE ALGORITHM

An algorithm to smooth two-dimensional data series has been successfully developed (Chapters 5 and 6) and proven feasible with the LOREX positioning data (Chapters 9 and 10). From the numerous studies done for this thesis, the following are the conclusions and recommendations.

11.1.1 Number and Placements of Knots

The spline algorithm requires a sufficient density of knots to aptly portray the underlying nature of the data series in question. As discussed in Section 9.2, an indication of the adequacy of the number of knots can be arrived at through the evaluation of the root mean square of

the residuals and the a posteriori variance factor of the subsequently fitted spline curve (equation 7.8).

This, however, remains only a global indication of knot sufficiency. Knot selection at local intervals can be obtained through the analysis of the time series of standardised residuals of the observed data points (Section 9.3). Where the knot intervals can be linked to some physical evidence pertaining to the data series, the knot selection process is very simple. This is the minimum data period in which the process can be aptly portrayed as being cubic.

The simplistic nature of selecting the desired degree of smoothness within the data series (i.e. through defining the knot intervals) is a unique feature of this technique.

11.1.2 Joining Splines

The aspect of joining splines within a data series has been successfully explored (Section 9.5) and a minimum of two common knot intervals is recommended.

11.1.3 Predicted Data Points

The developed program (Appendix VII) computes, on request, the smoothed data points and first derivatives at any time within the data series. Estimated covariance matrices are derived for these quantities using the covariance law (Section 3.1). For a complete model, i.e.

with a sufficient density of knots, the estimated covariance matrix reflects the accuracy of the predicted data points (Section 9.3). Covariance matrices can be derived for all subsequently computed quantities using the covariance law outlined in Chapter 8.

11.1.4 The DSPLIN Program

A computer program (DSPLIN), based on the spline algorithm developed in this thesis, has been created (Appendix VII). All computations involving the spline algorithm are done with the DSPLIN Program. Various optimising procedures aid in the handling of large matrices and inverses. These, along with a short description of the 64 subroutines in DSPLIN, are given in Appendix VII: Table VII-1. Currently, DSPLIN can handle up to 32 knots and a maximum of 500 data points in a data span. The program requires about 512 kilobytes of memory to run. The programming language used is Fortran IV. All software development was done using the Fortran H Extended Compiler on the IBM 3032 computer at the University of New Brunswick.

11.1.5 Comparison with SMOBS and GEODOP

The DSPLIN program smoothed values are compared with SMOBS's (Section 2.2) using GEODOP as the reference standard (Section 10.6). In the comparisons of position and velocity differences (equations 10-1 and 10-2) of DSPLIN versus

GEODOP and SMOBS versus GEODOP, the root mean square of the differences computed from DSPLIN versus GEODOP are about 50 percent smaller than those of SMOBS versus GEODOP. Figures 10-21 to 10-23 portray the improvement of DSPLIN over SMOBS as time series plots of differences and cumulative distributions of differences. The standardised position differences in the DSPLIN and GEODOP comparison shows that the precision estimates produced by DSPLIN are not consistent in time with the accuracy. There exist however, short periods where they are consistent.

11.2 LOREX NAVIGATION DATA SETS

The following conclusions and recommendations are arrived at from the analysis and processing of the LOREX navigation data sets (Chapter 10). Conclusions drawn are applicable to high latitude navigation using the NNSS system.

The final smoothed positions of the LOREX three ice stations are given in Figure 10-15. Plots of the time series of coordinates, input positions and their formal error ellipses, and the final smoothed positions of the subsets of the three data sets from stations S0, S1 and S2 can be found in Quek [1983]. In the processing of the LOREX navigation data sets, the effects of real-time predicted velocity errors (Section 10.3.2) with high elevation satellites had to be taken into account. Their treatment involved the

modification of the a priori covariance matrix of the position fixes (Section 10.3.4).

11.2.1 A Priori Covariance Matrix of Observed Data Points

For a correct interpretation of the results of the Chi-squared test (Section 7.3.1) on the a posteriori variance factor of the computed spline curve, a reliable a priori covariance matrix has to be assigned to the observations (Section 10.3). With the LOREX data sets, extensive modifications to the formal error ellipses are made to account for errors affecting position determinations using the Transit system at high latitudes. These include the modelling of predicted velocity (Section 10.3.2) and assumed height errors (Section 10.3.3), and the accuracy of the satellite broadcast ephemerides (Section 10.3.1). An algorithm for determining the elevation angle of the observed satellite from the formal error ellipses has been developed (Appendix III: equation III-3). The conservative formal error ellipses recorded, primarily result from the small sample size of the Doppler counts used in computing the fixes.

11.2.2 Unbalanced Doppler Counts

A great majority of the computed satellite passes were observed to have Doppler counts that are severely unbalanced about the point of closest approach. As the NNSS system was

used in its weakest single pass point positioning mode, the computed positions are displaced in the along track direction of the satellite. Outright rejection of such passes is not being recommended as they do contain some useful information. Unbalanced Doppler counts within a fix computation, as mentioned above, propagate as a bias in the position of the receiver in the along track direction of the satellite. By using known accuracy estimates of the Transit position determinations and modelling all other possible errors (Section 10.3) useful information from these observations can be drawn.

11.2.3 Station Motion

The computation of position determinations with the NNSS system requires the monitoring of the motion of the receiver during the satellite pass. Any errors in the assumed velocity vector reduces the accuracy of the computed position. This degradation is especially severe with high elevation satellites. In order to minimise this phenomenon, an on-site reprocessing of the position determinations using iteratively improved velocity vectors is recommended (Section 10.5.1). The improved velocity vectors can be obtained from, for example, the spline algorithm developed in this thesis (Figure 10-1).

Computed velocity vectors of this nature, however, represent the long term variations in the motion of the

receiver. Under short term velocity vector changes, the position fixes should be computed with zero velocity vectors unless the rapid changes in velocity and direction are determined by other external means. The presence of the predicted velocity vector, when in error, will only downgrade the precision of the computed positions.

11.2.4 High Elevation Satellites

From the limited experiments made to study the behaviour of high elevation satellite passes with the spline algorithm (Section 10.3.4), it is concluded that for a non-stationary observer, the position coordinate in the cross satellite track is extremely poor. The current treatment of those fixes as line fixes (defined in Section 10.3.2) has met with some success.

11.3 SUGGESTIONS FOR FUTURE WORK

The following areas are recommended for further investigation:

For the spline algorithm:

1. The evaluation of the performance of the curve fitting routine with less noisy data.
2. The effect of different base functions for the cubic spline (e.g. those given by Spath [1974]: page 58).

3. Extension of the spline algorithm, developed here, to smooth multi-dimensional data series.

The technique, as described in this thesis, can be easily extended to smooth a multi-dimensional data series. Here, more than two parametric cubic splines are simultaneously solved using the method of least-squares.

For the computer program:

4. The incorporation of a banded inverse routine which operates on a banded normal matrix and produces only a banded a posteriori covariance matrix.

The processing time in computing the inverses can be reduced by a factor of b^2/n^2 ; with n being the order of the matrix and b being the bandwidth (Appendix VII).

5. Additions to the program to allow the processing of a full data series without any manual intervention.

Currently, the subsets of a data series are individually splined and the technique of splicing splines (described in Section 9.5) used to achieve continuity. The proposed modifications here involve automating data management of the data series, which currently is done manually through interactive files.

For the LOREX navigation data series:

6. Further investigation into the effect of velocity-caused errors on position fixes with high elevation satellites.
7. Reprocessing of the position fixes, using velocities derived from the spline-smoothed trajectories, and reprocessing using the spline algorithm on these improved position fixes.
8. Real-time implementation of the spline algorithm.

The real-time application of the spline algorithm is described in Section 10.3. The DSPLIN program with minor alterations, easily done due to its modular structure, and a new driver routine, can be adapted to operate in real-time mode. It has to be used together with a satellite fix computation routine and in the pre-processing mode supply better velocity estimates for a recomputation of the position fixes.

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Appendix I
LEAST-SQUARES ADJUSTMENT VIA PARAMETER
ELIMINATION

In this appendix, the least-squares adjustment with constraints through the elimination of constraint equations is presented. The working equations are derived and the compatibility of implementing these equations in the current algorithm discussed.

The basic models, primary and secondary, were given in Chapter 7. Reference should be made to that chapter for clarification of model definitions and variable names used in this appendix.

Constraint equations relate only the functional relationship between parameters (or unknowns). The functional dependence of the parameters leads to the fact that there are as many dependent parameters as there are constraint equations. In the spline algorithm developed in Chapter 5, the constraint equations functionally relate the first derivative (or slope) at the current knot with the first derivatives and positions of fore and aft knots (equations 5.4).

Using the method of parameter elimination [Mikhail 1976: page 217], the constraint equations are used to functionally solve for as many parameters as there are constraints.

With Taylor's expansion and Lagrange multipliers using the constrained minima technique, the following sets of equations can be obtained (as in Section 7.3).

$$\begin{bmatrix} \underline{w}_1 \\ \underline{w}_2 \end{bmatrix} + \begin{bmatrix} \underline{A}_1 \\ \underline{A}_2 \end{bmatrix} \underline{\delta} + \begin{bmatrix} \underline{B} & \underline{0} \\ \underline{0} & \underline{0} \end{bmatrix} \underline{v} = \underline{0} \quad - \text{(I-1)}$$

where

$$\begin{aligned} \underline{w}_1 &:= \partial \underline{f}_1(\underline{x}^0, \underline{l}^0) \\ \underline{w}_2 &:= \partial \underline{f}_2(\underline{x}^0) \\ \underline{A}_1 &:= \left. \frac{\partial \underline{f}_1}{\partial \underline{x}} \right|_{\underline{x}^0, \underline{l}^0}, \quad \underline{A}_2 := \left. \frac{\partial \underline{f}_2}{\partial \underline{x}} \right|_{\underline{x}^0} \\ \underline{B} &:= \left. \frac{\partial \underline{f}_1}{\partial \underline{l}} \right|_{\underline{x}^0, \underline{l}^0} \end{aligned}$$

and with $\underline{P} := \sigma_{\underline{0}} \underline{\Sigma}_1^{-1}$
 ($\underline{\Sigma}_1$ is the covariance matrix of observables, \underline{l})

Now, let the subvector $\underline{\delta}_2$ contain the parameters to be eliminated

$$\text{i.e.} \quad \underline{\delta} := [\underline{\delta}_1 \quad \vdots \quad \underline{\delta}_2]$$

Similarly, by partitioning the design matrices,

$$\text{i.e.} \quad \underline{A}_1 := [\underline{C} \quad \vdots \quad \underline{D}]$$

$$\text{and} \quad \underline{A}_2 := [\underline{G} \quad \vdots \quad \underline{H}]$$

equation (I-1) is transformed to

$$\begin{bmatrix} \underline{C} & \underline{D} \end{bmatrix} \begin{bmatrix} \delta_1 \\ \delta_2 \end{bmatrix} + \underline{Bv} + \underline{w}_1 = \underline{0} \quad - \text{(I-2)}$$

$$\begin{bmatrix} \underline{G} & \underline{H} \end{bmatrix} \begin{bmatrix} \delta_1 \\ \delta_2 \end{bmatrix} + \underline{w}_2 = \underline{0} \quad - \text{(I-3)}$$

Solving equation (I-3),

$$\delta_2 = - \underline{H}^{-1}(\underline{w}_2 + \underline{G}\delta_1) \quad - \text{(I-4)}$$

Note that the \underline{H}^{-1} matrix must exist for this technique to be feasible. A discussion relating this "constraint" to the spline algorithm was presented under Section 7.2.

Eliminating δ_2 in equation (I-2),

$$\underline{C}\delta_1 - \underline{DH}^{-1}(\underline{w}_2 + \underline{G}\delta_1) + \underline{Bv} + \underline{w}_1 = \underline{0} \quad - \text{(I-5)}$$

Rearranging equation (I-5),

$$\begin{bmatrix} \underline{C} - \underline{DH}^{-1}\underline{G} \end{bmatrix} \delta_1 + \begin{bmatrix} \underline{w}_1 - \underline{DH}^{-1}\underline{w}_2 \end{bmatrix} + \underline{Bv} = \underline{0} \quad - \text{(I-6)}$$

By letting

$$\underline{\bar{A}} := \begin{bmatrix} \underline{C} - \underline{DH}^{-1}\underline{G} \end{bmatrix}$$

and $\underline{\bar{w}} := \begin{bmatrix} \underline{w}_1 - \underline{DH}^{-1}\underline{w}_2 \end{bmatrix}$

and with the assumption that the model is of a parametric nature, the direct least-squares treatment of equation (I-6) yields:

$$\hat{\underline{\delta}}_1 = - (\underline{\overline{A}}^T \underline{\overline{PA}})^{-1} \underline{\overline{A}}^T \underline{\overline{Pw}} := - \underline{\overline{N}}^{-1} \underline{\overline{A}}^T \underline{\overline{Pw}} \quad - (I-7)$$

Through back substitution,

$$\hat{\underline{\delta}}_2 = - \underline{\overline{H}}^{-1} [\underline{\overline{w}}_2 - \underline{\overline{G}} (\underline{\overline{A}}^T \underline{\overline{PA}})^{-1} \underline{\overline{A}}^T \underline{\overline{Pw}}] \quad - (I-8)$$

Using the covariance law (see Section 8.1), the covariance of the subvectors of the least-squares estimates are as follows:

$$\begin{aligned} \hat{\underline{\Sigma}}_{\underline{\delta}_1} &:= \underline{\overline{JC}} - \underline{\overline{J}} \underline{\overline{J}}^T, \quad \underline{\overline{J}} := \frac{\partial \hat{\underline{\delta}}_1}{\partial \underline{\overline{w}}} \\ &= (\underline{\overline{N}}^{-1} \underline{\overline{A}}^T \underline{\overline{P}}) \underline{\overline{\Sigma}}_{\underline{\delta}} (\underline{\overline{PAN}}^{-1}) \end{aligned} \quad - (I-9)$$

Simplifying,

$$\hat{\underline{\Sigma}}_{\underline{\delta}_1} = \underline{\overline{N}}^{-1} \quad - (I-10)$$

In a similar manner,

$$\hat{\underline{\Sigma}}_{\underline{\delta}_2} = (\underline{\overline{H}}^{-1} \underline{\overline{G}}) \underline{\overline{N}}^{-1} (\underline{\overline{H}}^{-1} \underline{\overline{G}})^T$$

and $\hat{\underline{\Sigma}}_{\underline{\delta}_1 \underline{\delta}_2} = - \underline{\overline{N}}^{-1} (\underline{\overline{H}}^{-1} \underline{\overline{G}})^T$

Finally, in summary,

$$\hat{\underline{\delta}} = [\hat{\underline{\delta}}_1 \quad \hat{\underline{\delta}}_2]$$

and

$$\hat{\underline{\Sigma}}_{\underline{\delta}} = \begin{bmatrix} \underline{\bar{N}}^{-1} & -\underline{\bar{N}}^{-1}(\underline{H}^{-1}\underline{G})^T \\ -(\underline{H}^{-1}\underline{GN}^{-1}) & \underline{H}^{-1}\underline{GN}^{-1}(\underline{H}^{-1}\underline{G}^T)^T \end{bmatrix} \quad - (I-11)$$

Hence for the spline algorithm, the parameter solution through the elimination of constraints is possible only if \underline{H}^{-1} matrix exists (equation I-4).

Three routines (LS2, TRNSFM and PERM) have been formulated and listed in Appendix VII. Subroutine TRNSFM reformats the primary and secondary design matrices into their various submatrices. Subroutine LS2 performs the least-squares adjustment using the method described above. Finally subroutine PERM unscrambles the least-squares estimates and covariances to conform to the rest of the DSPLIN program. This has to be done because the DSPLIN program expects the solution vector and the covariance matrix to be of the form produced by the functionally constrained least-squares method.

Appendix II
COMPUTATIONAL ACCURACY

In this appendix, the aspect of computational accuracy is discussed. Primarily there are two possible conditions which can lead to a degradation in the computational precision of the solution vector in the linear system of equations, $\underline{N} \underline{x} = \underline{b}$, that is, the use of floating-point arithmetic and the presence of an unstable algorithm.

The accuracy of floating-point arithmetic [Forsythe et al. 1977: page 13] can be characterized at run time by the so-called "machine epsilon"; the smallest floating point number ϵ such that

$$1 \oplus \epsilon > 1$$

- (II-1)

Round-off error, through a phenomenon called "catastrophic cancellation" [Forsythe et al. 1977: page 15] in badly conceived computation sequences can result in a near total loss of significant digits. Although it is possible to carry more digits to avoid this phenomenon, it is always more costly in terms of execution time and storage space. A better approach is to keep a good track of the arithmetic process and the expected sizes of the numbers involved in the computations.

An estimate of the internal computational accuracy can be arrived at through the manipulation of the results such that a null vector is formulated. In the direct least-squares treatment of the system of equations, $\underline{N} \underline{x} = \underline{b}$, where $\underline{N} = (\underline{A}^T \underline{P} \underline{A})$ and $\underline{b} = -(\underline{A}^T \underline{P} \underline{w})$, the null vector, \underline{e} can be expressed as $\underline{e} = \underline{A}^T \underline{P} (\underline{A} \hat{\underline{x}} + \underline{w})$. For the functionally constrained least-squares model, the vector \underline{e} takes the form:

$$\underline{e} = \underline{\Sigma}_x^T \underline{A} \quad - \text{(II-2)}$$

with $\underline{\Sigma}_x$ and \underline{A} matrices as defined in Section 8.2. Theoretically, the vector \underline{e} is a null vector. However, with the use of finite precision arithmetic, the maximum $|\underline{e}|$, ($\underline{e} \in \underline{e}$) so obtained, gives a good estimate of the computational accuracy of the algorithm.

For certain problems, good answers cannot be obtained no matter how well the algorithm is conceived. This aspect of numerical analysis is independent of the floating-point number system or the algorithm used.

When small errors in the right hand side of a system of linear equations causes a large effect on the solution vector, the problem is termed "ill-conditioned", i.e. it is very sensitive to the values on the right-hand side. Ill-conditioning occurs when the transformation (or coefficient) matrix \underline{N} is nearly singular. An example of such an effect is illustrated in Westlake [1968]: page 89. If \underline{N} is a

singular matrix, then for some \underline{b} 's a solution of \underline{x} does not exist. If \underline{N} is nearly singular, then small changes in \underline{b} would result in disproportionately large changes in \underline{x} .

To have a more precise and comprehensible measure of nearness to singularity, there exist the "condition numbers". Determinants of unnormalised transformation matrices are ineffective as a yardstick for conditioning as the equations can be premultiplied by any constant to obtain any value of $\det(\underline{N})$.

Considering the system of equations $\underline{N} \underline{x} = \underline{b}$, introducing an error of $\Delta \underline{b}$ in \underline{b} results in a change of $\Delta \underline{x}$ in \underline{x} . The condition number of \underline{N} is then defined as the ratio between the relative change in the right-hand side and the relative error caused by this change [Forsythe et al. 1977: page 43], i.e.

$$\text{cond}(\underline{N}) \geq \frac{\|\Delta \underline{x}\| / \|\underline{x}\|}{\|\Delta \underline{b}\| / \|\underline{b}\|}$$

where $\|\cdot\|$ denotes the norm of a vector. - (II-3)

The condition number, as mentioned earlier, is a measure of the nearness to singularity and can be thought of as the reciprocal of the relative distance of the matrix to a set of singular matrices [Forsythe et al. 1977: page 43]. If $\text{cond}(\underline{N})$ is large, then \underline{N} is close to being singular.

The actual computation of $\text{cond}(\underline{N})$ involves knowing the inverse of \underline{N} . If \underline{n}_j and \underline{n}'_j are the column vectors of \underline{N} and \underline{N}^{-1} respectively, then in terms of the Euclidean vector norm ($\|\underline{x}\|^2 := \sum_{j=1}^m x_j^2$).

$$\text{cond}(N) = \max_j \left\| \frac{n_j}{-j} \right\| \cdot \max_j \left\| \frac{n'_j}{-j} \right\|$$

- (II-4)

Other norms, like the sum of absolute values can be used as an alternative to the expensive-to-evaluate Euclidean norm.

This definition represents but only one of the family of possible condition numbers; Turing's m-condition number, Von Neuman and Goldstine's P-condition number, are but a few [Westlake 1968: page 90].

In the realm of computational accuracy estimates in performing the inverse, the power of the condition number is an approximate estimate as to the number of significant digits lost during the inversion process.

A third method which assesses the cumulative loss in significant figures due to round-off and conditioning of the transformation matrix, is the multiplication of the inverse with the uninverted matrix, i.e. $\underline{N}^{-1}\underline{N} = [\underline{I}]$. The technique requires a massive amount of array space when large inverses are contemplated. Hence it is seldom used.

In relation to the program DSPLIN, both the condition numbers (computed via equation II-4) and the internal computational accuracy estimates (computed via equation II-2) are evaluated to assess the conditioning of the inverses and the computational accuracy of the least-squares estimates (in equations 7.9).

Appendix III

ALGORITHM FOR COMPUTING MAXIMUM SATELLITE ELEVATION

The maximum elevation of the Transit satellite can be evaluated solely from geometrical considerations given the position of observer and the velocity vector of the satellite at point of closest approach (obtained from the formal error ellipse associated with each position determination - see Section 10.2.2).

Consider Figure III-1, we have

$$(y + R_e)/R_s = \cos \gamma \quad - \text{(III-1)}$$

Rearranging

$$y = R_s \cos \gamma - R_e$$

and

$$x = R_s \sin \gamma \quad - \text{(III-2)}$$

with R_s = radius of the satellite at the center of the earth

and R_e = radius of the observer at the center of the earth

Now, the elevation angle of the satellite (E) can be expressed as

$$E = \tan^{-1} [y/x]$$

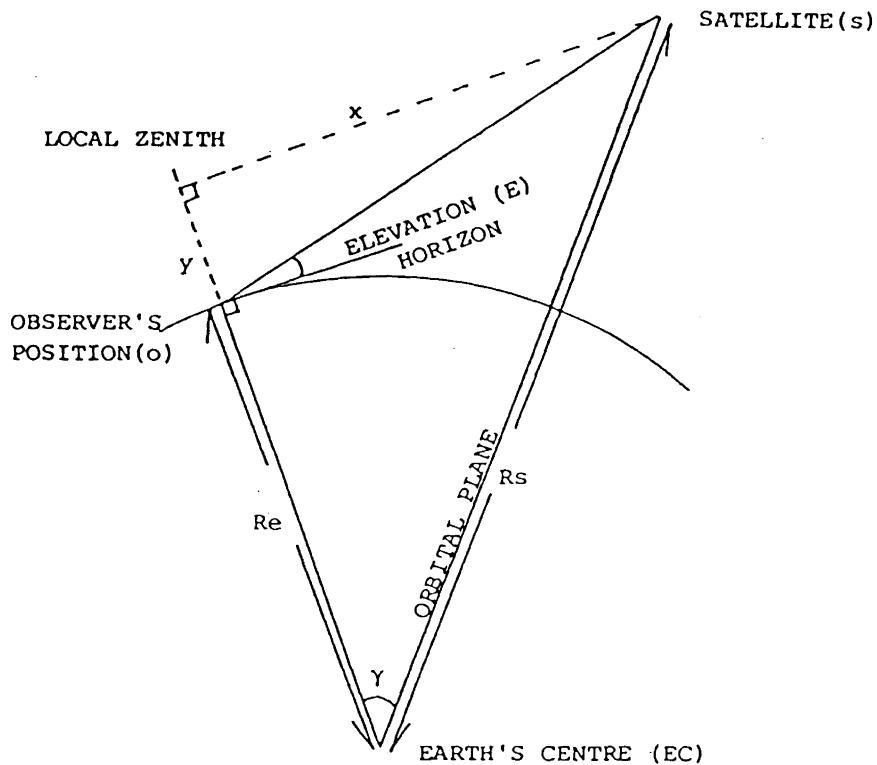


FIGURE III-1 Plane defined by the Earth's centre, the observer's position and the point of closest approach of the satellite.

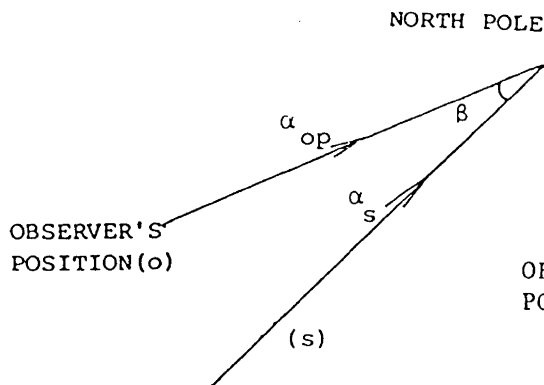


Figure III-3 North Pole view in the Polar Stereographic Coordinate System.

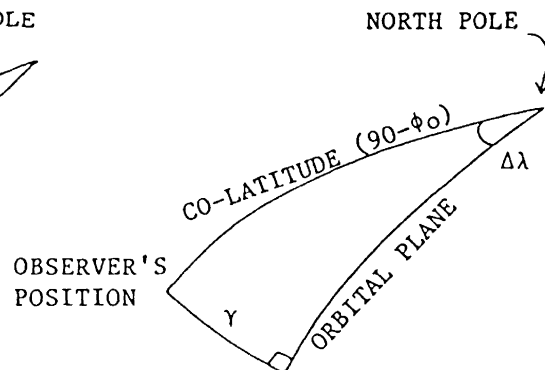


FIGURE III-2 Spherical triangle defined by the observer's position, point of closest approach of the satellite and the North Pole.

Substituting for x and y ,

$$E = \tan^{-1} \frac{\cos \gamma - R_e/R_s}{\sin \gamma} \quad - \text{(III-3)}$$

Assuming that all satellites pass directly over the North Pole, the angle γ can be expressed as being (see Figure III-2):

$$\sin \gamma = \cos \phi_o \sin \Delta\lambda \quad - \text{(III-4)}$$

where ϕ_o := observer's latitude,
and $\Delta\lambda$:= difference in longitude between observer and
satellite orbital plane.

However, the difference in longitude (i.e. $\Delta\lambda$) between the observer and the ground track of the satellite is the difference between the direction vector from the observer to the pole (α_{op}) and the velocity vector of the satellite at point of closest approach (α_s) (Figure III-3).

Hence given the position of the observer and the velocity vector of the satellite at the point of closest approach, the maximum elevation of the satellite can be computed (i.e. via equation III-3).

Appendix IV
FORMULATION OF SIMULATED DATA SET

In this appendix, the explicit equations used to generate the simulated data points are given along with the data points chosen as being the simulated data set. There are no specific reasons behind choosing this form to portray the simulated data set. The data set need only be smooth, not necessarily periodic, and with some superimposed "noise".

The following are the formulas used:

$$(x,y) := \left(\begin{array}{l} a \sin(w_x t + \phi_x) + R_x , \\ b \sin(w_y t + \phi_y) + 3t + 250 + R_y \end{array} \right)$$

with $a := 1400 \text{ m}$ - (IV-1)

$b := 250 \text{ m}$

$w_x := 2 * \pi / 440$

$w_y := 2 * \pi / 70$

$\phi_x := 2^\circ$

$\phi_y := 40^\circ$

$R_x := 5 \sin (2 * \pi t / 1.5)$

$R_y := -5 \sin (2 * \pi t / 1.5 - \pi)$

and $t := 0, 2, 4, \dots, 100$.

Basically, the x component has only a periodic term and a phase offset, whereas the y component incorporates, in addition, a linear trend. Both coordinates have a high frequency term (i.e. R_x and R_y) which acts as noise on the simulated data set.

TABLE IV-1

SIMULATED DATA SET

Time	Easting (x)	Northing (y)	Time	Easting (x)	Northing (y)
0	48.859	410.697	36	730.550	180.783
4	124.325	475.412	42	830.070	133.425
10	243.151	525.592	52	977.734	203.142
14	330.073	528.126	60	1089.400	380.462
20	445.395	465.281	66	1160.651	531.156
24	516.200	393.303	70	1199.122	616.366
26	577.481	359.702	72	1223.388	658.309
28	585.321	312.231	88	1341.437	693.779
30	625.670	278.311	92	1369.932	643.273
32	665.509	246.374	94	1369.522	598.973
			98	1391.317	530.892

Note : All points are assigned a variance of 25 square metres in x and y, and a covariance of 0.0001 square metres. The selection of the points constituting the simulated data set is described in Section 9.1.

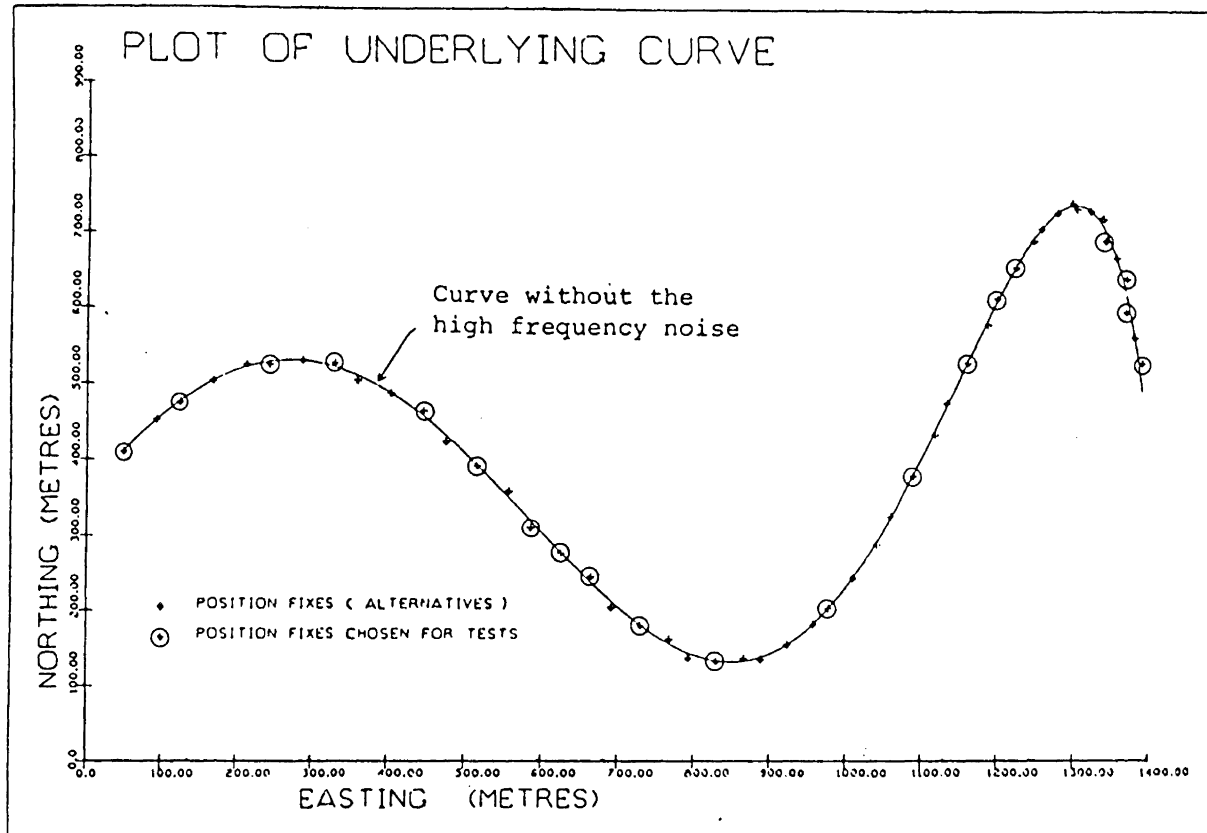


FIGURE IV-1 Location of the simulated data points chosen to test the spline algorithm

Appendix V

DESCRIPTION OF LOREX-79 TEST DATA SETS

In this appendix, a brief description and nature of the selected three disjointed stretches of the LOREX Main Camp positioning data used in evaluating the performance of the spline algorithm are given.

To aptly sample the LOREX Doppler data, three separate segments of the satellite fix data series were chosen. This is done to allow the evaluation of the algorithm (see Chapter 9) under a variety of different conditions at the time of the observation of the Transit satellites.

V.1 LOREX TEST DATA SET ONE

Period : From day 113 hr 19 min 38

to day 116 hr 19 min 44

Number of points : 100

Receiver's motion : Fairly constant; velocity northwards was about 100 metres per hour and velocity eastwards was about 120 metres per hour.

Data Plots : Figures V-1 (or V-1a), V-2 and V-3

V.2 LOREX TEST DATA SET TWO

Period : From day 120 hr 2 min 18
to day 123 hr 3 min 2

Number of points : 100

Receiver's motion : Accelerating; velocity north changes from +50 to -50 metres per hour and velocity east changes from -110 to -620 and finally to -300 metres per hour.

Data Plots : Figures V-4, V-5 and V-6

V.3 LOREX TEST DATA SET THREE

Period : From day 130 hr 2 min 30
to day 139 hr 8 min 30

Number of points : 100

Receiver's motion : Decelerating; ice platform slows down from 90 metres per hour, stops and moves off in a new direction at 140 metres per hour.

Data Plots : Figures V-7, V-8 and V-9

Note : All plotted ellipses are drawn using the formal covariance matrix of the satellite fixes at the 99 percent confidence level.

FIGURE V-1 OBSERVED POSITION FIXES OF TEST DATA SET ONE. ALL
ERROR ELLIPSES ARE AT THE 99 % CONFIDENCE LEVEL

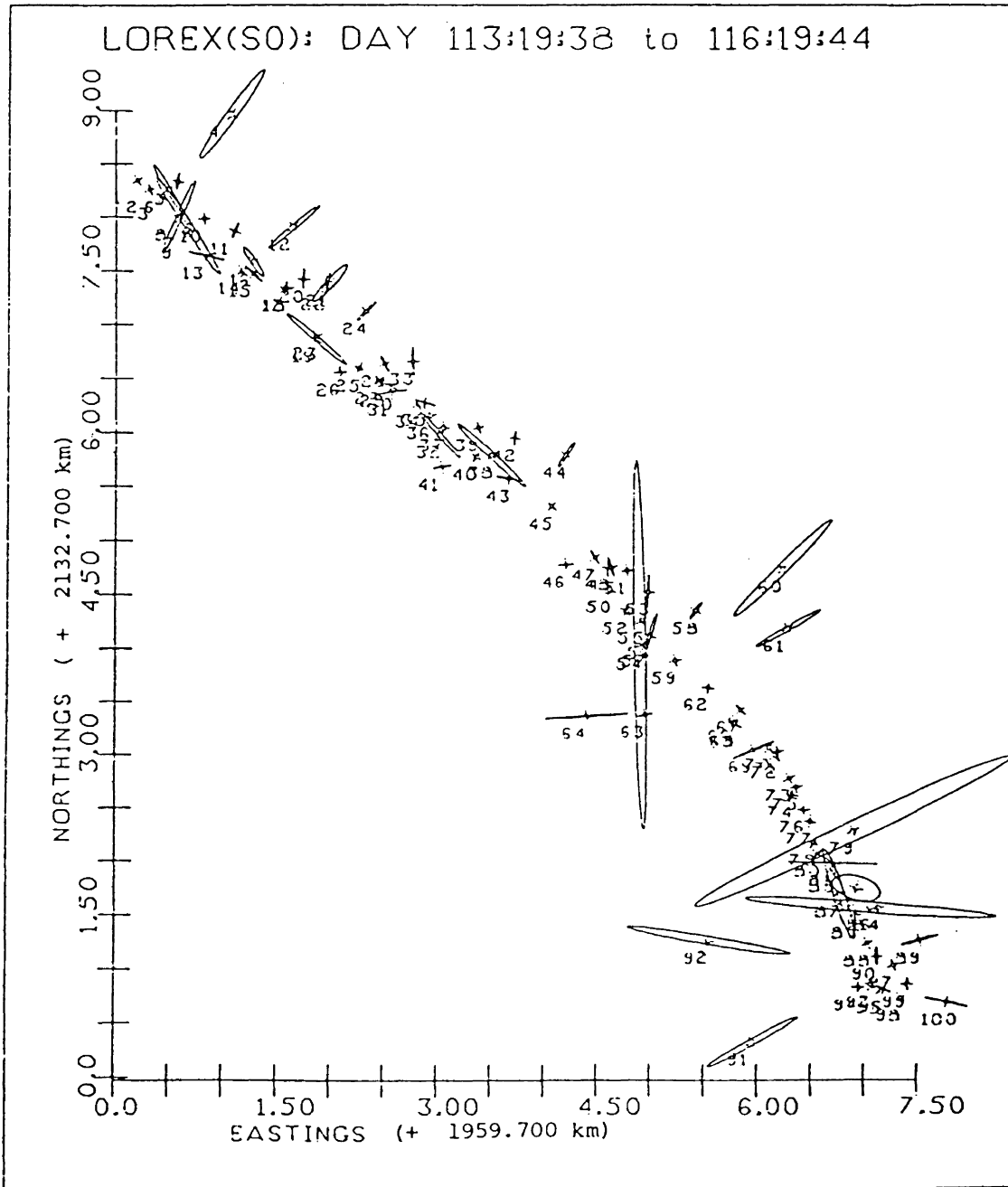


FIGURE V-1a OBSERVED POSITION FIXES OF TEST DATA SET ONE. ALL ERROR ELLIPSES WITH STD DEV. OF LESS THAN 20 m HAVE BEEN SCALED UP EQUALLY IN EASTINGS AND NORTHINGS

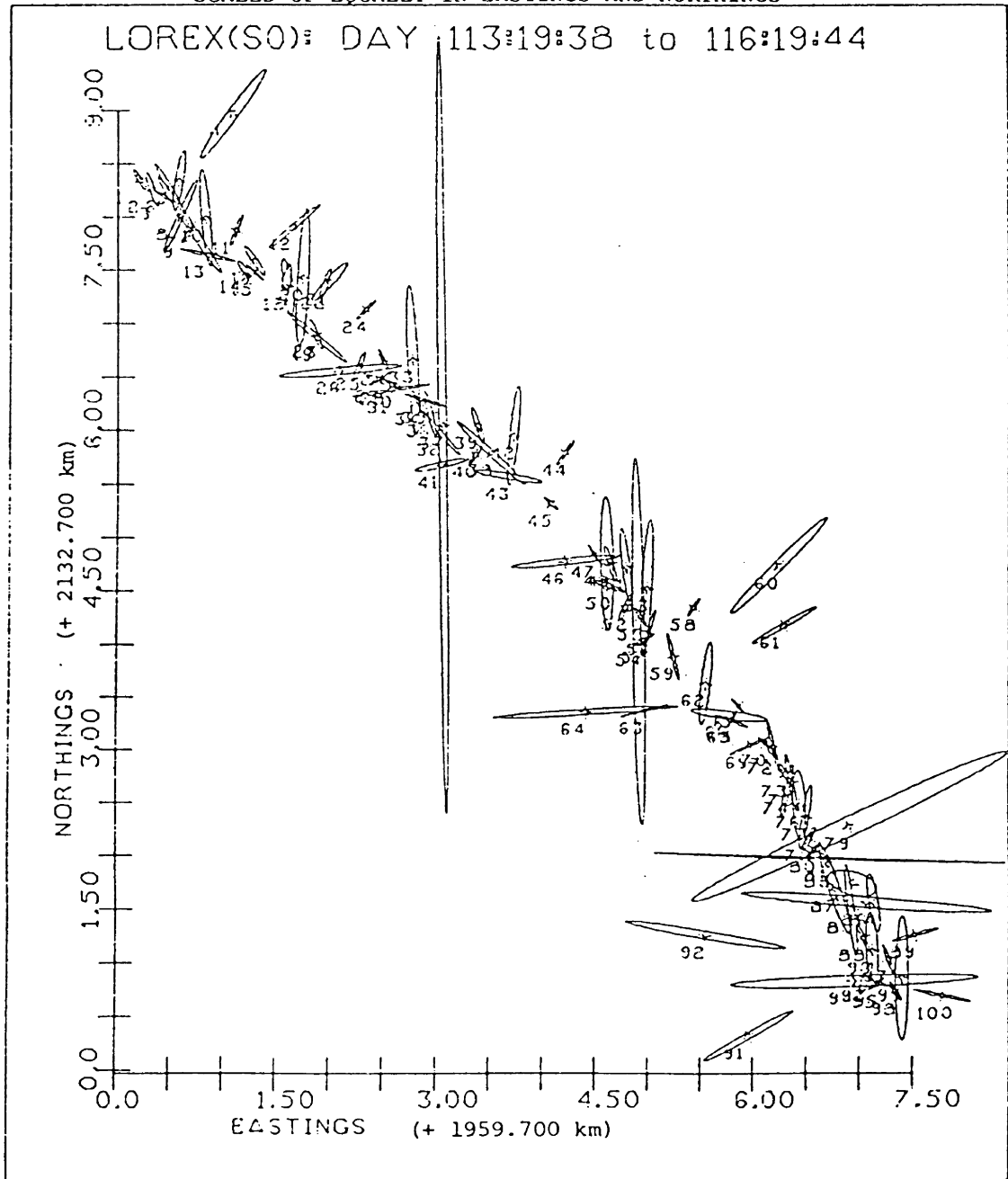


FIGURE V-2 OBSERVED POSITIONS OF TEST DATA SET ONE PORTRAYED IN THE TIME DOMAIN

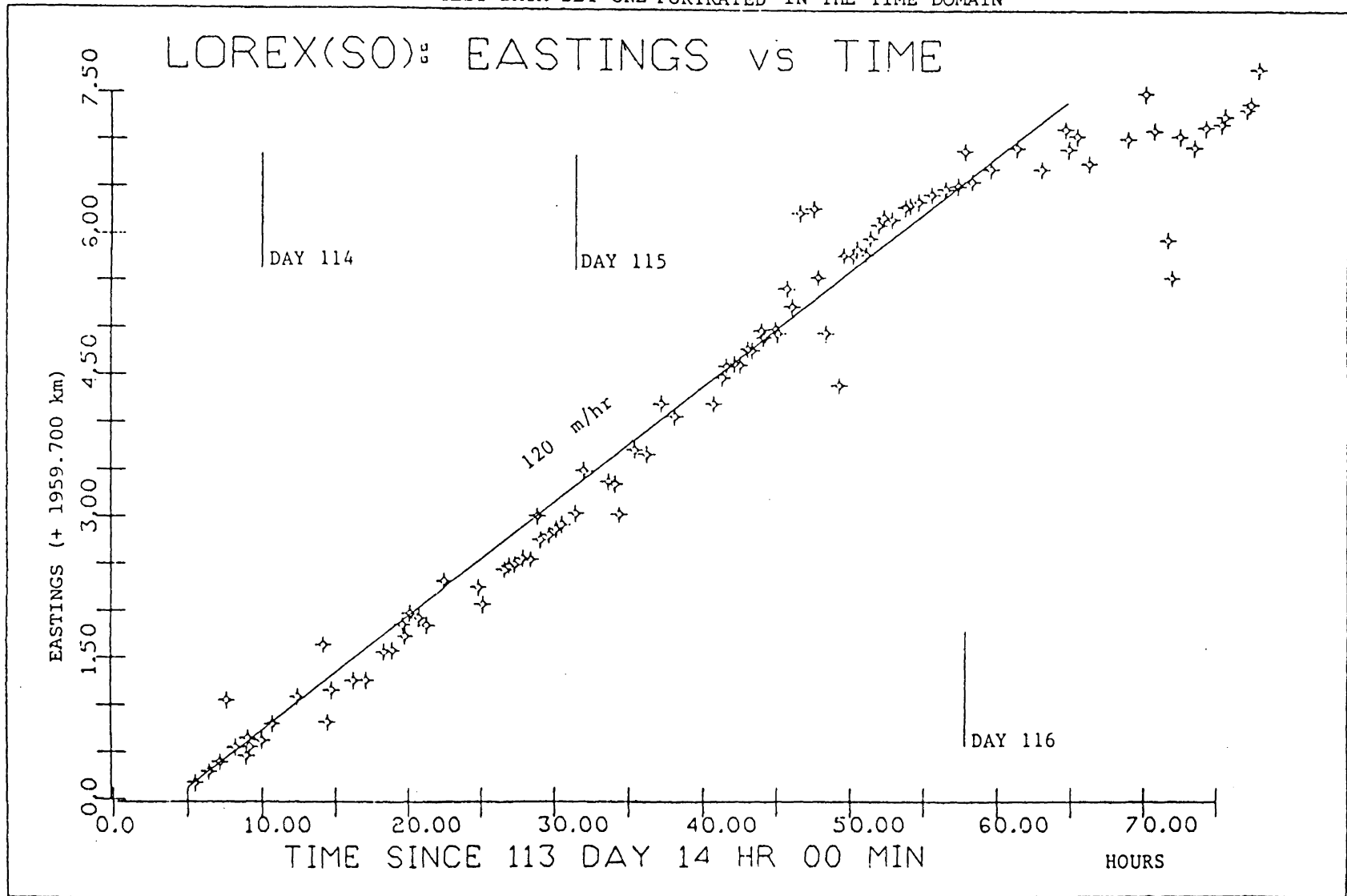


FIGURE V-3 OBSERVED POSITIONS OF TEST DATA SET ONE PORTRAYED IN THE TIME DOMAIN

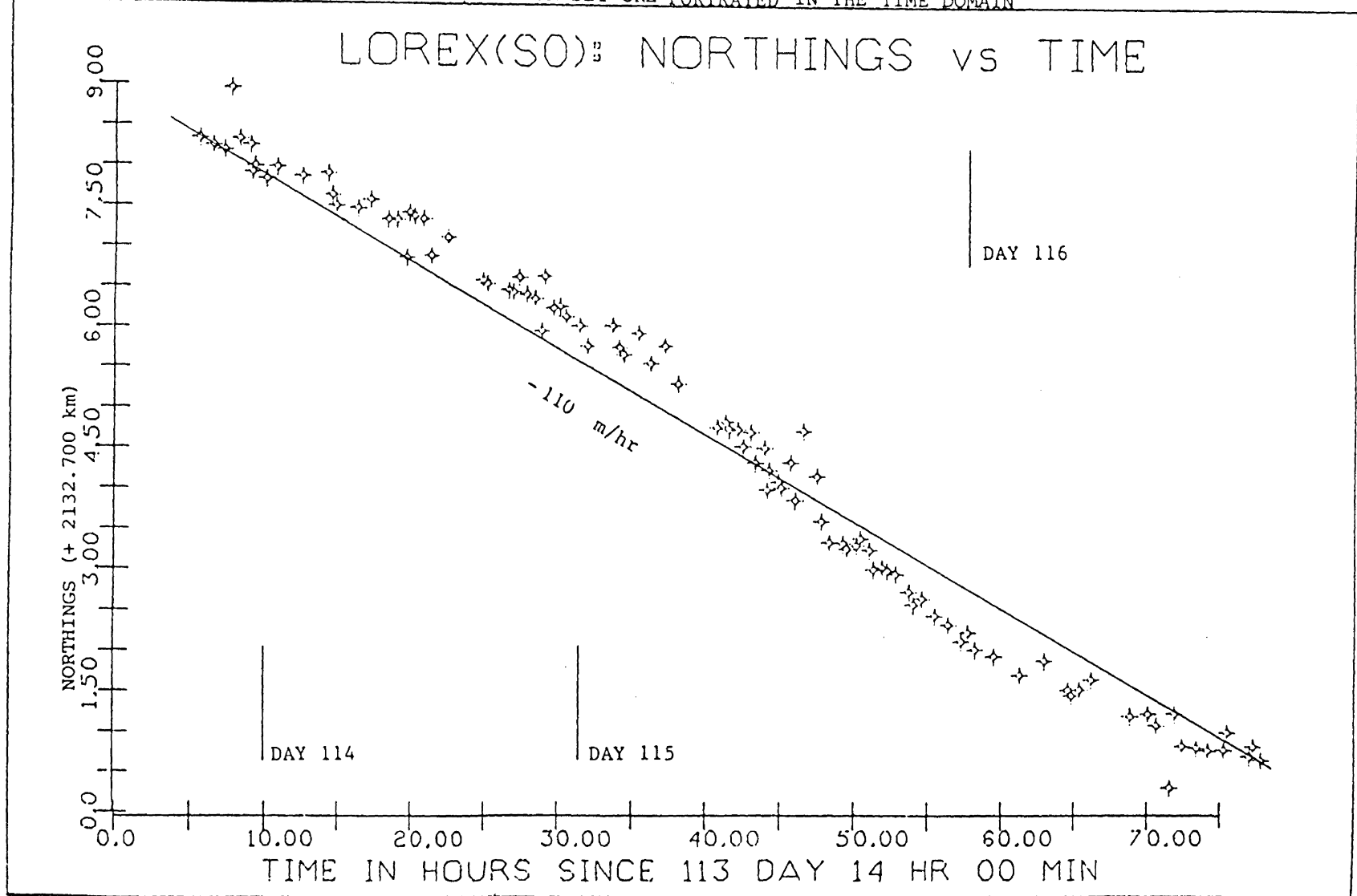


FIGURE V-4 OBSERVED POSITION FIXES OF TEST DATA SET TWO

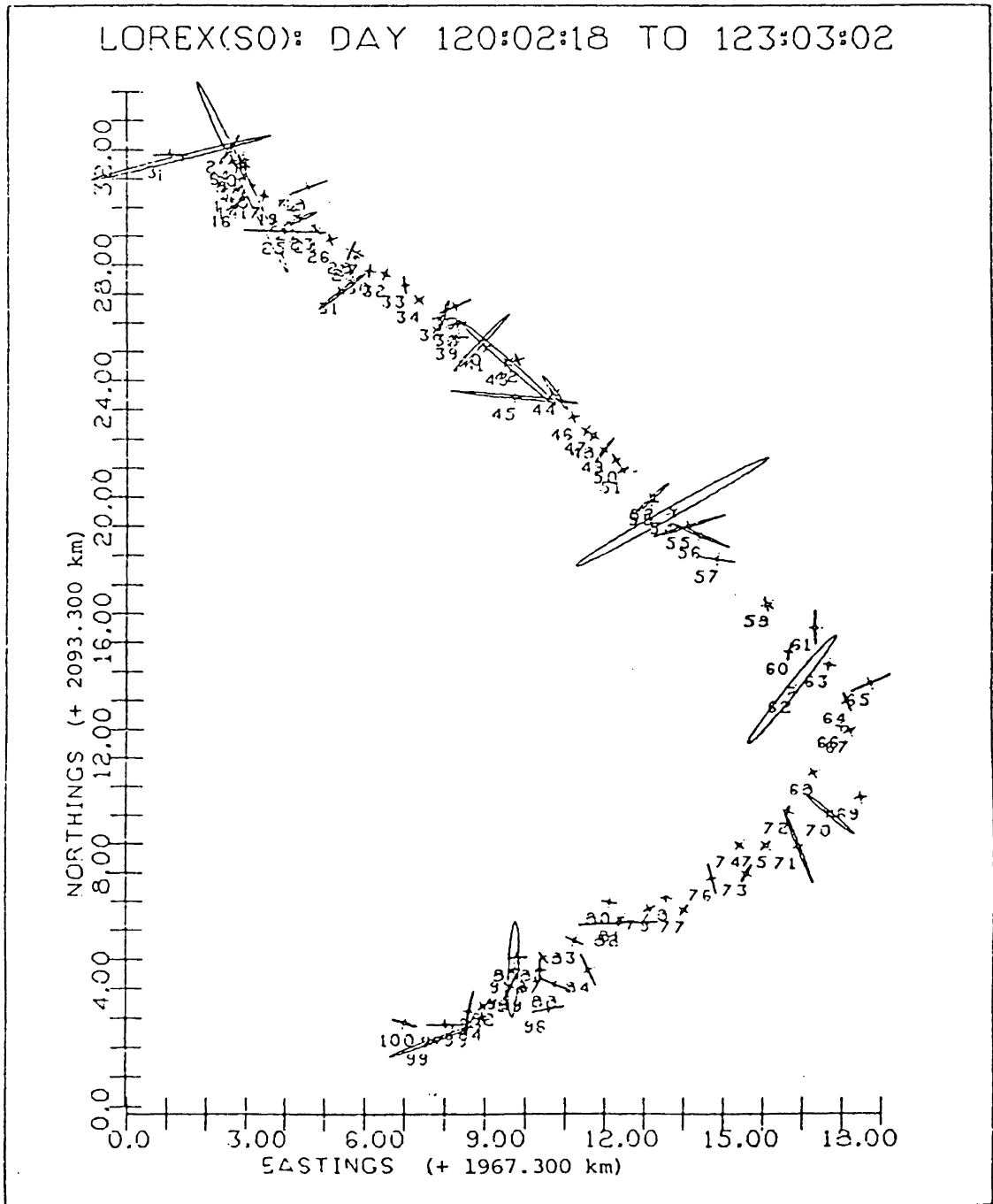


FIGURE V-5 OBSERVED POSITIONS OF TEST DATA SET TWO PORTRAYED IN THE TIME DOMAIN

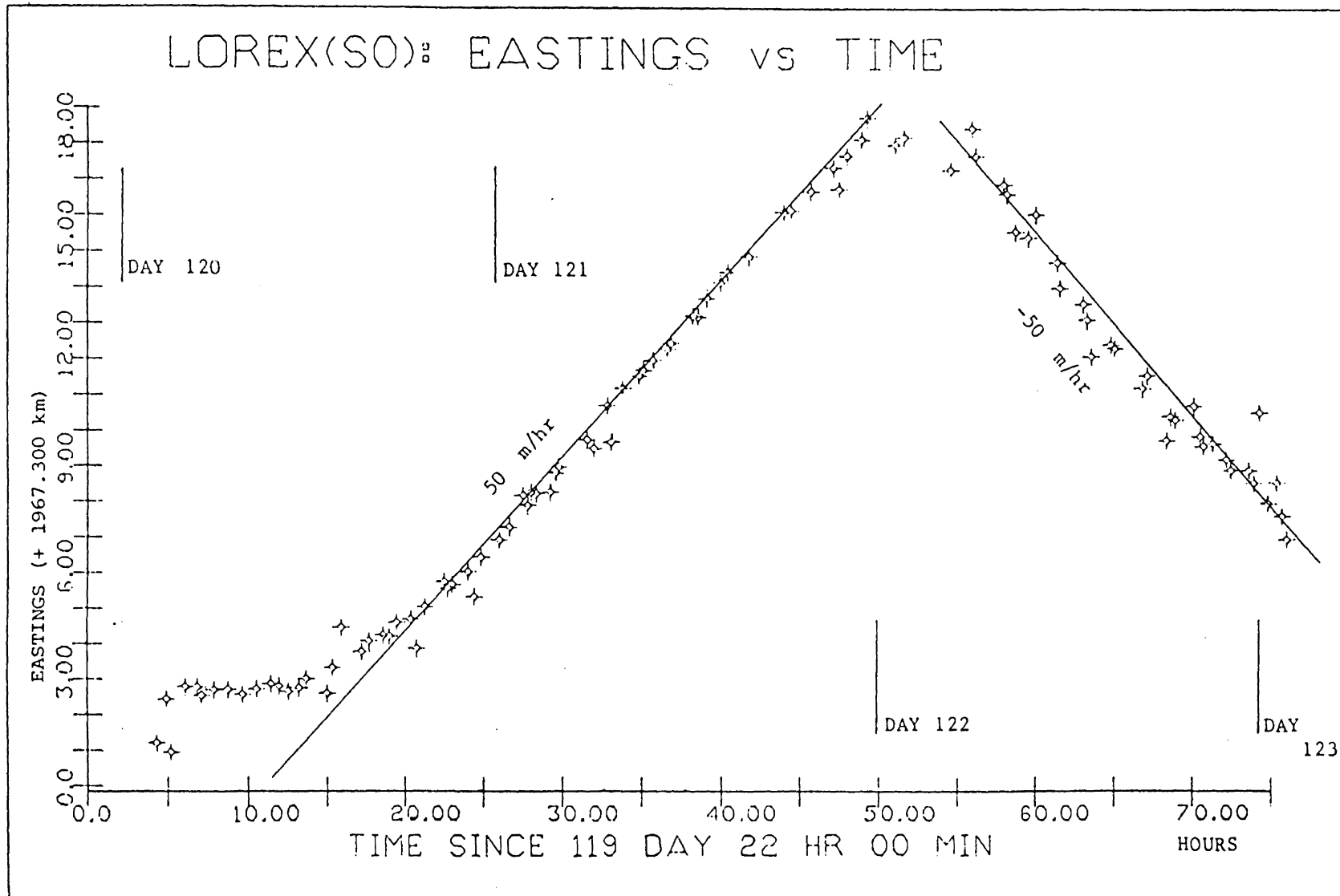


FIGURE V-6 OBSERVED POSITIONS OF TEST DATA SET TWO PORTRAYED IN THE TIME DOMAIN

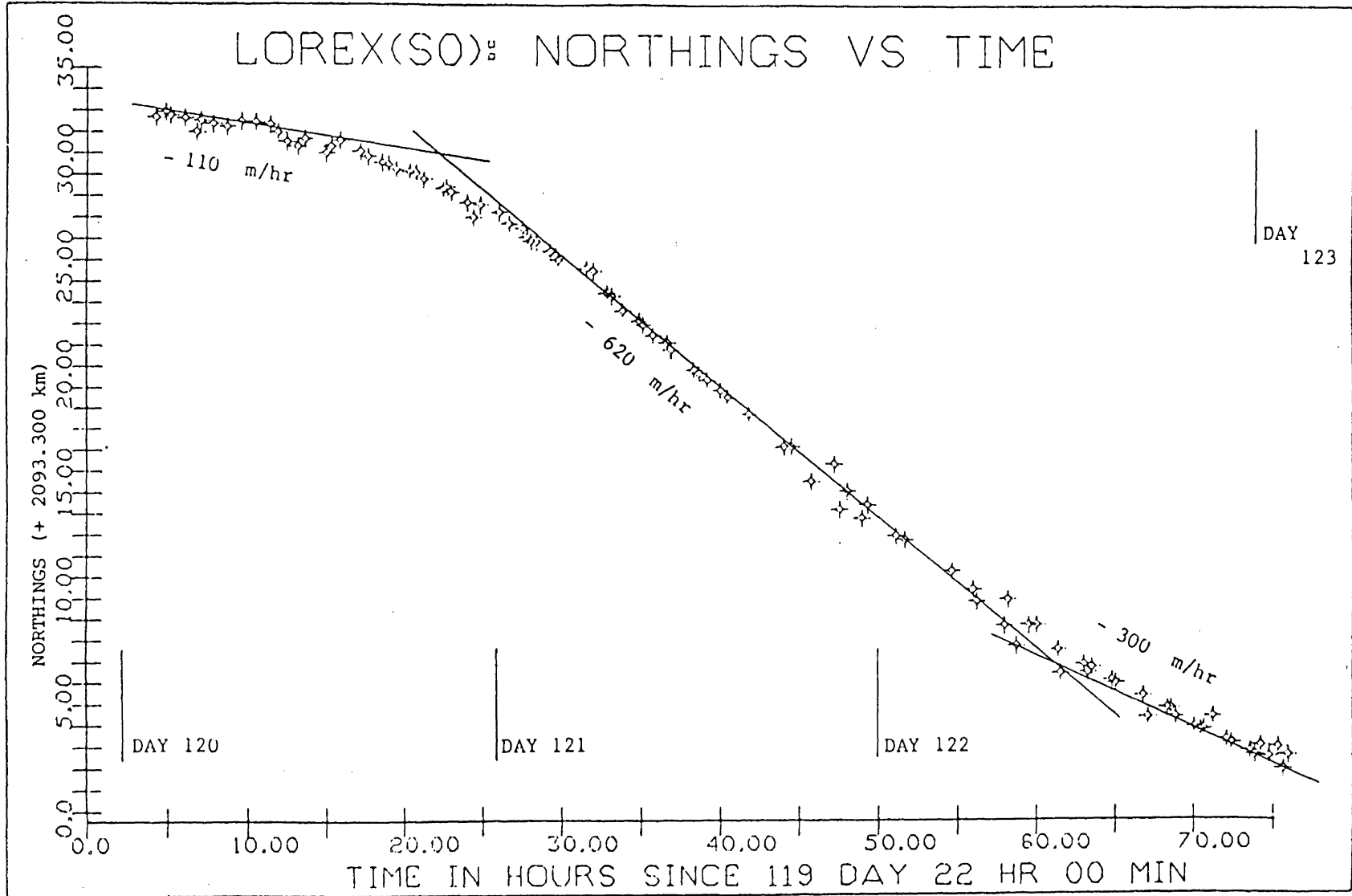


FIGURE V-7 OBSERVED POSITION FIXES OF TEST DATA SET THREE

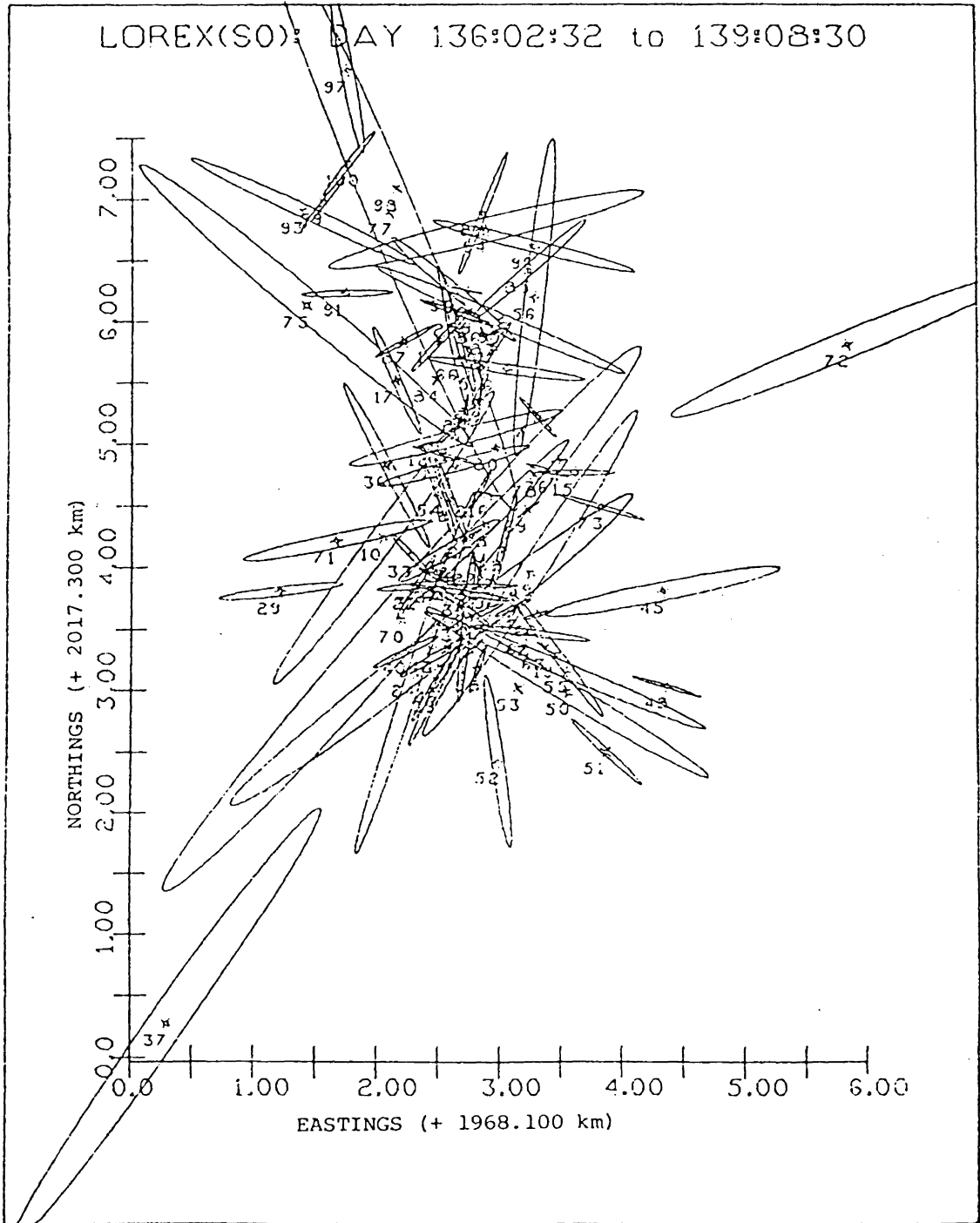


FIGURE V-8 OBSERVED POSITIONS OF TEST DATA SET THREE PORTRAYED IN THE TIME DOMAIN

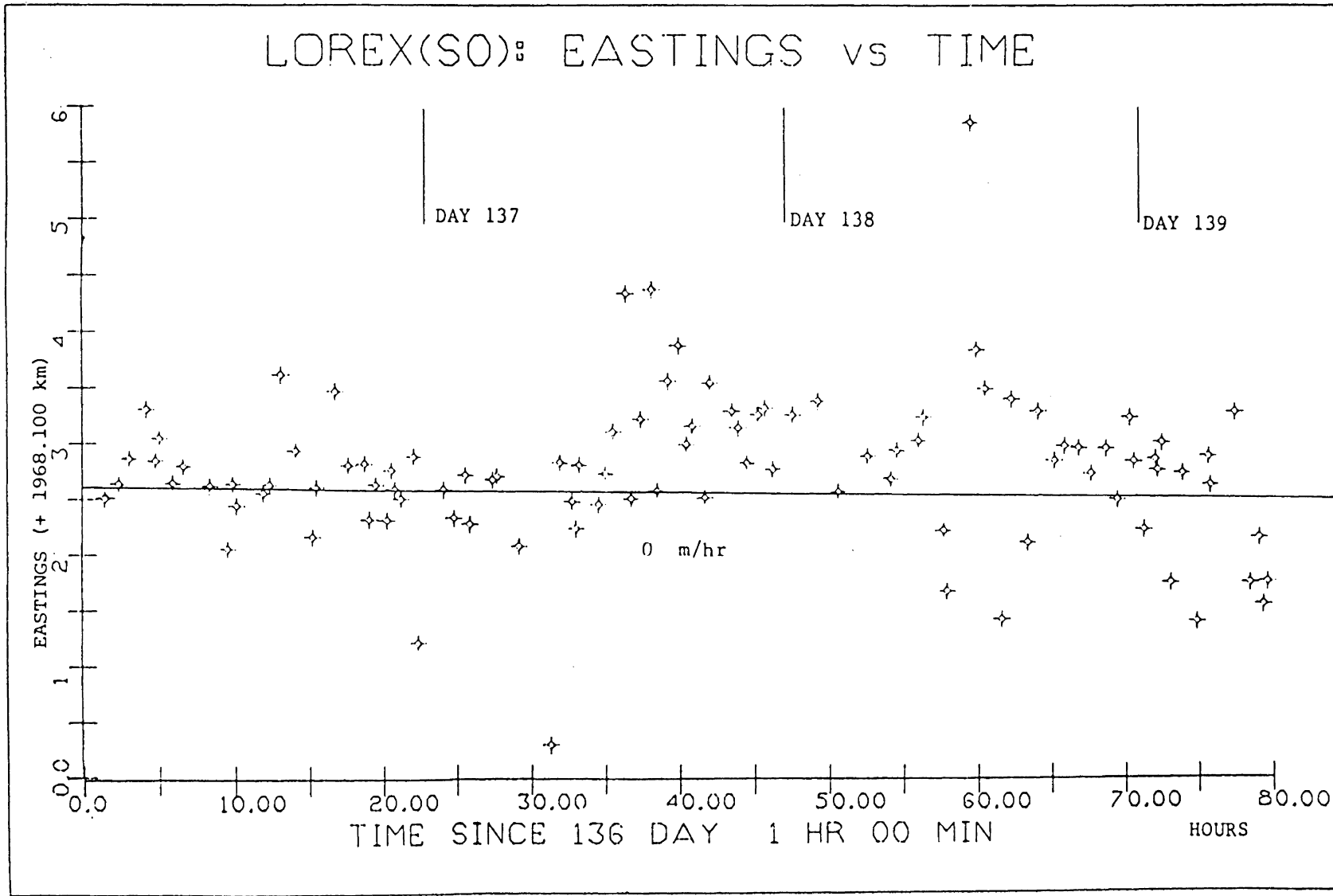
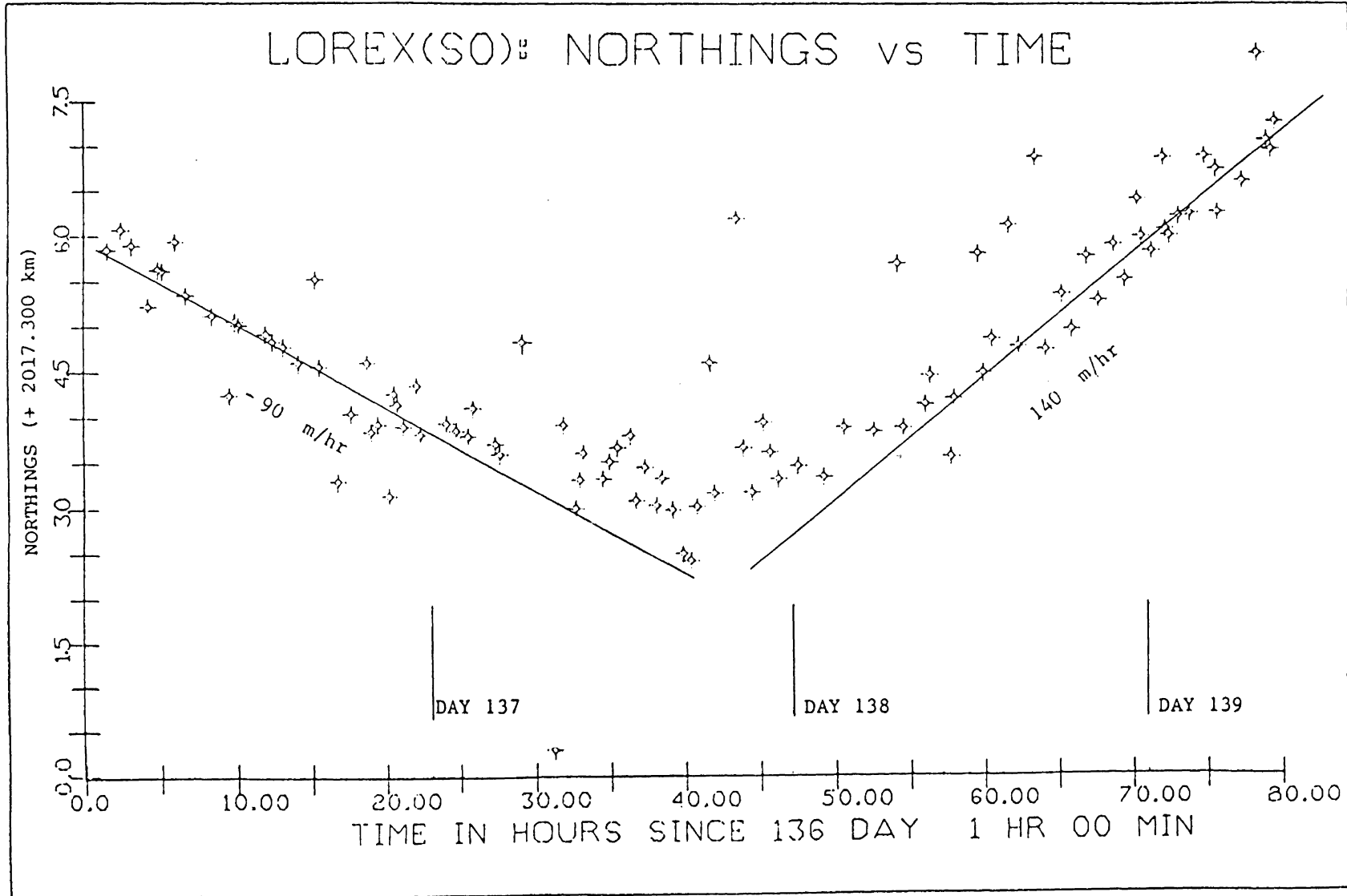


FIGURE V-9 OBSERVED POSITIONS OF TEST DATA SET THREE PORTRAYED IN THE TIME DOMAIN



APPENDIX VI
TRANSFORMATION FROM ERROR ELLIPSES TO
STANDARD DEVIATIONS

In this appendix, the algorithm used to transform the parameters of an error ellipse to its corresponding standard deviation is described.

The following are the assumed knowns and unknowns (Figure VI-1)

Known

- a - semi-major axis of the error ellipse
- b - semi-minor axis of the error ellipse
- γ - direction of semi-major axis of error ellipse with respect to the x-axis (or $90^\circ - \theta$; with θ being the azimuth of the semi-major axis of the error ellipse).

Unknown

- σ_x - standard deviation along the x - axis
- σ_y - standard deviation along the y - axis
- σ_{xy} - covariance between coordinates.

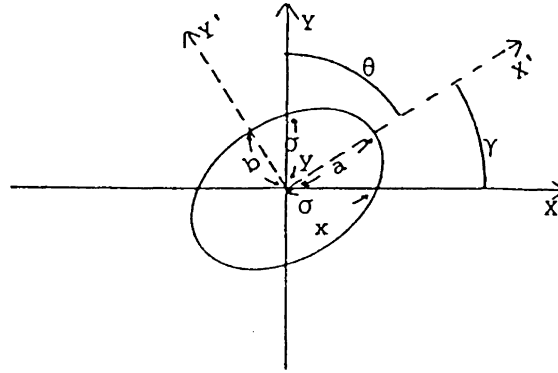


FIGURE VI-1 Relationship Between Error Ellipse and Covariance Matrix.

The transformation from the error ellipse (i.e. a , b and γ) to the covariance matrix (i.e. σ_x , σ_y and σ_{xy}) is achieved using rotation matrices, i.e.

$$\begin{bmatrix} x \\ y \end{bmatrix} = R(-\gamma) \begin{bmatrix} x' \\ y' \end{bmatrix} \quad - \text{(VI-1)}$$

where

$$R(-\gamma) = \begin{bmatrix} \cos \gamma & -\sin \gamma \\ \sin \gamma & \cos \gamma \end{bmatrix}$$

is the negative rotation matrix for the coordinate axes.

Now, the covariance matrix in the $x' y'$ coordinate system can be written as:

$$C_{x'y'} = \begin{bmatrix} a^2 & 0 \\ 0 & b^2 \end{bmatrix}$$

Therefore, using the covariance law (as outlined in Chapter 8):

$$\begin{aligned} C_{xy} &= R(-\gamma) C_{x'y'} R(-\gamma)^T \\ &= R(-\gamma) C_{x'y'} R(\gamma) \end{aligned} \quad - \text{(VI-2)}$$

or

$$\begin{bmatrix} \sigma_x^2 & \sigma_{xy} \\ \sigma_{xy} & \sigma_y^2 \end{bmatrix} = \begin{bmatrix} \cos \gamma & -\sin \gamma \\ \sin \gamma & \cos \gamma \end{bmatrix} \begin{bmatrix} a^2 & 0 \\ 0 & b^2 \end{bmatrix} \begin{bmatrix} \cos \gamma & \sin \gamma \\ -\sin \gamma & \cos \gamma \end{bmatrix} \quad - \text{(VI-3)}$$

In terms of θ , we have

$$C_{xy} = R(\theta - 90^\circ) C_{x'y'}, R(90^\circ - \theta) \quad - \text{(VI-4)}$$

Rearranging equations (VI-3),

$$\begin{aligned} \sigma_x &= [\tfrac{1}{2}(a^2 + b^2 + 2\sigma_{xy} \cot 2\gamma)]^{\frac{1}{2}} \\ \sigma_y &= [\tfrac{1}{2}(a^2 + b^2 - 2\sigma_{xy} \cot 2\gamma)]^{\frac{1}{2}} \\ \text{and } \sigma_{xy} &= \tfrac{1}{2}(a^2 - b^2) \sin 2\gamma \end{aligned} \quad - \text{(VI-5)}$$

(Note: If the azimuth (θ) is given instead of γ , replace γ by $(90^\circ - \theta)$ in equations (VI-5)).

Appendix VII
ALGORITHM DESIGN, IMPLEMENTATION AND COMPUTER
LISTINGS

In this appendix, the general flow of the algorithm, together with any special considerations made are mentioned.

The basic structure of the program is given in Figure VII-1. The routines are classified into "levels"; with the following definitions:

Level I - routines called only once to perform a specific task.

Level II - routines called more than once, but of a specialised nature.

Level III - routines called extensively by other routines.

Displayed in Figure VII-1 are all level I subroutines called during the processing of a data set and with the order of execution being from the left to right. A complete description of the function of each routine, along with the input and output parameters and external routines called, are given in their computer listings. The list of 64 subroutines developed for this thesis, together with a short description and external routines called are given in Table VII-1.

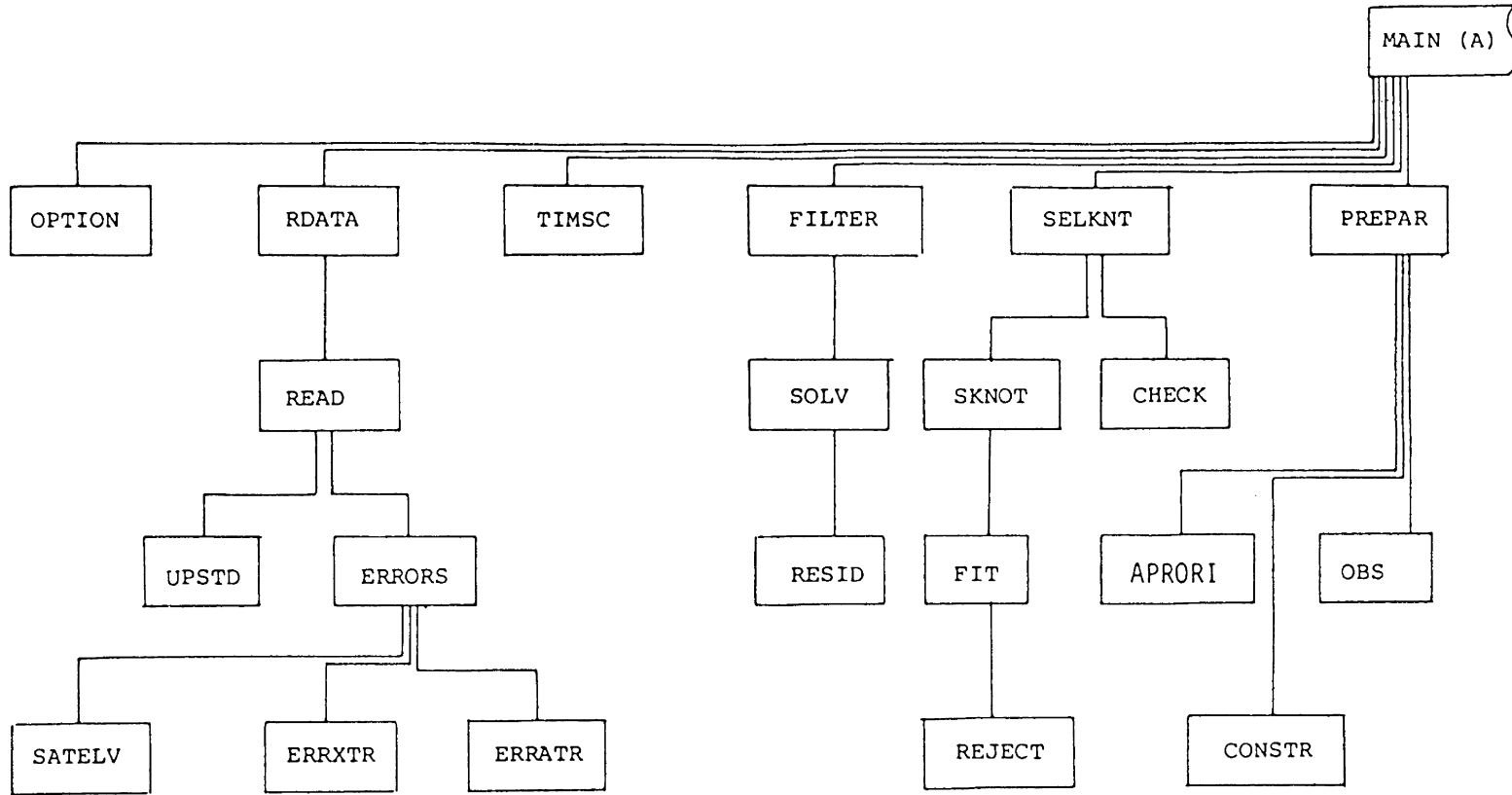


FIGURE VII - 1a Basic Structure of the DSPLIN Program

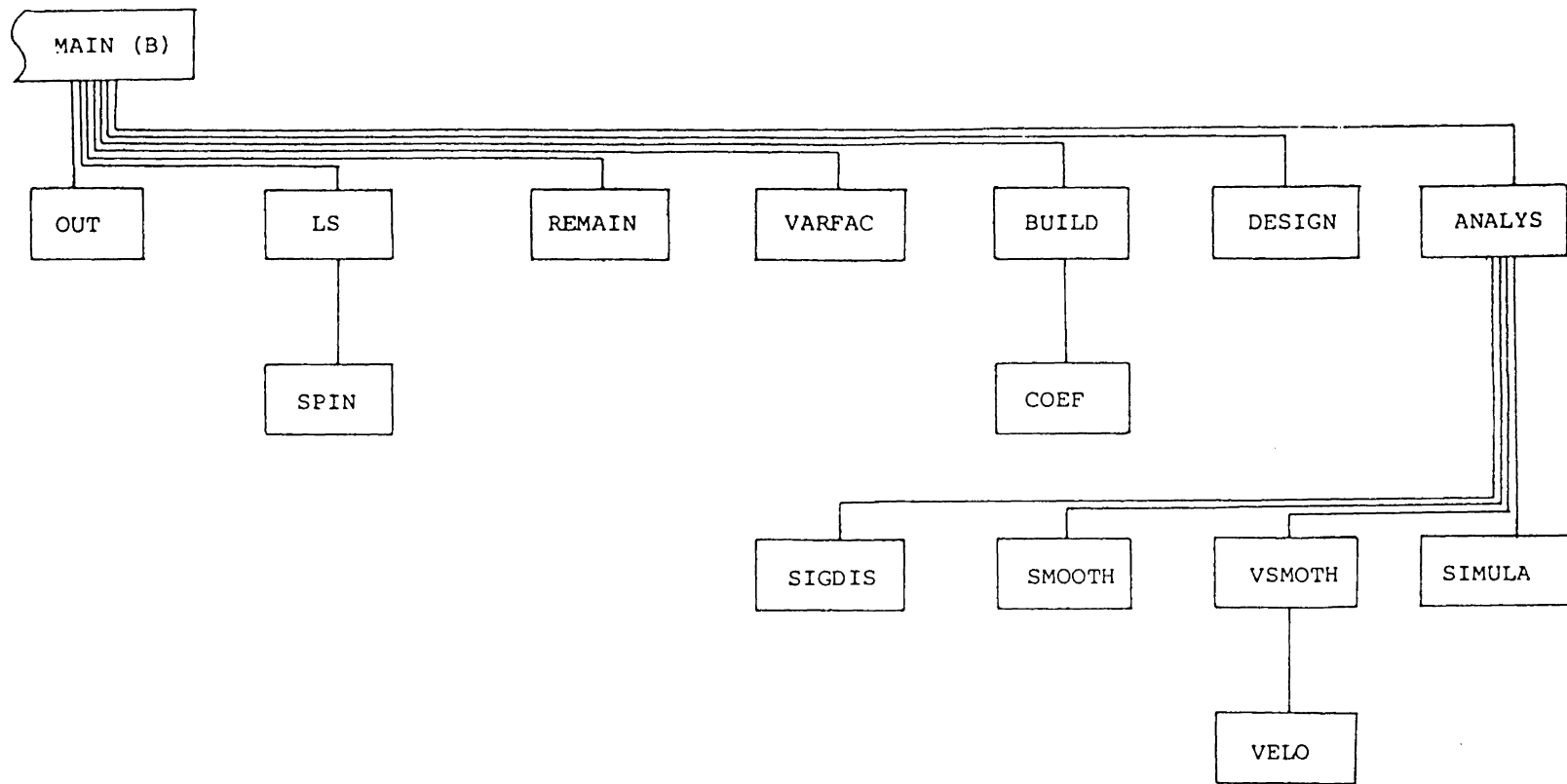


FIGURE VII - 1b Basic Structure of the DSPLIN Program

TABLE VII-1

List and Description of Subroutines

I) Level I subroutines

Name	Description and external routines called
ANALYS	: Plots the different components of the least-squares residuals and printing of smoothed data series at equal time intervals. Calls - CTIME, DSHLNS, DSQRT, ELIPSE, ENDPLT, NOWPLT, PCOPY, PLOT, POINT, PRNTCH, SCMULT, SIGDIS, SIMULA, SMOOTH, VSMOTH,
APRORI	: Reads or generates an a priori solution vector for the least-squares adjustment. Calls - none
BUILD	: Transforms position and velocity knot vectors into cubic coefficients. Driver routine for COEF. Calls - COEF, DPRINT, PCOPY
CHECK	: Checks the number of data points per cubic knot interval and drops superfluous knots. Calls - INTERV
COEF	: Transforms a set of adjacent knot vectors into cubic coefficients defining the interval between the two knots. Calls - DMULT
CONSTR	: Generate the coefficients of a constraint equation. Calls - none
DESIGN	: Display of knots, data points and smoothed points at time series plots, individually or overlaid in the Polar Stereographic Coordinate system. Calls - CIRCLE, DSHLNS, DSQRT, ELIPSE, ELLIPS, ENDPLT, NMBR, NOWPLT, PLOT, POINT, PRNTCH, RADD, SPSYMB
ERRATR	: Computes along track fix error due to estimated receiver motion and height errors. Calls - DSQRT

TABLE VII-1 - cont'd

ERRXTR	:	Computes cross track fix error due to estimated receiver motion and height errors. Calls - DSQRT
ERRORS	:	Modify input formal covariance matrices based on computed fix errors in the along and cross track directions of the passing satellite. Calls - DCOS,DSIN,ELIPSE,ELLSIG,ERRATR,ERRXTR,SATELV
FILTER	:	Linear filter routine for detection of outliers. Calls - DSQRT,DABS,SOLV
FIT	:	Cubic curve fitting using weighted beginning position and slope vectors. Calls - CHOLD,OBS,REJECT
LS	:	Least-squares adjustment of the functionally constrained least-squares model. Calls - COND,DABS,SPIN
LS2	:	Least-squares adjustment using the method of elimination of constraints. Calls - CHOLD,COND,DINV,DMAG,DMULT,DPRINT,PCOPY,SCMULT
OBS	:	Generate the coefficients of an observation equation. Calls - none
OPTION	:	Allow user changes to any or all of the default options, parameters or constants. Calls - ELSFAC
OUT	:	Print banded observation or constraint design matrix, formal covariance matrices of data points, banded weight matrix, knot times and knot time intervals. Calls - DPRINT
PREM	:	Permutation of the a posteriori covariance matrix computed using LS2 to as if it is produced by LS. Calls - none

TABLE VII-1 - cont'd

PREPAR	:	Formulate design matrices and misclosure vectors for the functionally constrained least-squares model. Calls - APRORI, CONSTR, DCLEAR, INTERV, OBS
RDATA	:	Read input data points and end knot vectors. Constructs the banded weight matrix. Driver routine for READ. Calls - CHOLD, READ
READ	:	Read in one line of input data. Modify formal covariances if requested. Calls - DABS, ERRORS, UPSTD
REJECT	:	Perform tests on the estimated residuals based on selected curve fitting rejecting criteria. Calls - CHITES
RESID	:	Compute the residual vector in least-squares adjustment with banded design matrix. Calls - none
REMAIN	:	Compute observation and constraint residuals of the functionally constrained least-squares model. Calls - DMAG
SATELV	:	Compute maximum satellite elevation. Calls - DATAN2, DCOS, DSIN, RTOP
SELKNT	:	Selection of knot generation scheme and prints number of data points in each knot interval. Calls - CHECK, SKNOT
SIGDIS	:	Evaluate if the input data point falls to the right or left of the smoothed series of positions. Calls - DATAN2, DSQRT, POINT
SIMULA	:	Generate simulated data series (without any superimposed noise). Calls - DSIN
SKNOT	:	Driver routine for FIT. Calls - FIT
SMOOTH	:	Computes smoothed positions and precision estimates from the cubic coefficients and its covariance matrix. Calls - ELIPSE, DSQRT, POINT, RADD

TABLE VII-1 - cont'd

SPIN	:	Positive-definite symmetrical matrix inversion Calls - DABS,DLOG10
SOLV	:	Least-squares adjustment with a banded design matrix. Calls - BMULT1,CHOLD,COND,DMAG,RESID,SCMULT
TIMSC	:	Scaling of data point and knot times. Calls - SCMULT
TRNSFM	:	Rearrangement of design matrices produced for the functionally constrained least-squares technique to the least-squares method using the elimination of constraints model. Calls - DCLEAR
UPSTD	:	Scaling of a formal covariance matrix accord- ing to the minimum allowable semi-minor axis of error ellipse. Calls - ELIPSE,ELLSIG
VARFAC	:	Compute and performs the Chi-squared test on the a posteriori variance factor of the func- tionally constrained least-squares model. Calls - DABS,CHITES,BMULT1
VELO	:	Compute the smoothed velocity and associated covariance matrix from the cubic coefficients. Calls - DABS,DATAN2,DMULT,DSQRT,INTERV
VSMOTH	:	Compute a data series of smoothed velocities at input data times. Driver routine for VELO. Calls - RADD,VELO

II) Level II subroutines

Name	Description and external routines called
CHITES	: Perform the Chi-squared statistical test on the a posteriori variance factor. Calls - MDCHI
CHOLD	: Matrix inversion using the Choleski algorithm. Calls - DABS,DSQRT,TRAPS

TABLE VII-1 - cont'd

COND	:	Compute the condition number of a matrix. Calls - none
CTIME	:	Convert time in days and decimals of a day to days, hours and minutes. Calls - none
DINV	:	Inversion routine for a square non-symmetric matrix. Calls - DBLE
ELIPSE	:	Compute the parameters of an error ellipse from its covariance matrix. Calls - DSQRT,DATAN2
ELLSIG	:	Compute the covariance matrix from the error ellipse. Calls - DTAN,DSQRT
ELSFAC	:	Compute the scale factor for non-standard error ellipses. Calls - MDCHI
FORM	:	Formulate the transformation matrix to convert cubic coefficients to smoothed positions. Calls - none
INTERV	:	Locate the interval in which a data point lies within the knot structure. Calls - DABS
PLOT	:	Set up plot specifications, draw axes and titles. Calls - AREA,AXS,CHRPRT,RECT
POINT	:	Compute smoothed position and associated covariance matrix at any given time. Calls - FORM,INTERV,DMULT,TRAPS
PRNKNT	:	Print the position and slope vectors, and covariance matrix for any specified knot time. Calls - DSQRT

TABLE VII-1 - cont'd

RADD : Convert radians to degrees.
Calls - none

RTOP : Convert differences in plane coordinates to
polar coordinates.

III) Level III subroutines

Name	Description and external routines called
BMULT1	: Multiply a banded matrix with a full matrix. Calls - none
DADD	: Add two matrices. Calls - none
DCLEAR	: Set all elements in a matrix to zero. Calls - none
DCOPY	: Copy a matrix. Calls - none
DMAG	: Seek the largest or smallest element in a matrix. Calls - DABS
DMULT	: Multiply two matrices. Calls - none
DPRINT	: Print the elements of a matrix with a user specified title. Calls - SPACE
DSUBT	: Subtract two matrices. Calls - none.
DTRAN	: Transpose a matrix. Calls - none
PCOPY	: Copy one part of a matrix into another part of a matrix. Calls - none
SPACE	: Create blank lines. Calls - none

TABLE VII-1 - cont'd

IV) Other library routines used.

Name	Description of routines
A) FORTRAN library with plotting routines	
AREA	: Physical plot area specification.
AXS	: Draw plot axes.
CHRPRT	: Draw a sequence of characters.
CIRCLE	: Draw a circle.
DABS	: Absolute value of a variable.
DATAN2	: Arc tangent of an angle based on sides of a right-angle triangle.
DBLE	: Conversion from single to double precision.
DCOS	: Cosine of an angle.
DLOG10	: Logarithm to the base 10.
DSIN	: Sine of an angle.
DSQRT	: Square root.
DTAN	: Tangent of an angle.
ELLIPS	: Draw an ellipse.
ENDPLT	: Terminate plotting.
NMBR	: Draw numbers on plot.
NOMPLT	: Plotter pen movement commands.
PRNTCH	: Line printer character to be used for plotting.
RECT	: Draw a rectangle.
TRAPS	: Error trap routine.

[Reference : Gujar, U.G. 1981 and IBM 1974]

B) IMSL library routines

MDCHI	: Inverse Chi-squared probability density function.
-------	---

[Reference : IMSL 1975]

The program is designed to be as modular as possible. This allows modifications to any of the routines to be done with relative ease. Certain routines are incorporated into the algorithm to take advantage of the uniqueness of the computations. They fall mainly into the category of reducing the enormous array storage requirements of the technique.

The design and weight matrices are kept as banded matrices. The design matrices (\underline{A}_1 and \underline{A}_2 - see Section 7.3.1) are stored using variable profile banding techniques. A further reduction is obtained (i.e. only one-half of the total rows of the design matrices are actually kept) by exploiting the similarities in the coefficients between adjacent rows. The weight matrix, on the other hand, uses a fixed bandwidth scheme to optimise storage. The extensive use of pointers reduces the computational cost (i.e. removing all multiplications outside the bandwidth) and allows the location of the desired elements in a matrix.

DSPLIN uses the SPIN routine for matrix inversion in the functionally constrained least-squares algorithm. This is a full matrix inversion routine. The use of a banded matrix inversion routine cuts down the processing time used in computing the inverses by a factor of b^2/n^2 ; where n is the order of the matrix and b is the bandwidth [Steeves 1974]. More studies are needed before a banded matrix inversion routine can be used. Unlike the normal least-squares

adjustment, the functionally constrained least-squares algorithm requires the inversion of two matrices. The interrelationship between these inverses and the solution vector has to be investigated before a banded inversion routine can be used.

Figure VII-2 shows the processing time of DSPLIN against the number of knots used in the data span. The processing time, however, varies with the options for a particular run.

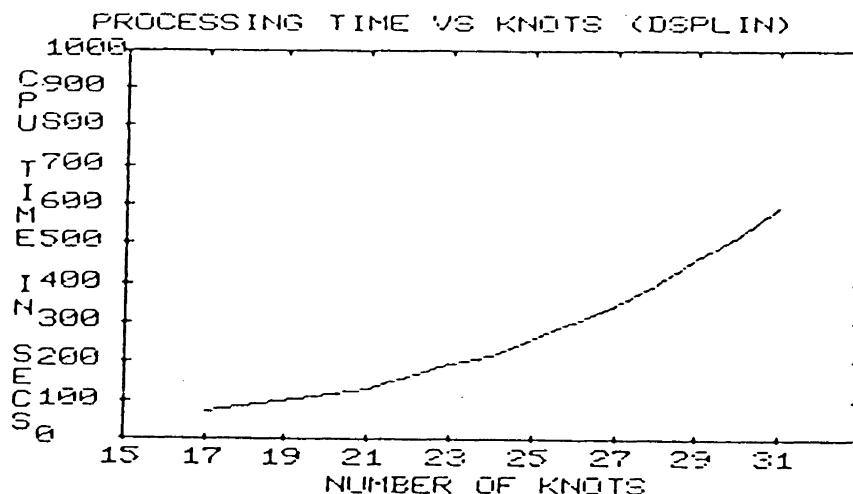


FIGURE VII-2 Processing Times of DSPLIN

Finally, given below, is the general outline of the processing sequence within the algorithm (see Figure VII-1).

1. Selection of options.
(Routine: OPTION)
2. Input and pre-processing of data for smoothing.
(Routines: RDATA, TIMSC and FILTER)

3. Selection of knot scheme.
(Routine: SELKNT)
4. Formulation and printing of design matrices and misclosure vectors
(Routines: PREPAR and OUT)
5. Computation of least-squares estimates using the functionally constrained least-squares model.
(Routines: LS, REMAIN and VARFAC)
6. Generation of time-tagged coefficients and associated covariance matrices for each knot interval.
(Routine: BUILD)
7. Generation of smoothed points, velocities, plotting of smoothed and raw data points or the analysis of residuals.
(Routines: DESIGN and ANALYS)

The displays of raw and smoothed data points are made possible by several plot routines. A complete description of the possible options is included in the computer listings (i.e. in routines ANALYS and DESIGN).

Input to the program is described in the program listings and free format is used to read all variables.


```

00049 C* LINE SHOULD CONTAIN THE 1ST DERIVATIVES AND THEIR VARIANCES *DSPLIN
00050 C* AND CORRELATION IN THE FORMAT 'X1 Y1 SIGX1 SIGY1 CORRXY1. *DSPLIN
00051 C* CUPRENT SETTING: *DSPLIN
00052 C* MAXIMUM NUMBER OF DATA POINTS PROGRAM CAN TAKE *DSPLIN
00053 C* (DETERMINED BY ARRAY DECLARATION) = 500 *DSPLIN
00054 C* MAXIMUM NUMBER OF KNOTS THAT THE PROGRAM CAN *DSPLIN
00055 C* (DETERMINED BY ARRAY DECLARATION) = 32 *DSPLIN
00056 C* GENERALLY: *DSPLIN
00057 C* VARIABLES BEGINNING WITH 'ID' OR 'JD' DENOTES THE INTEGER *DSPLIN
00058 C* DIMENSIONS OF THE RESP MATRIX. *DSPLIN
00059 C* VARIABLES WITH PREFIX 'PR' ARE PRINTING CODES FOR RESP MATRICES. *DSPLIN
00060 C* PLOTTING: *DSPLIN
00061 C* PROGRAMS SUPPORTS ONE DATA SET WITH OVERLAYING PLOTS OR MULTIPLE *DSPLIN
00062 C* DATA SETS AND SEPERATE PLOTS FOR EACH DATA SET. TO UPGRADE *DSPLIN
00063 C* PROGRAM TO HANDLE MULTIPLE DATA SETS WITH OVERLAYING CAPABILITIES *DSPLIN
00064 C* MODIFY CALL ROUTINES PLOT AND ENDPLT IN MAIN, SUBR ANALYS AND *DSPLIN
00065 C* SUBR DESIGN. *DSPLIN
00066 C* *DSPLIN
00067 C***** *DSPLIN
00068 C VARIABLE NAMES : DESCRIPTION *DSPLIN
00069 C *DSPLIN
00070 C M : NUMBER OF UNKNOWNNS *DSPLIN
00071 C N : NUMBER OF OBSERVATION EQUATIONS *DSPLIN
00072 C P : FIXED BANDWIDTH WEIGHT MATRIX *DSPLIN
00073 C R : NUMBER OF CONSTRAINT EQUATIONS IN SECONDARY MODEL *DSPLIN
00074 C V : RESIDUAL VECTOR OF OBSERVABLES *DSPLIN
00075 C X : LS SOLUTION VECTOR *DSPLIN
00076 C A1 : VARIABLE PROFILE BANDWIDTH OBSERVATION (PRIMARY) DESIGN MATRIX *DSPLIN
00077 C A2 : VARIABLE PROFILE BANDWIDTH CONSTRAINT (SECONDARY)DESIGN MATRIX *DSPLIN
00078 C NO : NUMBER OF DATA POINTS *DSPLIN
00079 C SC : INVERSE OF THE SCALE FACTOR FOR THE TIME DOMAIN *DSPLIN
00080 C S0 : APCSTERIORI VARIANCE FACTOR *DSPLIN
00081 C TK : VECTOR OF KNOT TIMES *DSPLIN
00082 C TX : VECTOR OF DATA TIMES *DSPLIN
00083 C VX : COVARIANCE MATRIX OF LS ESTIMATES *DSPLIN
00084 C V2 : RESIDUAL VECTOR OF CONSTRAINTS *DSPLIN
00085 C W1 : OBSERVATION MISCLOSURE VECTOR *DSPLIN
00086 C W2 : CCNSTRRAINT MISCLOSURE VECTOR *DSPLIN
00087 C XC : APRIORI SOLUTION VECTOR *DSPLIN
00088 C COF : MATRIX OF COEFFICIENTS DEFINING CUBICS *DSPLIN
00089 C DTK : VECTOR CONTAINING KNCT TIME INTERVALS *DSPLIN
00090 C ESC : SCALE FACTOR AT ALPHA PERCENT CONFIDENCE INTERVAL *DSPLIN
00091 C IDP : DIM DEC FOR P MATRIX *DSPLIN
00092 C IDV : DIM DEC FOR V VECTOR *DSPLIN
00093 C IDX : DIM DEC FOR X VECTOR *DSPLIN
00094 C IER : ERROR CODE USUALLY ASSOCIATED WITH INVERSES *DSPLIN
00095 C IRD : READ UNIT *DSPLIN
00096 C IWR : WRITE UNIT *DSPLIN

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00097	C	KNO	:	NUMBER OF KNOTS	DSPLIN
00098	C	VAR	:	HYPER MATRIX OF INPUT DATA POINT COVARIANCE MATRICES	DSPLIN
00099	C	ACON	:	WORK ARRAY OF SUBR CONSTR	DSPLIN
00100	C	ALPH	:	LEVEL OF SIGNIFICANCE TESTS - SEE SUBR FILTER	DSPLIN
00101	C	AOBS	:	WORK ARRAY OF SUBR CBS	DSPLIN
00102	C	DINC	:	INTERVAL INCREMENT - SEE SUBR FILTER	DSPLIN
00103	C	DINT	:	INTERVAL WIDTH - SEE SUBR FILTER	DSPLIN
00104	C	DRAW	:	SPLINE DRAWING - SEE SUBR DESIGN	DSPLIN
00105	C	ECHO	:	INPUT ECHO OPTION	DSPLIN
00106	C	FESC	:	SCALE FACTOR RELATED TO VARIABLE ALPH	DSPLIN
00107	C	GINT	:	INTERVAL BETWEEN SMOOTHED PARAMETERS - SEE SUBR ANALYS	DSPLIN
00108	C	ICOL	:	FUNCTION - COLUMN POINTERS FOR A1 AND A2 MATRICES	DSPLIN
00109	C	IDA1	:	ROW DIM DEC OF A1 MATRIX	DSPLIN
00110	C	IDA2	:	ROW DIM DEC OF A2 MATRIX	DSPLIN
00111	C	IDTK	:	DIM DEC FOR TK VECTOR	DSPLIN
00112	C	IDTX	:	DIM DEC FOR TX VECTOR	DSPLIN
00113	C	IDVX	:	DIM DEC FOR VX MATRIX	DSPLIN
00114	C	IDV2	:	DIM DEC FOR V2 VECTOR	DSPLIN
00115	C	IDW1	:	DIM DEC FOR W1 VECTOR	DSPLIN
00116	C	IDW2	:	DIM DEC FOR W2 VECTOR	DSPLIN
00117	C	IDX0	:	DIM DEC FOR X0 VECTOR	DSPLIN
00118	C	IFLT	:	CALL CODE FOR FILTER ROUTINE - SEE SUBR OPTION	DSPLIN
00119	C	IRCW	:	FUNCTION - RCW POINTERS FOR A1 AND A2 MATRICES	DSPLIN
00120	C	ISCT	:	CALL CODE FOR TIME SCALING - SEE SUBR OPTION	DSPLIN
00121	C	LCBS	:	VECTOR CONTAINING ALL OBSERVABLES	DSPLIN
00122	C	PRTK	:	PRINT CODE FOR TK VECTOR	DSPLIN
00123	C	PRTX	:	PRINT CODE FOR TX VECTOR	DSPLIN
00124	C	TKRD	:	CODE ON KNCT TYPE	DSPLIN
00125	C	VCOF	:	COVARIANCE MATRIX FOR COEFFICIENTS (CCF)	DSPLIN
00126	C	VTWV	:	QUADRATIC NORM OF RESIDUALS	DSPLIN
00127	C	XINT	:	PLOTTING SPLINE IN XINT INCREMENTS - SEE SUBR DESIGN	DSPLIN
00128	C	ADDA1	:	ADDRESS SEQUENCE FOR A1 MATRIX	DSPLIN
00129	C	ADDA2	:	ADDRESS SEQUENCE FOR A2 MATRIX	DSPLIN
00130	C	ALPHA	:	PERCENTAGE CONFIDENCE LEVEL OF DRAWN ELLIPSES	DSPLIN
00131	C	DEGOF	:	DEGREES OF FREEDOM IN CURRENT MODEL	DSPLIN
00132	C	GOATE	:	SUBP - GETS DATE FOR RUN (FORTRAN LIBRARY)	DSPLIN
00133	C	IAPRI	:	CALL CCDE ON SUBR APRIORI - SEE SUBR APRIORI	DSPLIN
00134	C	IDCOF	:	ROW DIM DEC FOR COF MATRIX	DSPLIN
00135	C	IDOTK	:	DIM DEC FOR DTK VECTOR	DSPLIN
00136	C	IDVAR	:	ROW DIM DEC FOR VAR MATRIX	DSPLIN
00137	C	IPLOT	:	PLOTTING OPTIGN CODE - SEE SUBR OPTION	DSPLIN
00138	C	IREAD	:	READ FORMAT CODE - SEE SUBR READ	DSPLIN
00139	C	IRJET	:	TOTAL NO OF FAILURES BY REJECTION - SEE SUBR REJECT	DSPLIN
00140	C	ITYPE	:	PRINTER PLOT CR GRAPHIC PLOT	DSPLIN
00141	C	NINTY	:	90 DEG IN RADIAN	DSPLIN
00142	C	PRCOV	:	PRINT CODE FOR INPUT COVARIANCES OF DATA POINTS	DSPLIN
00143	C	PRDTX	:	PRINT CODE FOR KNOT INTERVAL TIMES	DSPLIN
00144	C	PRGEN	:	PRINT CODE FOR SMOOTHED POINTS USED IN DRAWING SPLINE	DSPLIN

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00145 C PRKNT : SELECTIVE PRINTING OF KNOT INFORMATION DSPLIN
00146 C PRPTS : PLOTTING CCODE CN DATA POINTS DSPLIN
00147 C SPLIN : CALL CCODE CN SUBR DESIGN DSPLIN
00148 C ALPKNT : LEVEL OF SIGNIFICANCE TO BE USED IN REJECT ROUTINE DSPLIN
00149 C CALPHA : PERCENTAGE LEVEL OF SIGNIFICANCE TO BE USED IN SUDR VARFAC DSPLIN
00150 C CHANGE : DIFFERENT DATA SETS - SEE SUBR OPTION DSPLIN
00151 C FORFIV : 45 DEGREES IN RADIANS DSPLIN
00152 C GSTART : TIME TO BEGIN GENERATION OF SMOOTH PARAMETERS - SUBR ANALYS DSPLIN
00153 C IANLYS : CALL CODE FOR ANALYS SUBROUTINE DSPLIN
00154 C ICANYS : OPTION VECTOR OF CCODES FOR ANALYS ROUTINE DSPLIN
00155 C ICHECK : CODE FOR CHECK ROUTINE - SEE CHECK SUBROUTINE DSPLIN
00156 C ICKNOT : OPTION CODE ON KNOT GENERATION ROUTINE - SEE SKNOT ROUTINE DSPLIN
00157 C ICOUNT : NUMBER OF PROCESSED DATA SETS DSPLIN
00158 C IDKNOT : MAXIMUM NUMBER OF KNOTS THE PROGRAM CAN HANDLE DSPLIN
00159 C IDLOBS : DIM DEC FOR LCBS VECTOR DSPLIN
00160 C IDVCOF : ROW DIM DEC FOR VCOF MATRIX DSPLIN
00161 C IELIPS : CODE ON PLOTTED ELLIPSES - SEE OPTION SUBR DSPLIN
00162 C ICBSNO : MAX NUMBER OF OBSERVED SADA POINTS THE PROGRAM CAN MANAGE DSPLIN
00163 C ITOTAL : TOTAL NUMBER OF DATA SETS TO BE PROCESSED DSPLIN
00164 C PRMAT : PRINT CODE FOR A1 AND A2 MATRICES DSPLIN
00165 C PRCOFF : PRINT CODE FOR COEFFICIENTS OF SPLINE DSPLIN
00166 C PRCOFV : PRINT CCODE FOR COVARIANCES OF CCEFFICIENTS DSPLIN
00167 C PRKNOT : PLOTTIG CODE ON KNOTS - SEE DESIGN SUBR DSPLIN
00168 C PRLOBS : PRINT CODE CN LCBS ROUTINE DSPLIN
00169 C PRPMAT : PRINT CODE CN WEIGHT MATRIX DSPLIN
00170 C PRRESO : PRIN CODE ON RESIDUALS DSPLIN
00171 C PRVARX : PRINT CODE ON COVARIANCE OF LS ESTIMATES DSPLIN
00172 C PRXMAT : PRINT CODE ON LS ESTIMATES - X VECTOR DSPLIN
00173 C SCTIME : SCALE FACTOR ON TIME DOMAIN DSPLIN
00174 C XSTART : TIME TO BEGIN DRAWING SPLINE,CO OR SPD - SUBR DESIGN/ANALYS DSPLIN
00175 C
00176 C CALLS - GDATE,CPUTIM (EXTERNAL ROUTINES) DSPLIN
00177 C OPTION,DCLEAR,RCATA,TIMSC,FILTER,SELKNT,PREPAR,OUT, DSPLIN
00178 C LS,VARFAC,SCMULT,DADD,DPRINT,PRNKNT,BUILD,DESIGN,ANALYS DSPLIN
00179 C
00180 C
00181 C*PROGRAM BEGINS DSPLIN
00182 C* COMMON BLK CONTAINING DECLARED MATRIX DIMENSIONS DSPLIN
00183 COMMON /DIM1/IOBSNO,ICA1,IDW1,IDTX,IDP,IDPV,IOLORS,IDVAR,IDV DSPLIN
00184 COMMON /DIM2/IDKNGT,IDA2,IDTK,IDOTK,IDX,IDXV,IDW2,IDX2,IDXC DSPLIN
00185 @ IDCOF, IDVCOF DSPLIN
00186 C* DIMENSION BLK CONTAINING ARRAY DECLARATIONS DSPLIN
00187 REAL*8 A1(504,7),W1(1008,1),TX(502,1),P(1008,3),PV(1008,1), DSPLIN
00188 LCBS(1008,1),VAR(502,2,2),V(1008,1) DSPLIN
00189 REAL*8 A2(30,11),TK(32,1),OTK(31,1),X(128,1), DSPLIN
00190 VX(128,128),W2(60,1),V2(60,1),XO(128,1),COF(31,8),VCOF(31,8,8) DSPLIN
00191 REAL*8 ACBS(7,1),ACON(11,1),MAT(2,2),VTWV, DSPLIN
00192 CX(8,1),VCX(8,8),CC(8,1),VCC(8,8) DSPLIN

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00193 C* WORK ARRAY DIMENSIONS WK1(IDX,IDA2*2) AND WK2(IDA2*2,IDA2*2) DSPL IN
00194 REAL*8 WK1(128,60),WK2(60,60) DSPL IN
00195 C* WORK ARRAYS DSPL IN
00196 C* AS DIMENSIONED IN FIT ROUTINE ;SEE FIT ROUTINE DSPL IN
00197 REAL*8 FWK1(102,7),FWK2(204,3),FWK3(100,2,2),FWK4(8,8),FWK5(8,8), DSPL IN
00198 @ FWK6(200,1),FWK7(8,204) DSPL IN
00199 C* AS DIMENSIONED IN FILTER ROUTINE DSPL IN
00200 REAL*8 FLWK1(20,3),FLWK2(40,3),FLWK3(40,1),FLWK4(40,1),FLWK5(4,4) DSPL IN
00201 C* AS DIMENSIONED IN ANALYS ROUTINE DSPL IN
00202 REAL*8 AWK1(500,1),AWK2(500,1),AWK3(500,1),AWK4(500,1),AWK5(500,1) DSPL IN
00203 C* DSPL IN
00204 INTEGER*4 NC,KNO,R,M,N,L,K,SPLIN,DRAW, DSPL IN
00205 @ ADDA1(504),ADDA2(30),ICANYS(10),ICKNOT(10) DSPL IN
00206 INTEGER*4 PRTX,PRTK,PRDTK,PRLOBS,PRCOV,PRCOFF,PRCOFV,ECHO, DSPL IN
00207 @ PRPTS,PRKNCT,PRMAT,PRPMAT,PRXMAT,PRVARX,PRRESO,PRGEN, DSPL IN
00208 @ CHANGE,IAPRI,TKRD,PRKNT,CEGOF DSPL IN
00209 C* DSPL IN
00210 LOGICAL*1 ITITLE(80),DATE(18),TIME(6) DSPL IN
00211 C* SPACE ECOMCNIZING VIA EQUIVALENCE STATEMENTS DSPL IN
00212 EQUIVALENCE (A2(1),VCOF(1)), DSPL IN
00213 @ (V(1),W1(1)), DSPL IN
00214 @ (V2(1),W2(1)) DSPL IN
00215 EQUIVALENCE (A1(1),CX(1)), DSPL IN
00216 @ (A1(9),VCX(1)), DSPL IN
00217 @ (A1(73),MAT(1)), DSPL IN
00218 @ (A1(77),CO(1)), DSPL IN
00219 @ (A1(85),VCO(1)) DSPL IN
00220 EQUIVALENCE (A1(149),VTWV), DSPL IN
00221 @ (A1(150),XX), DSPL IN
00222 @ (A1(151),YY), DSPL IN
00223 @ (A1(152),CXY) DSPL IN
00224 EQUIVALENCE (WK1(1),DX1), DSPL IN
00225 @ (WK1(2),DX2), DSPL IN
00226 @ (WK1(3),TUME), DSPL IN
00227 @ (WK1(4),DD) DSPL IN
00228 EQUIVALENCE (WK1(5),XLR), DSPL IN
00229 @ (WK1(6),S0), DSPL IN
00230 @ (WK1(7),ACBS(1)), DSPL IN
00231 @ (WK1(15),PV(1)) DSPL IN
00232 EQUIVALENCE (WK1(1100),FWK1(1)), DSPL IN
00233 @ (WK1(1815),FWK2(1)), DSPL IN
00234 @ (WK1(2428),FWK3(1)), DSPL IN
00235 @ (WK1(2829),FWK4(1)), DSPL IN
00236 @ (WK1(2894),FWK5(1)), DSPL IN
00237 @ (WK1(2959),FWK6(1)), DSPL IN
00238 @ (WK1(3160),FWK7(1)) DSPL IN
00239 EQUIVALENCE (WK1(4800),FLWK1(1)), DSPL IN
00240 @ (WK1(4861),FLWK2(1)), DSPL IN

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00241          @          (WK1(4982),FLWK3(1)),          DSPL IN
00242          @          (WK1(5023),FLWK4(1)),          DSPL IN
00243          @          (WK1(5064),FLWK5(1)),          DSPL IN
00244          @          EQUIVALENCE (WK1(5100),AWK1(1)), DSPL IN
00245          @          (WK1(5601),AWK2(1)),          DSPL IN
00246          @          (WK1(6102),AWK3(1)),          DSPL IN
00247          @          (WK1(6603),AWK4(1)),          DSPL IN
00248          @          (WK1(7104),AWK5(1))          DSPL IN
00249          @          EQUIVALENCE (WK2(1),VCOF(331)) DSPL IN
00250 C* DATA ASSIGNMENT          DSPL IN
00251          DATA ITITLE/80*' ',ACON/11*0.0D00/,ICANYS/10*0/ DSPL IN
00252          DATA FCRFIV/0.785398164D0/,NINTY/1.570796327D0/ DSPL IN
00253 C* FUNCTIONS          DSPL IN
00254          IROW(I) = (I+1)/2          DSPL IN
00255          ICOL(I) = (2 - ((I+1)/2 - (I/2))) DSPL IN
00256 C* READ UNIT          DSPL IN
00257          IRD = 5          DSPL IN
00258 C* WRITE UNIT          DSPL IN
00259          IWR = 6          DSPL IN
00260 C* EQUALITIES GOVERNING THE MATRIX SIZES          DSPL IN
00261 C* MAXIMUM NUMBER OF OBSERVATIONS THAT CAN BE TAKEN INTO THE PROGRAM DSPL IN
00262          IOBSNO = 500          DSPL IN
00263 C* MATRIX SIZES ARE AS FOLLOWS          DSPL IN
00264          IOA1 = IOBSNO + 4          DSPL IN
00265          IO*1 = IOBSNO*2 + 8          DSPL IN
00266          IDTX = IOBSNO + 2          DSPL IN
00267          IDP = IOBSNO*2 + 8          DSPL IN
00268          IDPV = IOBSNO*2 + 8          DSPL IN
00269          IDLOBS= IOBSNO*2 + 8          DSPL IN
00270          IDVAR= IOBSNO + 2          DSPL IN
00271          IDV = IOBSNO*2 + 8          DSPL IN
00272 C* MAXIMUM NUMBER OF KNOTS THAT CAN BE TAKEN INTO THE PROGRAM DSPL IN
00273          IOKNOT = 32          DSPL IN
00274 C* MATRIX SIZES ARE AS FOLLOWS          DSPL IN
00275          IOA2 = IOKNOT - 2          DSPL IN
00276          IDTK = IOKNOT          DSPL IN
00277          IDOTK = IOKNOT - 1          DSPL IN
00278          IOX = IOKNOT*4          DSPL IN
00279          IDVX = IOKNOT*4          DSPL IN
00280          ID*2 = IOKNOT*2 - 4          DSPL IN
00281          IDV2 = IOKNOT*2 - 4          DSPL IN
00282          IOXO = IOKNOT*4          DSPL IN
00283          IDCOF = IOKNOT - 1          DSPL IN
00284          IDVCOF= IOKNOT - 1          DSPL IN
00285 C* ADDRESS SEQUENCE OF A1 AND A2 MATRICES FOLLOW THEIR RESP MATRICES DSPL IN
00286 C *** SUBR LS1FCF02 REQS MODIFICATION TO DIM IF NO. OF KNOT CHANGES *** DSPL IN
00287 C* PRINTS THE DATE AND TIME OF RUN          DSPL IN
00288          CALL GOATE(DATE,TIME)          DSPL IN

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00337          @          CALL FILTER(NO,TX,LOBS,P,VAR,DINT,DINC,ALPH,FESC,SCTIME, DSPLIN
00338          @          FLWK1,FLWK2,FLWK3,FLWK4,FLWK5,FLWK6) OSPLIN
00339 C* FORMULATION OF KNOTS OSPLIN
00340          CALL SELKNT(TKRD,KNO,NO,ICHECK,TX,TK,LOBS,VAR,ICKNOT, OSPLIN
00341          @          IRJET,ALPKNT,DTK,DD,FWK1,FWK2,FWK3,FWK4,FWK5,FWK6,FWK7) OSPLIN
00342 C* SET UP MATRICES FOR LS SOLUTION OSPLIN
00343          CALL PREPAR(KNO,NO,R,M,N, TX,TK,DTK,AOBS,ACON, OSPLIN
00344          @          A1,ADDA1,A2,ADDA2, OSPLIN
00345          @          XO,LOBS,W1,W2,IAPRI) OSPLIN
00346 C* PROGRAM OUTPUT SECTION PRIOR TO LS SOLUTION OSPLIN
00347          CALL CUT(KNO,NO,R,M,N, OSPLIN
00348          @          PRTX,PRTK,PRLOBS,PRDTK,PRCOV,PRPMAT,PRMAT, OSPLIN
00349          @          TX,TK,LOBS,DTK,VAR,P,A1,A2,ADDA1,ADCA2) OSPLIN
00350 C* LEAST SQUARES PROCESS OSPLIN
00351          CALL LS(A1,ADDA1,A2,ADDA2,P,W1,W2,X,VX,R,N,M, OSPLIN
00352          @          IDA1,IDA2,IDP,IDW1,IDW2,IDX,IER,WK1,WK2) OSPLIN
00353 C* TERMINATE DATA SET PROCESSING IF INVERSE FAILS OSPLIN
00354          IF(IER.NE.0)GO TO 7000 OSPLIN
00355 C* COMPUTE RESIDUALS OSPLIN
00356          CALL REMAIN(R,M,N,A1,A2,ADDA1,ADDA2,W1,W2, X,V,V2) OSPLIN
00357 C* COMPUTE VARIANCE FACTOR AND DEGREES OF FREEDOM OSPLIN
00358          CALL VARFAC(SO,DEGOF,NO,R,M,N,CALPHA,TX,P,V,PV,VTWV,DX1,DX2) OSPLIN
00359 C* SCALING OF THE COVARIANCE MATRIX = NOTICE THE APOSTERIORI VAR USED. OSPLIN
00360          CALL SCMULT(SO,VX,VX,M,M,IDX,IDX) OSPLIN
00361 C* FC RMS FINAL LEAST SQUARES ESTIMATES OSPLIN
00362          CALL CADD(XO,X,M,1,X,IDX,1) OSPLIN
00363 C* RESULTS OUTPUT SECTION OSPLIN
00364          IF(PRXMAT.EQ.1)CALL DPRINT(X,M,1,IDX,1,'FINAL EST X-VECTOR',9) OSPLIN
00365          IF(PRVARX.EQ.1)CALL CPRINT(VX,M,M,IDX,IDX,'COVARIANCE AF SC',8) OSPLIN
00366 C* PRINT END SLOPE AND KNOT INFORMATION OSPLIN
00367          IF(PRVARX.NE.1.AND.PRKNT.NE.0) OSPLIN
00368          @          CALL PRNKNT(X,M,IDX,VX,IDX,PRKNT) OSPLIN
00369          IF(PRESO.EQ.1)CALL DPRINT(V,N,1,IOV,1,'OBS VECTOR RESIDUALS',10) OSPLIN
00370 C* TRANSFORM KNOT VECTORS TO CUBIC COEFFICIENTS OSPLIN
00371          CALL BUILD(KNO,X,VX,COF,VCOF,DTK, OSPLIN
00372          @          CX,VCX,CO,VCO,PRCOFV,PRCOFF) OSPLIN
00373 C* PLOTTING OF KNOTS,POINTS AND SPLINE OSPLIN
00374 C* CONFIDENCE ELLIPSE SET AT THE ALPHA PERCENTAGE LEVEL OSPLIN
00375 7000 IF(IELIPS.EQ.1)WRITE(IWR,7540)ALPHA,ESC OSPLIN
00376          IF(IELIPS.EQ.0)WRITE(IWR,7570) OSPLIN
00377          IF(SPLIN.EQ.0)GO TO 8020 OSPLIN
00378          DO 7010 I = 1,SPLIN OSPLIN
00379          @          CALL DESIGN(NC,KNC,ICOUNT, ITYPE,SPLIN,PRGEN,PRPTS,PRKNOT, OSPLIN
00380          @          @          DRAW,IER,ESC,SCTIME, OSPLIN
00381          @          @          XSTART,XINT,FOFIV,NINTY, OSPLIN
00382          @          @          TK,TX,COF,VCOF,DTK,VAR,LOBS) OSPLIN
00383          IF(SPLIN.GT.1.AND.I.NE.SPLIN)READ(IRD,*)PRPTS,PRKNOT,DRAW,PRGEN OSPLIN
00384          IF(SPLIN.GT.1.AND.I.NE.SPLIN.AND.DRAW.NE.0)READ(5,*)XSTART,XINT OSPLIN

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00433      END
00434      SUBROUTINE ANALYS(IANLYS,ESC,ICANYS,KNO,NO,SCTIME,XSTART,XINT,      DSPLIN
00435      @      GSTART,GINT,SO,DEGOF,LOBS,      DSPLIN
00436      @      VAR,TX,TK,COF,VCOF,V,IC,IPLLOT,IER,TIM,DIST,XX,YY,SDIST)      DSPLIN
00437      IMPLICIT REAL*8(A-H,O-Y),REAL*4(Z)      DSPLIN
00438 C *****      DSPLIN
00439 C * VERSION      : 23 SEPTEMBER 1982      DSPLIN
00440 C * DESCRIPTION : ANALYSIS AND DISPLAY OF RESIDUALS      DSPLIN
00441 C *****      DSPLIN
00442 C INPUT PARAMETERS      DSPLIN
00443 C 10 OPTIONS CCNTAINED IN ICANYS CONTROL THE PERFORMANCE      DSPLIN
00444 C OF THIS SUBROUTINE.      DSPLIN
00445 C ICANYS(10) :      DSPLIN
00446 C   A) ICANYS(1) - BREAKDQWN OF RESIDUALS - ESSENTIAL FOR ICANYS(2)      DSPLIN
00447 C                      AND ICANLYS(5)      DSPLIN
00448 C   B) ICANYS(2) - PLOTTING OF RESIDUALS      DSPLIN
00449 C                      0 - NC PLOT DESIRED      DSPLIN
00450 C                      1 - RESIDUALS ONLY      DSPLIN
00451 C                      2 - INCLUDED SMOOTHED STANDARD DEVIATIONS      DSPLIN
00452 C                      3 - INCLUDED ALSO RAW STANDARD DEVIATIONS      DSPLIN
00453 C   C) ICANYS(3) - COMPUTE AND PRINT SMOOTH DATA POINTS      DSPLIN
00454 C   D) ICANYS(4) - COMPUTE AND PRINT SMOOTH VELOCITIES AT DATA TIMES      DSPLIN
00455 C   E) ICANYS(5) - PLOT OF RESIDUALS VS TIME DESIRED.      DSPLIN
00456 C                      1 - ABSOLUTE DISTANCE      DSPLIN
00457 C                      2 - EASTING      DSPLIN
00458 C                      3 - NORTHING      DSPLIN
00459 C                      4 - SIGNED DISTANCE      DSPLIN
00460 C                      5 - APP. STD RESIDUALS IN EASTINGS      DSPLIN
00461 C                      6 - APP. STD RESIDUALS IN NORTHINGS      DSPLIN
00462 C   F) ICANYS(6) - ACTIVATE SIMULATED DATA COMPARISON      DSPLIN
00463 C   G) ICANYS(7) - PRINT PLOTTING VALUES OF OPTION (E)      DSPLIN
00464 C   H) ICANYS(8) - LOREX PRINT FORMAT      DSPLIN
00465 C   I) ICANYS(9) - PLOT VS TIME      DSPLIN
00466 C                      1 - COURSE      DSPLIN
00467 C                      2 - SPEED      DSPLIN
00468 C   J) ICANYS(10) - NOT USED      DSPLIN
00469 C
00470 C IF ICANYS(8) = 1 THEN INPUT      DSPLIN
00471 C K) GSTART - TIME TO BEGIN SMOOTHED VALUES      DSPLIN
00472 C L) GINT - INCREMENT BETWEEN SMOOTHED PARAMETERS      DSPLIN
00473 C FOR FIRST CALL TO ANALYS SUBROUTINE      DSPLIN
00474 C INPUT OF VARIABLES XSTART AND XINT IS VIA THE OPTION SUBR      DSPLIN
00475 C FOR THE SECOND AND SUBSEQ CALLS TO ANALYS SUBROUTINE,I.E. IANLYS >1      DSPLIN
00476 C IF ICANYS(9) = 1 OR = 2 INPUT:      DSPLIN
00477 C M) XSTART - TIME TO START SPEED/COURSE PLOT      DSPLIN
00478 C N) XINT - PLOTTING INCREMENTS      DSPLIN
00479 C IC - CURRENTLY PROCESSING DATA SET NUMBERED 'IC'      DSPLIN
00480 C IANLYS - NO OF TIMES THE ROUTINE IS TO CALL IN THIS DATA SET      DSPLIN

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00481 C ESC,KNO,NO,SCTIME,S0,DEGOF,LOBS,VAR,TX,TK,COF, OSPL IN
00482 C VCOF,V,IPL0T,IER OSPL IN
00483 C - SEE MAIN FOR DESCRIPTION OSPL IN
00484 C OSPL IN
00485 C OUTPUT PARAMETERS OSPL IN
00486 C PROGRAM NOT DESIGN TO RETURN ANY PARAMETERS OSPL IN
00487 C OSPL IN
00488 C WORK ARRAYS OSPL IN
00489 C TIM,DIST,XX,YY,SDIST OSPL IN
00490 C OSPL IN
00491 C CALLS - PRNTCH,NOWPLT,DSHLNS,ENDPLT ( PLOTTING LIB ROUTINES ) OSPL IN
00492 C PLOT,PCOPY,POINT,SCMULT,SMOOTH,VSMOTH,SIMULA,ELIPSE, OSPL IN
00493 C SIGDIS,CTIME OSPL IN
00494 C - OSORT OSPL IN
00495 C* OSPL IN
00496 C COMMON /DIM1/ICBSNO,IDA1,IDW1,IDTX,IDP,IDPV,IOLCBS,IDVAR,ICV OSPL IN
00497 C COMMON /DIM2/IDKNOT,IDA2,IDTK,IDDTK,IDX,IDVX,IDW2,IDV2,IDXQ, OSPL IN
00498 C @ IDCOF,IDVCOF OSPL IN
00499 C REAL*8 LOBS(ILOBS,1),VAR(IDVAR,2,2),TX(IDTX,1),TK(IDTK,1), OSPL IN
00500 C @ CUF(IDCOF,8),VCOF(IOVCOF,8,8),V(IDV,1) OSPL IN
00501 C* OSPL IN
00502 C* DIMENSIONS OF LOCAL MATRICES - IDCOM = ICBSNO OSPL IN
00503 C* - DIM TKO = IDKNOT OSPL IN
00504 C REAL*8 XX(500,1),YY(500,1),DIST(500,1),TIM(500,1),TKO(32,1) OSPL IN
00505 C REAL*8 SDIST(500,1) OSPL IN
00506 C REAL*4 ZDASH(2) OSPL IN
00507 C INTEGER ICANYS(10),DEGOF OSPL IN
00508 C* OSPL IN
00509 C IDCOM = IOBSNO OSPL IN
00510 C IDTKO = IDKNOT OSPL IN
00511 C SC = 1.0000/SCTIME OSPL IN
00512 C* IGNORE ROUTINE IF SUBR LS FAILED OSPL IN
00513 C IF((IANLYS.EQ.1.AND.IPLOT.EQ.1)CALL PLOT(ZA,ZB,ZC,ZG,ZS,ZD,ZF,ZE) OSPL IN
00514 C IF(IER.NE.0)RETURN OSPL IN
00515 C IF((IANLYS.GT.1).AND.( (ICANYS(2).NE.0) OSPL IN
00516 C @.OR.(ICANYS(9).NE.0) ) )CALL PLOT(ZA,ZB,ZC,ZG,ZS,ZD,ZF,ZE) OSPL IN
00517 C IF(ICANYS(1).NE.1)GO TO 50 OSPL IN
00518 C* TRANSFER AND COMPUTATION OF THE TIME , RMS AND DISTANCES OSPL IN
00519 C IL = 2*NO + 4 OSPL IN
00520 C J = 0 OSPL IN
00521 C RMS = 0.0000 OSPL IN
00522 C DO 10 I = 5,IL,2 OSPL IN
00523 C J = J + 1 OSPL IN
00524 C I2 = I + 1 OSPL IN
00525 C XX(J,1) = V(I,1) OSPL IN
00526 C YY(J,1) = V(I2,1) OSPL IN
00527 C X2 = XX(J,1)*XX(J,1) OSPL IN
00528 C Y2 = YY(J,1)*YY(J,1) OSPL IN

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00673          DR = RADD(DIR)
00674          CALL VELO(TFIX,SPEED,DIR,VE,VN,SVE,SVN,CVEN,ICO,KNO,TK,COF,VCOF)
00675          SDR = RADD(DIR)
00676          VX = SVE*SVE
00677          VY = SVN*SVN
00678          CALL ELIPSE(VX,VY,CVEN,VA,VB,ESC,DIR)
00679          VDR = RADD(DIR)
00680          TRU = TFIX/SCTIME
00681          CALL CTIME(TRU,IDAY,IHR,IMIN)
00682 C* CCNVERT TO INTEGERS
00683          IX = X
00684          IY = Y
00685          IA = A
00686          IB = B
00687          IDR = DR
00688          IVE = VE
00689          IVN = VN
00690          ISDR = SDR
00691          ISPD = SPEED
00692          IVA = VA
00693          IVB = VB
00694          IVDR = VDR
00695 C*
00696 C* WRITE HEADING
00697          IF (IST.NE.IK)GO TO 405
00698          IK = IK + 45
00699          WRITE(6,9130)
00700          405 WRITE(6,9140)IDAY,IHR,IX,IY,IA,IB,IDR,
00701             @ IVE,IVN,ISPD,ISDR,IVA,IVB,IVDR
00702          410 CONTINUE
00703 C*
00704          500 IF(ICANYS(9).NE.1.AND.ICANYS(9).NE.2)GO TO 999
00705 C*
00706 C* DRAW COURSE VS TIME OR SPEED VS TIME CHARTS
00707          CALL PRNTCH(' ')
00708          YSTART = XSTART*SCTIME
00709          YINT = XINT*SCTIME
00710          INO = ((TK(KNO,1)-YSTART)/YINT) + 1
00711          IK = 0
00712          DO 510 I = 1,INO
00713          TFIX = YSTART + (I-1)*YINT
00714          CALL VELO(TFIX,SPEED,DIR,VE,VN,SVE,SVN,CVEN,ICC,KNO,TK,COF,VCOF)
00715          IF(ICO.EQ.0)GO TO 510
00716          IK = IK + 1
00717          SDR = RADD(DIR)
00718          ZX = TFIX/SCTIME
00719          ZY = SPEED
00720          IF(ICANYS(9).EQ.1)ZY = SDR

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00865      20 VCOF(J,IK,IJ) = VCC(IK,IJ)
00866        IF(PRCOFV.EQ.0)GO TO 10
00867        CALL DPRINT(CO,8,1,8,1,'COEFFICIENTS',6)
00868        CALL DPRINT(VCO,8,8,8,8,'COVARIANCE',5)
00869      10 CONTINUE
00870 C* OUTPUT OF COEFFICIENTS
00871        IF(PRCOFF.EQ.0)RETURN
00872        IF(PRCOFF.EQ.1.AND.PRCOFV.EQ.1)RETURN
00873        CALL DPRINT(COF,J,8,IDCOF,8,'COEFFICIENTS PER INTERVAL',13)
00874        RETURN
00875        END
00876        SUBROUTINE CHECK(KNO,NO,TX,TK,ICODE)
00877        IMPLICIT REAL*8(A-H,O-Z)
00878 C *****
00879 C * VERSION      : 22ND MARCH 1982
00880 C * DESCRIPTION : CHECKING AND OPTIONAL DROPPING OF KNOTS
00881 C *****
00882 C INPUT PARAMETERS
00883 C   KNO  - NUMBER OF KNOTS
00884 C   NO   - NUMBER OF POINTS
00885 C   TX   - ARRAY CONTAINING DATA POINT TIMES
00886 C   TK   - ARRAY CONTAINING KNOT TIMES
00887 C   ICODE - 0 TKNOT VS DATA POINT SEQUENCE IS NOT CHECKED
00888 C           1 CHECKING AND DROP SCHEME KNOT ACTIVATED
00889 C
00890 C OUTPUT PARAMETERS
00891 C   TK   - MODIFIED AS INSTRUCTED BY CCOES
00892 C
00893 C CALLS   - INTERV
00894 C ADDITIONAL NOTES
00895 C   CRTERA DENOTES THE PRESET MINIMUM NUMBER OF DATA POINTS ALLCWD
00896 C   PER INTERVAL BEFORE THE 'DROP KNOT SCHEME' IS IMPLEMENTED.
00897 C
00898 C   KNOTS ARE DROPPED IN SUCH A MANNER AS TO INCREASE THE
00899 C   MORE DEFICIENT ADJACENT INTERVAL.
00900 C   EG. DATA PLACEMENT  6 2 1 4 5   UNDER CRTERA = 2
00901 C   BECOMES              6 3 4 5
00902 C WHEREAS
00903 C   DATA PLACEMENT  6 4 1 2 5   UNDER CRTERA = 2
00904 C   BECOMES          6 4 3 5
00905 C *****
00906 C COMMON /DIM1/IQBSNO,IDA1,IDW1,IDX,IDX,IDX,IDX,IDX,IDX,IDX,ICV
00907 C COMMON /DIM2/IDKNOT,IDA2,IDTK,IDDTK,IDX,IDX,IDX,IDX,IDX,IDX,
00908 C           IDCGF,IOVCOF
00909 C REAL*8 TX(IDTX,1),TK(IDTK,1)
00910 C INTEGER*4 NO,KNO,NUM(40),NOK,ITOTAL,IB4,IAF,IDROP,CRTERA
00911 C DATA CRTERA/1/
00912 C*BEGINS

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01297 C SCTIME - SCALE FACTOR ON TIME DOMAIN DSPLIN
01298 C XSTART,XINT- TIME TO BEGIN DRAWING SPLINE AT XINT INCREMENTS DSPLIN
01299 C TK,TX,COF,VCOF,DTK,VAR,LCBS DSPLIN
01300 C - DATA ARRAYS AS DESCRIBED IN THE MAIN DSPLIN
01301 C FORFIV,NINTY - 45 DEG AND 90 DEG IN RADIANS DSPLIN
01302 C DSPLIN
01303 C CALLS - PRNTCH,NMBR,ELLIPS,SPSYMD,NOWPLT,CIRCLE,DSHLNS, DSPLIN
01304 C ENDPLT ( FORTPLOT LIBRARY ROUTINES ) DSPLIN
01305 C - PLOT,ELIPSE,POINT,RADD DSPLIN
01306 C - DSORT DSPLIN
01307 C ADDITIONAL NOTES DSPLIN
01308 C THE INPUT OF THE DATA POINTS ARE STORED IN THE LCBS DSPLIN
01309 C MATRIX BET AND INCLUDING THE 5ND ELEMENT AND (2*NO+4) DSPLIN
01310 C ELEMENT . ARRAYS SIZES ARE TRANSFER THROUGH COMMON BLOCKS DSPLIN
01311 C ***** DSPLIN
01312 C COMMON /DIM1/IOBSNO,IDA1,IDW1,IDTX,IDP,IDPV,IOLORS,IDVAR,IDV DSPLIN
01313 C COMMON /DIM2/IDKNOT,IDA2,IDTK,IDDTK,IDX,IOVX,IDW2,IOV2,IOXO, DSPLIN
01314 C @ IDCOF,IOVCOF DSPLIN
01315 C* ARRAYS DSPLIN
01316 C REAL*8 TK(IDTK,1),TX(IDTX,1),COF(IDCOF,8),VCOF(IOVCOF,8,8), DSPLIN
01317 C @ DTK(IDDTK,1),VAR(IOVAR,2,2),LOBS(IOLCBS,1), DSPLIN
01318 C @ NINTY DSPLIN
01319 C REAL*4 ZDASHG(2) DSPLIN
01320 C INTEGER SPLIN,PRGEN,PRPTS,PRKNGT,DRAW DSPLIN
01321 C* APPLY SCALE FACTOR ON PLOTTED ELLIPSES DSPLIN
01322 C DATA SCALEL/1.000/ DSPLIN
01323 C* DSPLIN
01324 C* PROGRAM BEGINS DSPLIN
01325 C* SET UP PLOT AREA FOR CNCE ONLY DSPLIN
01326 C IF(:CCUNT.EQ.1.AND.SPLIN.EQ.1) DSPLIN
01327 C @ CALL PLOT(ZIHF,ZIHC,ZIDPX,ZIDPY,ZX1,ZY1,ZX2,ZY2) DSPLIN
01328 C IF(SPLIN.NE.1) DSPLIN
01329 C @ CALL PLOT(ZIHF,ZIHC,ZIDPX,ZIDPY,ZX1,ZY1,ZX2,ZY2) DSPLIN
01330 C IF(PRPTS.EQ.0)GO TO 100 DSPLIN
01331 C CALL PRNTCH('X') DSPLIN
01332 C L = NC + 1 DSPLIN
01333 C J = 3 DSPLIN
01334 C INUMP = 1 DSPLIN
01335 C DO 10 I = 2,L DSPLIN
01336 C INUM = I-1 DSPLIN
01337 C J = J + 2 DSPLIN
01338 C J1 = J + 1 DSPLIN
01339 C* SELECT OPTION DSPLIN
01340 C ZX = LOBS(J,1) DSPLIN
01341 C ZY = LOBS(J1,1) DSPLIN
01342 C IF(PRPTS.EQ.2)ZY = ZX DSPLIN
01343 C IF(PRPTS.EQ.2.OR.PRPTS.EQ.3)ZX = TX(I,1)/SCTIME DSPLIN
01344 C* PRINT NUMBER DSPLIN

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01393 C* CORRECTION APPLIED TO THE TIME INTERVAL AND INPUT TIME DSPL IN
01394 YINT = XINT*SCTIME DSPL IN
01395 YSTART = XSTART*SCTIME DSPL IN
01396 C* POSITIONS THE PEN AT THE FIRST KNOT DSPL IN
01397 ZAX = COF(1,1) DSPL IN
01398 ZAY = COF(1,2) DSPL IN
01399 IF(DRAW.EQ.2)ZAY = ZAX DSPL IN
01400 IF(DRAW.EQ.2.OR.DRAW.EQ.3)ZAX = YSTART/SCTIME DSPL IN
01401 CALL NOWPLT(0,ZAX,ZAY) DSPL IN
01402 CALL PRNTCH(' ') DSPL IN
01403 INO = (TK(KNO,1)-YSTART)/YINT + 1 DSPL IN
01404 WRITE(6,9000) DSPL IN
01405 C* BEGIN DRAWING DSPL IN
01406 DO 210 I = 1,INO DSPL IN
01407 TFIX = YSTART + (I-1)*YINT DSPL IN
01408 CALL POINT(TFIX,XN,YN,VXN,VYN,VXY,ICODE,KNO,TK,COF,VCOF) DSPL IN
01409 IF(ICODE.EQ.0)GO TO 210 DSPL IN
01410 SE = DSORT(VXN) DSPL IN
01411 SN = DSORT(VYN) DSPL IN
01412 C* ESC IS SET TO PRODUCE THE ALPHA PERCENT ELLIPSE DSPL IN
01413 CALL ELLIPSE(VXN,VYN,VXY,A,B,ESC,DIR) DSPL IN
01414 ZDR = NINTY - DIR DSPL IN
01415 ZA = A DSPL IN
01416 ZB = B DSPL IN
01417 ZAX = XN DSPL IN
01418 ZAY = YN DSPL IN
01419 IF(DRAW.EQ.2)ZAY = ZAX DSPL IN
01420 IF(DRAW.EQ.2.GR.DRAW.EQ.3)ZAX = TFIX/SCTIME DSPL IN
01421 ZDASHG(1) = ICQUNT*0.05 DSPL IN
01422 ZCASHG(2) = 0.1 DSPL IN
01423 C* CONFINE PLOTTING TO WITHIN GRID AREA DSPL IN
01424 IF(ZAX.GT.ZX2.OR.ZAX.LT.ZX1)GO TO 220 DSPL IN
01425 IF(ZAY.GT.ZY2.OR.ZAY.LT.ZY1)GO TO 220 DSPL IN
01426 C* CHIOCES DSPL IN
01427 IF(ITYPE.EQ.1)GO TO 230 DSPL IN
01428 IF(DRAW.EQ.1)CALL DSHLNS(ZAX,ZAY,ZDASHG,-2) DSPL IN
01429 IF(DRAW.EQ.4)CALL ELLIPS(ZAX,ZAY,-ZA,-ZB,ZDR) DSPL IN
01430 IF(DRAW.EQ.4)CALL SPSYMB(ZAX,ZAY,-4,ZCR,ZIMF) DSPL IN
01431 IF(DRAW.EQ.2.OR.DRAW.EQ.3)CALL NOWPLT(1,ZAX,ZAY) DSPL IN
01432 230 IF(ITYPE.EQ.1)CALL NOWPLT(1,ZAX,ZAY) DSPL IN
01433 220 TFIX = TFIX/SCTIME DSPL IN
01434 DR = RADD(DIR) DSPL IN
01435 IF(PRGEN.EQ.1)WRITE(6,9010)1,TFIX,XN,YN,SE,SN,VXY,A,B,DR DSPL IN
01436 210 CONTINUE DSPL IN
01437 999 IF(SPLIN.NE.1)CALL ENDPLT DSPL IN
01438 RETURN DSPL IN
01439 9000 FORMAT(//,10X,'PREDICTED FIXES AT SPECIFIED TIMES',/10X, DSPL IN
01440 .17('=='),//,3X,'NO',6X,'TIME',12X, DSPL IN

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01489 C OUTPUT PARAMTERS
01490 C SE - STANDARD DEVIATION IN THE EASTINGS DSPL IN
01491 C SN - STANDARD DEVIATIONS IN THE NORTHINGS DSPL IN
01492 C SEN - COVARIANCE BETWEEN EASTINGS AND NORTHINGS DSPL IN
01493 C DSPL IN
01494 C CALLS - DSORT,DTAN DSPL IN
01495 C DSPL IN
01496 C ***** DSPL IN
01496 REAL*8 A,B,DIR,SE,SN,SEN,DR,K,C,GAMMA,PHI DSPL IN
01497 DATA PHI/3.141592654000/ DSPL IN
01498 DR = DIR DSPL IN
01499 IF(ICODE.EQ.0)DR = (DIR/180.000)*PHI DSPL IN
01500 GAMMA = 2.000*(PHI/2.000 - DR) DSPL IN
01501 K = PHI*2.000 DSPL IN
01502 IF(GAMMA.GT.K)GAMMA = GAMMA - K DSPL IN
01503 SEN = 0.500*(A*A - B*B)*DSIN(GAMMA) DSPL IN
01504 K = A*A + B*B DSPL IN
01505 C = 2.000*SEN/DTAN(GAMMA) DSPL IN
01506 SE = DSQRT((K+C)/2.000) DSPL IN
01507 SN = DSQRT((K-C)/2.000) DSPL IN
01508 RETURN DSPL IN
01509 END DSPL IN
01510 REAL FUNCTION ELSFAC*8(ALPHA) DSPL IN
01511 REAL*8 ALPHA DSPL IN
01512 C ***** DSPL IN
01513 C * VERSION : JUNE 1982 * DSPL IN
01514 C * DESCRIPTION : TO COMPUTE THE SCALE FACTOR FOR THE CONFIDENCE * DSPL IN
01515 C * ELLIPSES AT THE ALPHA PERCENTAGE LEVEL. * DSPL IN
01516 C * IF ERROR DETECTED, SCALE FACTOR IS SET TO 1.000 * DSPL IN
01517 C ***** DSPL IN
01518 C CALLS - MDCHI (IMSL ROUTINE) DSPL IN
01519 C - DSQRT,DBLE DSPL IN
01520 C DSPL IN
01521 ZX = ALPHA/100.000 DSPL IN
01522 CALL MDCHI(ZX,2.0,Y,IER) DSPL IN
01523 IF(IER.EQ.0)ELSFAC = DSQRT(DBLE(Y)) DSPL IN
01524 IF(IER.NE.0)ELSFAC = 1.000 DSPL IN
01525 C* DSPL IN
01526 RETURN DSPL IN
01527 END DSPL IN
01528 SUBROUTINE ERRATR(XVELO,AVELO,ELEV,XTER) DSPL IN
01529 IMPLICIT REAL*8(A-H,O-Z) DSPL IN
01530 C ***** DSPL IN
01531 C * VERSION : AUGUST 1982 * DSPL IN
01532 C * DESCRIPTION : COMPUTES THE ALONG TRACK ERROR * DSPL IN
01533 C * DUE AN ERROR IN RECEIVER MOTION * DSPL IN
01534 C * BASED ON THE MAGNITUDE OF THE * DSPL IN
01535 C * MOTION AND THE ELEVATION OF THE * DSPL IN
01536 C * SATELLITE. * DSPL IN

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01537 C *****
01538 C INPUT PARAMETERS OSPLIN
01539 C AVELO - ERROR IN VELOCITY OF THE RECEIVER ALONG-TRACK DIRECTION OSPLIN
01540 C XVELO - ERROR IN VELOCITY OF THE RECEIVER CROSS-TRACK DIRECTION OSPLIN
01541 C ELEV - ELEVATION OF THE TRACKED SATELLITE OSPLIN
01542 C OSPLIN
01543 C OUTPUT PARAMETERS OSPLIN
01544 C XTER - COMPUTED RSS ALONG TRACK ERROR OSPLIN
01545 C OSPLIN
01546 C CALLS - DSQRT OSPLIN
01547 C OSPLIN
01548 ELEVAT = (ELEV/3.141592654)*180.000 OSPLIN
01549 C ERROR DUE TO VELOCITY NORTH ERRORS OSPLIN
01550 XTER1 = 0.0300*AVELG OSPLIN
01551 IF(ELEVAT.GT.75 )XTER1 = 0.0400*AVELO OSPLIN
01552 IF(ELEVAT.GT.80 )XTER1 = 0.07500*AVELO OSPLIN
01553 IF(ELEVAT.GT.83 )XTER1 = 0.0900*AVELO OSPLIN
01554 IF(ELEVAT.GT.85 )XTER1 = 0.1000*AVELO OSPLIN
01555 IF(ELEVAT.GT.87 )XTER1 = 0.1300*AVELO OSPLIN
01556 C ERROR DUE TO VELOCITY EAST ERRORS OSPLIN
01557 XTER2 = 0.0200*XVELO OSPLIN
01558 IF(ELEVAT.GE.75)XTER2 = 0.0200*XVELO OSPLIN
01559 IF(ELEVAT.GE.80)XTER2 = 0.01500*XVELO OSPLIN
01560 IF(ELEVAT.GE.85)XTER2 = 0.0100*XVELO OSPLIN
01561 C ERROR DUE TO INCORRECT ALTITUDE OSPLIN
01562 XTER3 = 12*0.25 OSPLIN
01563 IF(ELEVAT.GE.75)XTER3 = 12*0.35 OSPLIN
01564 IF(ELEVAT.GE.80)XTER3 = 12*0.50 OSPLIN
01565 IF(ELEVAT.GE.85)XTER3 = 12*0.75 OSPLIN
01566 IF(ELEVAT.GE.87)XTER3 = 12*1.00 OSPLIN
01567 C CUMMULATIVE ERROR OSPLIN
01568 XTER = DSQRT(XTER1*XTER1 + XTER2*XTER2 + XTER3*XTER3) OSPLIN
01569 RETURN OSPLIN
01570 END OSPLIN
01571 SUBROUTINE ERRORS(E0,N0,SE,SN,SEN,VELQ,DIR,ICODE) OSPLIN
01572 IMPLICIT REAL*8(A-H,C-Z) OSPLIN
01573 C ***** OSPLIN
01574 C * VERSION : 05 JULY 1982 OSPLIN
01575 C * DESCRIPTION : IF THE UNMODELLED ERRORS DUE TO VELOCITY AND OSPLIN
01576 C * ALTITUDE ERRORS EXCEED THAT OF THE FORMAL ERROR OSPLIN
01577 C * ESTIMATES, THE STD DEVIATIONS ARE ADJUSTED ACCORDING.* OSPLIN
01578 C ***** OSPLIN
01579 C INPUT PARAMETERS OSPLIN
01580 C E0,N0 - POSITION AS DETERMINED BY THE METHOD OF LEAST SQUARES OSPLIN
01581 C SE,SN - STANDARD DEVIATIONS IN EASTING AND NORTHING RESP. OSPLIN
01582 C SEN - COVARIANCE OSPLIN
01583 C VELO - ESTIMATED VELOCITY OF THE RECEIVER OSPLIN
01584 C DIR - AZIMUTH(IN RADIANS) OF THE MOTION OF RECEIVER OSPLIN

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01585 C
01586 C OUTPUT PARAMETERS DSPLIN
01587 C EO,NO, DSPLIN
01588 C VELO,DIR - UNCHANGED DSPLIN
01589 C SE,SN, DSPLIN
01590 C SEN - MODIFIED BY A FACTOR DETERMINED BY THE ROUTINE. DSPLIN
01591 C DSPLIN
01592 C CALLS - ELIPSE,SATELV,ERRXTR,ERRATR,ELLSIG DSPLIN
01593 C - DCOS,DSIN DSPLIN
01594 C ***** DSPLIN
01595 REAL*8 EO,NO,NINTY,FULC DSPLIN
01596 DATA PHI/3.14159265400/,NINTY/1.57079632700/,FULC/6.28318530800/ DSPLIN
01597 VX = SE*SE DSPLIN
01598 VY = SN*SN DSPLIN
01599 CALL ELIPSE(VX,VY,SEN,A,B,1.000,DRELL) DSPLIN
01600 C* COMPUTE ANGLE BETWEEN SATELLITE DIRECTION AND MOTION DSPLIN
01601 DRS = DRELL + NINTY DSPLIN
01602 IF(DRS.GT.FULC)DRS = DRS - FULC DSPLIN
01603 DR = DRS DSPLIN
01604 IF(DRS.LT.DIR)DR = DRS + FULC DSPLIN
01605 ADR = DR - DIR DSPLIN
01606 IF(ADR.GE.PHI)ADR = ADR - PHI DSPLIN
01607 IF(ADR.GT.NINTY)ADR = PHI - ADR DSPLIN
01608 C* VELOCITY COMPONENT OF RECEIVER IN THE CROSS TRACK AND ALONG TRACK DSPLIN
01609 C* DIRECTION OF THE SATELLITE DSPLIN
01610 AVELO = VELO*DCOS(ADR) DSPLIN
01611 XVELO = VELO*DSIN(ADR) DSPLIN
01612 CALL SATELV(EO,NO,2.006,2.006,DRS,ELEV) DSPLIN
01613 CALL ERRXTR(XVELO,AVELO,ELEV,AB) DSPLIN
01614 CALL ERRATR(XVELO,AVELO,ELEV,BA) DSPLIN
01615 DR = RADD(DRS) DSPLIN
01616 ELEV = RADD(ELEV) DSPLIN
01617 IF(ICODE.EQ.1)WRITE(6,9000)DR,ELEV,A,B,AB,BA DSPLIN
01618 IF((AB.LT.A.AND.BA.LT.B).AND.ICODE.EQ.1)WRITE(6,9010) DSPLIN
01619 IF(AB.LT.A.AND.BA.LT.B)RETURN DSPLIN
01620 C* ERROR ELLIPSES MODIFIED ACCORDING TO RSS ERRORS DSPLIN
01621 IF(AB.GT.A)A = AB DSPLIN
01622 IF(BA.GT.B)B = BA DSPLIN
01623 CALL ELLSIG(A,B,DRELL,SE,SN,SEN,1) DSPLIN
01624 IF(ICODE.EQ.1)WRITE(6,9020)SN,SE,SEN,A,B DSPLIN
01625 RETURN DSPLIN
01626 9000 FORMAT(/,3X,'AZIMUTH OF SATELLITE AT TCA ',F6.1,' DEGS',/, DSPLIN
01627 @ 3X,'ELEVATION OF SATELLITE ',F6.1,' DEGS',/, DSPLIN
01628 @ 3X,'INPUT ERROR ELLIPSE;A AND B ',D12.5,2X,D12.5,' M', DSPLIN
01629 @ /,3X,'RSS TRACK ERROR; XTR & ALTR ',D12.5,2X,D12.5,' M') DSPLIN
01630 9010 FORMAT(3X,'RSS ERRORS WITHIN ERROR ELLIPSE',/) DSPLIN
01631 9020 FORMAT(3X,'RSS ERRORS EXCEEDS ERROR ELLIPSE', DSPLIN
01632 @ /,3X,'NEW STD DEV(N,E) AND CCV ',3(F10.1,3X), DSPLIN

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01825          TED = TBG + DINT
01826          GO TO 1000
01827          2000 WRITE(6,9100)
01828          9100 FORMAT(3X,'FILTER TESTS COMPLETED',/)
01829          700  FORMAT(/,/,3X,'SUB FILTER DETECT THESE POINTS AS OUTLIERS',
01830          @ /,3X,'TIME SPAN ',1PD12.5,' INCREMENT WIDTH ',1PD12.5,/,/)
01831          710  FORMAT(/,3X,'POINT SPAN < ',13,' ',13,'>',/)
01832          720  FORMAT(3X,'NO',14,' TIME ',1PD12.5,' E RESIDUAL FAILED',
01833          @ ' (SEVERITY : ',12,' )')
01834          730  FORMAT(3X,'NO',14,' TIME ',1PD12.5,' N RESIDUAL FAILED',
01835          @ ' (SEVERITY : ',12,' )')
01836          740  FORMAT(/,3X,'POINT SPAN < ',13,' ',13,'> ERROR CODE ;',12,/)
01837          750  FORMAT(/,3X,'SCALE FACTOR FOR ',F6.1,' PERCENT CONFIDENCE',
01838          @ ' ELLIPSES = ',F10.4,/)
01839          RETURN
01840          END
01841          SUBROUTINE FIT(TIME,XX,YY,VXY,IOPT,ICODE,IRJET,ALPKNT,
01842          @          A,P,VAR,VX,VXOLD,LOBS,WKS)
01843          IMPLICIT REAL*8(A-H,O-Z)
01844          C *****
01845          C * DESCRIPTION OF ROUTINE
01846          C * VERSION      : 12 JULY 1982
01847          C * DEPLOYMENT  : CURVE FITTING
01848          C * QUALITIES   : HAS THE POSITION AND 1ST DERIVATIVE OF THE
01849          C *                  FORMER KNOT WEIGHTED : VARIABLE WEIGHTING ON SLOPE
01850          C *                  AND POSITION OF KNOT IS USED
01851          C * METHOD      : SEE THE OPTION SET FOR ANALYSIS OF PROGRAM
01852          C *                  CAPABILITIES
01853          C *****
01854          C INPUT PARAMETERS
01855          C TIME - TIME OF DATA POINT
01856          C XX,YY - COORDINATES OF DATA POINT
01857          C VXY - COVARIANCE MATRIX OF DATA POINTS
01858          C
01859          C IOPT - VECTOR OF OPTIONS GOVERNING THE CURVE FITTING
01860          C* A) IOPT(1) : MIN NUMBER OF DATA POINTS BEFORE DOING THE FIRST
01861          C CUBIC POLYNOMIAL FIT
01862          C* B) IOPT(2) : LOCATION OF KNOT = 1 MIDWAY BET TWO DATA POINTS
01863          C = 0 CONCIDENCE WITH THE DATA POINT
01864          C* C) IOPT(3) : % OF INTERVAL OVERHANGING .IE. X OF PTS
01865          C OUTSIDE THE INTERVAL WITH THE INTERVAL AS 100 X
01866          C* D) IOPT(4) : MAGNIFICATION FACTOR ON THE SLOPE VARIANCE
01867          C IF <1 THEN NO WEIGHT ; 100 ACTUAL COMPUTED VARIANCE
01868          C >100 INCREASE IN WEIGHT ; 1<A) 4)<100 X WT.
01869          C* E) IOPT(5) : MIN NUMBER OF DATA POINTS PER INTERVAL PERMITTED
01870          C
01871          C* F) IOPT(6) : INCLUSION OF FORWARD OUTER POINTS IN REJECTION TESTS
01872          C IF 1 - YES ; 0 - NO

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01873 C* G) IOPT(7) : MINIMUM LAG OF ONE POINT TO BE ENFORCED DSPLIN
01874 C          1 - YES OR 0 - NO OSPLIN
01875 C* H) IOPT(8) : ALL DIAGONSTIC PRINTOUT : 1 - YES ; 0 - NO OSPLIN
01976 C OSPLIN
01877 C* I) IOPT(9) : PRINT COMPUTED KNOTS : 1 - YES ; 0 - NO OSPLIN
01878 C OSPLIN
01879 C* J) IOPT(10) : PRINT COMPUTED KNCTS COVAR MATRIX : 1 - YES ; 0 - NO OSPLIN
01880 C OSPLIN
01881 C* K) IRJET - NO OF FAILURES ALLOWED OSPLIN
01882 C* L) ALPKNT - X LEVEL OF SIGNIFICANCE TESTS OSPLIN
01883 C OSPLIN
01884 C OUTPUT PARAMETERS OSPLIN
01885 C ICODE = 0 POINT READ AND PROCESSED BUT KNOT NOT RECOMMENDED OSPLIN
01886 C          = 1 FATAL ERROR DETECTED IN THE SUBROUTINE OSPLIN
01887 C          = 2 KNOT ESTABLISHED. OSPLIN
01888 C IF AND ONLY IF ICODE = 2 OSPLIN
01889 C TIME = NEXT KNOT TIME OSPLIN
01890 C OSPLIN
01891 C WORK ARRAYS - A,P,VAR,VX,VXOLD,LOBS ( AS DIM BELOW ) OSPLIN
01892 C          - WKS (WORK ARRAY AS REQUESTED BY SOLV ROUTINE ) OSPLIN
01893 C OSPLIN
01894 C CALLS - OBS,CHOLD,REJECT OSPLIN
01895 C ADDITIONAL NOTES OSPLIN
01896 C IOPT(1) MUST BE AT LEAST (100 + IOPT(3)) PERCENT LARGER OSPLIN
01897 C THAN IOPT(5). OSPLIN
01898 C ALL POINTERS IN COMMON BELOW HAVE TO BE RESET BEFORE OSPLIN
01899 C BEGINNING TO LOCATE OPTIMUM KNCTS. OSPLIN
01900 C 7 JULY 1982 - UPGRADE TO 100 PTS PER INTERVAL OSPLIN
01901 C COMMON /INIT/TK,ISWT2,ISWT,INO,PTX,PLOBS,PVAR OSPLIN
01902 C OSPLIN
01903 C* ARRAYS FEED INTO THE PROGRAM OSPLIN
01904 C REAL*8 VXY(2,2) OSPLIN
01905 C* ARRAYS USED BY THE PROGRAM OSPLIN
01906 C* STORAGE OF ONLY INPUT DATA POINTS OSPLIN
01907 C REAL*8 TX(100,1),LOBS(200,1),VAR(100,2,2) OSPLIN
01908 C* TEMPORARY OSPLIN
01909 C REAL*8 TK(2,1),AOBS(7,1),X(8,1),VX(8,8),XOLD(8,1),VXOLD(8,8) OSPLIN
01910 C* ACCOUNTS FOR THE KNCT INFORMATION OSPLIN
01911 C REAL*8 A(102,7),P(204,3),W(204,1),V(204,1) OSPLIN
01912 C* WORK ARRAY USED BY THE SOLV ROUTINE SEE SOLV FOR DIMENSIONS OSPLIN
01913 C REAL*8 WKS(8,204) OSPLIN
01914 C INTEGER IOPT(10),PTX,PLOBS,PVAR OSPLIN
01915 C* ARRAY SIZES OSPLIN
01916 C* VARIABLE INOBS - MAXIMUM NUMBER OF OBSERVATIONS(PER INTERVAL) OSPLIN
01917 C INOBS = 100 OSPLIN
01918 C IDTX = INCBS OSPLIN
01919 C IDLOBS = INOBS*2 OSPLIN
01920 C IDVAR = INOBS OSPLIN

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02113		DO 335 J = 1,7	
02114	335	A(I,J) = 0.000	DSPL IN
02115		A(1,1) = 1.000	DSPL IN
02116		A(2,3) = 1.000	DSPL IN
02117		DO 340 I = 1,4	DSPL IN
02118		IL = I + 4	DSPL IN
02119	340	W(I,1) = -XOLD(IL,1)	DSPL IN
02120	C* NO	CORRELATION BETWEEN POSITION AND SLOPE ASSUMED	DSPL IN
02121		CALL CHOLD(VXOLD, IDVX, IDVX, IDVX, DET, IER)	DSPL IN
02122		IF(IER.NE.0)GO TO 9300	DSPL IN
02123		P(1,2) = (IOPT(4)/100.000)*VXOLD(5,5)	DSPL IN
02124		P(1,3) = (IOPT(4)/100.000)*VXOLD(5,6)	DSPL IN
02125		P(2,1) = (IOPT(4)/100.000)*VXOLD(6,5)	DSPL IN
02126		P(2,2) = (IOPT(4)/100.000)*VXOLD(6,6)	DSPL IN
02127	C* WEI	GHTED SLOPE COVARIANCE	DSPL IN
02128		P(3,2) = (IOPT(4)/100.000)*VXOLD(7,7)	DSPL IN
02129		P(3,3) = (IOPT(4)/100.000)*VXOLD(7,8)	DSPL IN
02130		P(4,1) = (IOPT(4)/100.000)*VXOLD(8,7)	DSPL IN
02131		P(4,2) = (IOPT(4)/100.000)*VXOLD(8,8)	DSPL IN
02132		IF(IOPT(9).EQ.1)WRITE(6,7040)TK(1,1)	DSPL IN
02133		IF(IOPT(8).EQ.1)CALL DPRINT(XOLD,8,1,8,1,	DSPL IN
02134	a	'OLD KNOT VALUES.KEEP',10)	DSPL IN
02135		TIME = TK(1,1)	DSPL IN
02136		ICDE = 2	DSPL IN
02137		RETURN	DSPL IN
02138	C* ERRORS		DSPL IN
02139	9000	WRITE(6,9010)IOPT	DSPL IN
02140		STOP	DSPL IN
02141	9100	WRITE(6,9110)IER	DSPL IN
02142		ICODE = 1	DSPL IN
02143		RETURN	DSPL IN
02144	9200	WRITE(6,9210)	DSPL IN
02145		RETURN	DSPL IN
02146	9300	WRITE(6,9310)	DSPL IN
02147		ICODE = 1	DSPL IN
02148		RETURN	DSPL IN
02149	7005	FORMAT(//,3X,'INPUT NEW DATA POINT',/)	DSPL IN
02150	7000	FORMAT(/,3X,'INSUFFICIENT POINTS ',I4)	DSPL IN
02151	7010	FORMAT(/,3X,'NUMBER OF POINTS',I4)	DSPL IN
02152	7020	FORMAT(/,3X,'PASSED : KNOT TIMES : ',1PD12.5,3X,1PD12.5)	DSPL IN
02153	7030	FORMAT(///,3X,'SOLUTION OF CURRENT POINT')	DSPL IN
02154	7040	FORMAT(/,3X,'NEXT KNOT TIME ',1PD15.8)	DSPL IN
02155	7050	FORMAT(//,3X,'**WARNING** NEW KNOT TIME ACCEPTED ALTHOUGH',	DSPL IN
02156	a	' REJECTED BY TESTS',//)	DSPL IN
02157	7060	FORMAT(/,3X,'COMPUTED LAG ',I4,' POINTS')	DSPL IN
02158	7070	C FORMAT(/,3X,'**WARNING ** MAXIMUM PTS PER INTERVAL REACHED.',	DSPL IN
02159	a	' NEW KNOT TIME ACCEPTED',//)	DSPL IN
02160	9010	FORMAT(//,3X,'FIT : OPTION ERROR : INPUT ',I0I4,//)	DSPL IN


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02257 C X,VX - SOLUTION VECTOR AND VARIANCES DSPLIN
02258 C IX - DECLARED DIM OF X AND VX MATRICES DSPLIN
02259 C IER - ERROR CODES - 0 : SUCCESSFUL COMPLETION OF ROUTINE DSPLIN
02260 C 1 : ERROR DETECTED DSPLIN
02261 C DSPLIN
02262 C WORK ARRAYS - NAM,VM ( AS DIM BELOW ) DSPLIN
02263 C DSPLIN
02264 C ADDITIONAL NOTES DSPLIN
02265 C MATRICES USED BY THE SUBROUTINE MUST BE MODIFIED AS FOLLOWS DSPLIN
02266 C IF A CHANGE IN THE DECLARED DIMENSIONS OF MATRICES IS IN EFFECT. DSPLIN
02267 C THE FOLLOWING IS THE MODIFICATION PROCEDURE. DSPLIN
02268 C DSPLIN
02269 C* ATPW(IX,1) A2N(IA2*2,IX) DSPLIN
02270 C* VM (IA2*2,IA2*2) Q (IA2*2,1) NAM(IX,IA2*2) DSPLIN
02271 C* DSPLIN
02272 C* ***** DSPLIN
02273 C REAL*8 A1(IA1,7),A2(IA2,11),P(IP,3),W1(IW1,1),W2(IW2,1), DSPLIN
02274 C @ X(IX,1),VX(IX,IX) DSPLIN
02275 C* USED BY PROGRAM ** WORK ARRAYS - RELIES ON OTHER MATRIX SIZES DSPLIN
02276 C REAL*8 NAM(IX,IW2),VM(IW2,IW2) DSPLIN
02277 C* LOCAL ARRAYS * CURRENT SET FOR IOBSNO = 500 : IKNOT = 32 DSPLIN
02278 C* CURRENT SETTINGS DSPLIN
02279 C REAL*8 ATPW(128,1),A2N(60,128), DSPLIN
02280 C @ Q(60,1) DSPLIN
02281 C REAL*8 QSUM,ONE DSPLIN
02282 C INTEGER*4 R,M,N,ADDA1(IA1),ADDA2(IA2) DSPLIN
02283 C EQUIVALENCE (Q(1),ATPW(1),A2N(1)) DSPLIN
02284 C* FUNCTIONS DSPLIN
02285 C IROW(I) = (I+1)/2 DSPLIN
02286 C ICOL(I) = 2 - (((I+1)/2 - (I/2)) DSPLIN
02287 C* DIMENSION SETTING VARIABLE DSPLIN
02288 C IDVM = IA2*2 DSPLIN
02289 C IOATPW = IX DSPLIN
02290 C* WRITE UNIT DSPLIN
02291 C IWR = 6 DSPLIN
02292 C ONE = 1.000 DSPLIN
02293 C* DEFAULT ERROR SET DSPLIN
02294 C IER = 0 DSPLIN
02295 C* TEST ON CONDITION NUMBER DSPLIN
02296 C XLEVEL = 1.0D10 DSPLIN
02297 C* DSPLIN
02298 C* SINCE THE NORMAL MATRIX IS SYMMETRICAL, THE ROUTINE ONLY DSPLIN
02299 C* OPERATES ON THE LOWER HALF OF THE MATRIX AND EQUATES ITS COUNTERPART DSPLIN
02300 C* DSPLIN
02301 C DO 10 I = 1,M DSPLIN
02302 C IEND = I - 10 DSPLIN
02303 C DO 10 L = 1,M DSPLIN
02304 C QSUM = 0.0D00 DSPLIN

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02472		SUBROUTINE OBS(TXPT,TKNOT,DINTK,A)	DSPLIN
02473		IMPLICIT REAL*8(A-M,M-Z)	DSPLIN
02474	C	*****	DSPLIN
02475	C	* VERSION : JANUARY 1982 *	DSPLIN
02476	C	* DESCRIPTION : TO GENERATE THE COEFFICIENTS OF AN OBSERVATION *	DSPLIN
02477	C	* EQUATION AND SAVE IT IN 'A' MATRIX. *	DSPLIN
02478	C	*****	DSPLIN
02479	C	INPUT PARAMETERS	DSPLIN
02480	C	TXPT - TIME OF DATA POINT	DSPLIN
02481	C	TKNOT - TIME OF BEFORE KNOT OF THE INTERVAL IN WHICH THE TIME	DSPLIN
02482	C	DATA POINT FALLS	DSPLIN
02483	C	DINTK - TIME INTERVAL BETWEEN THE BEFORE KNOT AND AFTER KNOT	DSPLIN
02484	C	OF THE INTERVAL	DSPLIN
02485	C		DSPLIN
02486	C	OUTPUT PARAMETERS	DSPLIN
02487	C	A - THE MATRIX IN WHICH THE COEFFICIENTS ARE STORED	DSPLIN
02488	C		DSPLIN
02489	C	CALLS - DCLEAR	DSPLIN
02490	C	*****	DSPLIN
02491		REAL*8 A(7,1),X,Y	DSPLIN
02492		CALL DCLEAR(A,7,1)	DSPLIN
02493		DR = TXPT-TKNOT	DSPLIN
02494		DTR = DR/DINTK	DSPLIN
02495		X = (2.0000*DTR - 3.0000)*DTR*DTR	DSPLIN
02496		Y = 1.000 - DTR	DSPLIN


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02545 C PRLOBS: PRINT FORMULATED OBSERVATION VECTOR(1,0) DSPLIN
02546 C ICHECK: IMPLEMENTATION OF SUBR CHECK(1,0) DSPLIN
02547 C PRMAT: PRINT DESIGN MATRICES (1,0) - SEE MAIN DSPLIN
02548 C PRXMAT: PRINT LS ESTIMATED SOLUTION VECTOR(1,0) DSPLIN
02549 C PRVARX: PRINT COVARIANCE MATRIX OF LS ESTIMATES(1,0) DSPLIN
02550 C PRKNT : PRINT 'PRKNT' KNOT VALUES AND VARIANCE(1.,KNO)- SEE MAIN DSPLIN
02551 C PRRESO: PRINT RESIDUAL VECTOR(1,0) DSPLIN
02552 C PRCOFF: PRINT FORMULATED COEFFICIENTS(1,0) DSPLIN
02553 C PRCOFV: PRINT COAVRIANCE MATRIX OF COEFFICIENTS(1,0) DSPLIN
02554 C I TYPE : PLOTTER I - (1) LINE PRINTER CHCSEN DSPLIN
02555 C II- (0) ZETA/GOULD 5000 PLOTTER DSPLIN
02556 C SPLIN : NO OF TIME SUBR DESIGN IS TO BE CALLED(1.,99) - SEE MAIN DSPLIN
02557 C IANLYS: NO OF TIMES SUBR ANALYS IS TO BE CALLED(1.,99)- SEE MAIN DSPLIN
02558 C IPLOT : PLOTTING REQUIREMENTS OF SUBR ANALYS(1,0) - SEE SUBR ANALYS DSPLIN
02559 C *OPTIONAL INPUT(ONLY WHEN INVOKED FROM THE ABOVE) DSPLIN
02560 C IF SPLIN OPTION >= 1 :INPUT PRPTS,PRKNOT,DRAW AND PRGEN DSPLIN
02561 C SEE SUBR DESIGN FOR DETAILS (A-D) DSPLIN
02562 C IANLYS OPTION >= 1 :INPUT ITS 10 OPTIONS DSPLIN
02563 C SEE SUBR ANALYS FOR DETAILS (A-J) DSPLIN
02564 C SUBOPTION : IF ICANYS(8) = 1 INVOKED DSPLIN
02565 C GSTART - TIME TC BEGIN PRINT OF VALUES DSPLIN
02566 C GINT - TIME BETWEEN COMPUTATIONS DSPLIN
02567 C ISCT OPTION = 1 :INPUT THE TIME SCALE FACTOR DSPLIN
02568 C ICHI OPTION = 1 :INPUT NEW PERCENTAGE CONFIDENCE INTERVAL DSPLIN
02569 C IFLT OPTION = 1 :INPUT INTERVAL WIDTH, INCREMENT AND TEST DSPLIN
02570 C % LEVEL TO BE APPLIED - SEE FILTER (A-C) DSPLIN
02571 C IELIPS OPTION = 1 :INPUT NEW PERCENTAGE CONFIDENCE ELLIPSES DSPLIN
02572 C REQUIRED. DSPLIN
02573 C DRAW OR = 1 OR 2 :INPUT TIME OF BEGINNING OF CURVE AND POINT DSPLIN
02574 C ICANYS(9) XSTART - TIME OF BEGINNING OF CURVE DSPLIN
02575 C OPTION XINT - TIME BETWEEN COMPUTED POSITIONS DSPLIN
02576 C *END INPUT SEQUENCE DSPLIN
02577 C ADDITIONAL INFORMATION DSPLIN
02578 C SPLIN - PLOTTING OF SPLINE ** TOTAL CONTROL DSPLIN
02579 C DRAW - DRAW THE SPLINE DSPLIN
02580 C PRGEN - PRINT GENERATED DISCRETE POSITIONS OF DRAWN SPLINE DSPLIN
02581 C IPLOT - FOR PLOTTING IN THE ANALYS SUBROUTINE DSPLIN
02582 C ISCT - TIME SCALING FACTOR ON/OFF SWITCH DSPLIN
02583 C CALLS - ELSFAC DSPLIN
02584 C *PROGRAM BEGINS DSPLIN
02585 REAL*8 ELSFAC,CALPHA,GSTART,GINT DSPLIN
02586
02587
02588
02589
02590
02591
02592

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02593	REAL*8	SCTIME,DINT,DINC,XSTART,XINT,ALPH,ALPHA,FESC,ESC	DSPL IN
02594	INTEGER	CHANGE,IREAD,IFLT,IAPRI,ISCT,ICHI,IELIPS,ECHO,	DSPL IN
02595		PRCOV,PRPMAT,PRTX,PRTK,PRDTK,PRLOBS,ICHECK,	DSPL IN
02596	@	PRAMAT,PRXMAT,PRVARX,PRKNT,PRRESO,PRCOFF,PRCOFV,	DSPL IN
02597	@	ITYPE,SPLIN,PRPTS,PRKNOT,DRAW,PRGEN,IANLYS,IPLOT,	DSPL IN
02598	@	ICANYS(10)	DSPL IN
02599	C*	READ UNIT	DSPL IN
02600		IRD = 5	DSPL IN
02601	C*	WRITE UNIT	DSPL IN
02602		IWR = 6	DSPL IN
02603	C*		DSPL IN
02604	C	OPTIONS SELECTED (DEFAULT)	DSPL IN
02605	C*		DSPL IN
02606	C*	DATA SET CHANGE CONTROL VARIABLE	DSPL IN
02607		CHANGE = 0	DSPL IN
02608	C*	READ SPECIFICATION ?	DSPL IN
02609		IREAD = 1	DSPL IN
02610	C*	TO CALL FILTER ROUTINE OPTION	DSPL IN
02611		IFLT = 0	DSPL IN
02612	C*	CHOICE OF APRIORI VALUES	DSPL IN
02613		IAPRI = 0	DSPL IN
02614	C*	TIME SCALING OPTION	DSPL IN
02615		ISCT = 0	DSPL IN
02616		SCTIME = 1.000	DSPL IN
02617	C*	CHI-SQUARE TEST ON VARIANCE FACTOR CONDIENCE INTERVAL	DSPL IN
02618		ICHI = 0	DSPL IN
02619		CALPHA = 99.0	DSPL IN
02620	C*	CONFIDENCE ELLIPSE SCALE FACTOR OPTION: GOVERNS ALL ELLIPSES	DSPL IN
02621		IELIPS = 0	DSPL IN
02622		ESC = 1	DSPL IN
02623	C*	INPUT DATA PRINT AND DATA PRIOR TO COMPUTATIONS	DSPL IN
02624		ECHO = 1	DSPL IN
02625		PRCOV = 0	DSPL IN
02626		PRPMAT = 0	DSPL IN
02627		PRTX = 0	DSPL IN
02628		PRTK = 1	DSPL IN
02629		PRDTK = 0	DSPL IN
02630		PRLOBS = 0	DSPL IN
02631	C*	OPTION ON THE CHECK ROUTINE	DSPL IN
02632		ICHECK = 0	DSPL IN
02633	C*	COMPUTED DATA PRINT	DSPL IN
02634		PRAMAT = 0	DSPL IN
02635		PRXMAT = 1	DSPL IN
02636		PRVARX = 0	DSPL IN
02637		PRKNT = 0	DSPL IN
02638		PRRESO = 1	DSPL IN
02639		PRCOFF = 1	DSPL IN
02640		PRCOFV = 0	DSPL IN

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02641 C* PLOTTING CONTROL
02642 ITYPE = 0 DSPLIN
02643 SPLIN = 1 DSPLIN
02644 PRPTS = 1 DSPLIN
02645 PRKNOT = 1 DSPLIN
02646 DRAW = 0 DSPLIN
02647 PRGEN = 0 DSPLIN
02648 C* PLOT OTHER THAN SPLINE DRAWING DSPLIN
02649 IANLYS = 0 DSPLIN
02650 IPLOT = 0 DSPLIN
02651 C* IS THE DEFAULT SET OPTIONS TO BE CHANGED ? DSPLIN
02652 READ(IRD,*)IOPTON DSPLIN
02653 IF(IOPTON.EQ.0)RETURN DSPLIN
02654 C* READ IN THE NEW OPTIONS DSPLIN
02655 READ(IRD,*)CHANGE,IREAD,IFLT,IAPRI,ISCT,ICHI,IELIPS,ECHO,
02656 @ PRCOV,PRPMAT,PRTX,PRTK,PRDTK,PRLOBS,ICHECK, DSPLIN
02657 @ PRMAT,PRXMAT,PRVARX,PRKNT,PRRESO,PRCOFF,PRCOFV, DSPLIN
02658 ITYPE,SPLIN,IANLYS,IPLOT DSPLIN
02659 IF(ECHO.EQ.1)WRITE(IWR,7560)CHANGE,IREAD,IFLT,IAPRI,ISCT,ICHI,
02660 @ IELIPS,ECHO,PRCOV,PRPMAT,PRTX,PRTK,PRDTK,PRLOBS,ICHECK, DSPLIN
02661 @ PRMAT,PRXMAT,PRVARX,PRKNT,PRRESO,PRCOFF,PRCOFV, DSPLIN
02662 @ ITYPE,SPLIN,IANLYS,IPLOT DSPLIN
02663 C* OPTIONS RELATED TO SPLINE PLOT DSPLIN
02664 IF(SPLIN.NE.0)READ(IRD,*)PRPTS,PRKNOT,DRAW,PRGEN DSPLIN
02665 IF(ECHO.EQ.1.AND.SPLIN.NE.0)WRITE(IWR,7560)PRPTS,PRKNOT,DRAW,PRGEN DSPLIN
02666 C* OPTIONS RELATED TO ANALYS SUBROUTINE DSPLIN
02667 IF(IANLYS.NE.0)READ(IRD,*)(ICANYS(I),I = 1,10) DSPLIN
02668 IF(ECHO.EQ.1.AND.IANLYS.NE.0)WRITE(IWR,7560)(ICANYS(I),I=1,10) DSPLIN
02669 IF(IANLYS.NE.0.AND.ICANYS(8).EQ.1)READ(IRD,*)GSTART,GINT DSPLIN
02670 IF(ECHO.NE.0.AND.ICANYS(8).EQ.1)WRITE(IWR,7530)GSTART,GINT DSPLIN
02671 C* OPTION RELATED TO THE TIMSC ROUTINE DSPLIN
02672 IF(ISCT.EQ.1)READ(IRD,*)SCTIME DSPLIN
02673 IF(ISCT.EQ.1.AND.ECHO.EQ.1)WRITE(IWR,7520)SCTIME DSPLIN
02674 C* OPTION RELATED TO THE CHI SQUARED TEST ON VARIANCE FACTOR DSPLIN
02675 IF(ICHI.EQ.1)READ(IRD,*)CALPHA DSPLIN
02676 IF(ICHI.EQ.1.AND.ECHO.EQ.1)WRITE(IWR,7520)CALPHA DSPLIN
02677 C* OPTIONS RELATED TO THE FILTER ROUTINE DSPLIN
02678 IF(IFLT.EQ.0)GO TO 10 DSPLIN
02679 READ(IRD,*)DINT,DINC,ALPH DSPLIN
02680 IF(ECHO.EQ.1)WRITE(IWR,7520)DINT,DINC,ALPH DSPLIN
02681 FESC = ELSFAC(ALPH) DSPLIN
02682 C* CONFIDENCE ELLIPSE SET AT THE ALPHA PERCENTAGE LEVEL DSPLIN
02683 10 IF(IELIPS.NE.1)GO TO 20 DSPLIN
02684 READ(IRD,*)ALPHA DSPLIN
02685 WRITE(IWR,7520)ALPHA DSPLIN
02686 ESC = ELSFAC(ALPHA) DSPLIN
02687 C* READ POINT OF START OF CURVE AND INTERVAL- FOR DESIGN AND ANALYS DSPLIN
02688 20 IF(DRAW.EQ.0.AND.IANLYS.EQ.0)GC TC 999 DSPLIN

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02737      IF (PRDTK.EQ.1) CALL DPRINT(DTK,KNO,1,1DOTK,'INTERVAL BET KNOTS',9) DSPLIN
02738      IF (PRPMAT.EQ.1) CALL DPRINT(P,N,3,1DP,3,'BANDED P-MATRIX',8) DSPLIN
02739      IF (PRMAT.NE.1) RETURN DSPLIN
02740      L = N/2 DSPLIN
02741      WRITE(IWR,7030)(ADDA1(I),I=1,L) DSPLIN
02742      CALL DPRINT(A1,L,7,IDA1,7,'CONDENSED A1-MATRIX',10) DSPLIN
02743      L = R/2 DSPLIN
02744      WRITE(IWR,7040)(ADDA2(I),I=1,L) DSPLIN
02745      CALL DPRINT(A2,L,11,IDA2,11,'CONDENSED A2-MATRIX',10) DSPLIN
02746 C* DSPLIN
02747 7000 FORMAT(//,3X,'INPUT TIME OF DATA POINTS',//, DSPLIN
02748 @100(2X,8(1PD12.5,1X),/),//) DSPLIN
02749 7020 FORMAT(//,3X,'INPUT COVARIANCE',//, DSPLIN
02750 @100(5X,1PD12.5,3X,1PD12.5,/,5X,1PD12.5,3X,1PD12.5,//),//) DSPLIN
02751 7030 FORMAT(/,3X,'ADDRESS A1',/,3X,10(10I4,/,3X)) DSPLIN
02752 7040 FORMAT(/,3X,'ADDRESS A2',/,3X,10(10I4,/,3X)) DSPLIN
02753 RETURN DSPLIN
02754 END DSPLIN
02755 SUBROUTINE PLOT(ZIHF,ZIHC,ZIOPX,ZIDPY,ZLX,ZLY,ZUX,ZUY) DSPLIN
02756 C ***** DSPLIN
02757 C * VERSION : 24TH MARCH 1982 DSPLIN
02758 C * DESCRIPTION : LAYS OUT THE PLOT REQUIREMENTS: PLOT SIZE, GRID ETC *DSPLIN
02759 C ***** DSPLIN
02760 C PARAMETERS REQUESTED BY SUBROUTINE - READ DIRECTLY FROM UNIT IRD DSPLIN
02761 C DSPLIN
02762 C A) READ IN THE TITLE TO BE PRINTED ON PLOT DSPLIN
02763 C B) READ IN THE TITLE WITH THE X AXIS- EASTINGS DSPLIN
02764 C C) READ IN THE TITLE WITH THE Y AXIS - NORTHINGS DSPLIN
02765 C B) READ IN SIZE (INCH) AND CORNER COORD OF THE PLOT DSPLIN
02766 C E) READ THE ORIGIN(AXES) AND THE INTERVAL BET TICK MARKS DSPLIN
02767 C FIRST ALONG X THEN ALONG Y DSPLIN
02768 C F) READ PRINT AXES OFFSET(OFFX,OFFY) DSPLIN
02769 C AND PRINT SCALE FACTORS(SCX,SCY) DSPLIN
02770 C DSPLIN
02771 C CALLS - AREA,RECT,CHRPRT,AXS (FORTPLOT LIBRARY ROUTINES ) DSPLIN
02772 C DSPLIN
02773 C ADDITIONAL INFORMATION DSPLIN
02774 C COMPUTING THE LENGTH OF THE AXES DSPLIN
02775 C WORKINGS - THE SECTION FIRST COMPUTES THE LENGTH OF THE AXES BY DSPLIN
02776 C DEDUCTING 2* INTERVAL FORM THE PLOT SIZE. THIS IS THEN DSPLIN
02777 C DIVIDED BY THE INTERVAL AND THE NEAREST INTEGER ACCEPTED DSPLIN
02778 C AS THE MAX OF OF TICKS IN THE LINE. FROM THIS , THE DSPLIN
02779 C LENGTH OF THE AXES ARE COMPUTED - IN INCHES. DSPLIN
02780 C VARIABLES DSPLIN
02781 C ZINC - INTERVAL BETWEEN TICK MARKS ON THE X - AXIS DSPLIN
02782 C ZINT - INTERVAL BETWEEN TICK MARKS ON THE Y - AXIS DSPLIN
02783 C ZHT - HEIGHT OF THE TITLE CHARACTERS IN Y USER UNITS DSPLIN
02784 C ZIDP - THE VARIABLE TO BE SET IN USER UNITS FOR THE DISPLACEMENTS DSPLIN

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02785 C          OF THE NUMBERS OF THE KNOTS AND NOT KNOTS FROM THE POINT.      DSPLIN
02786 C      ZIHF - VARIABLE USED TO DEFINE THE HEIGHT OF THE SYMBOLS           DSPLIN
02787 C          IN Y USER UNITS                                               DSPLIN
02788 C      ZCHT - VARIABLE USED TO DEFINE THE HT OF THE CHARACTERS ALONG THE  DSPLIN
02789 C          AXES IN Y USER UNITS                                          DSPLIN
02790 C      ZIHC - VARIABLE DEFINING THE RADIUS OF THE CIRCLE IN X USER UNITS DSPLIN
02791 C
02792 C      NOTE                                                                DSPLIN
02793 C          AREA WITHIN AXES IS LOWER LEFT (ZLX,ZLY)                     DSPLIN
02794 C          UPPER RIGHT (ZUX,ZUY)                                         DSPLIN
02795 C          ZIHF AND ZIHC ARE THE NEGATIVE OF THEIR COORD VALUES        DSPLIN
02796 C          *****
02797 C* SUBROUTINE BEGINS                                                    DSPLIN
02798 C      LOGICAL*1 XAXIS(50),YAXIS(45),TITLE(41)                          DSPLIN
02799 C      DATA XAXIS/49*' ',.201/,YAXIS/44*' ',.201/                      DSPLIN
02800 C      DATA TITLE/40*' ',.201/                                         DSPLIN
02801 C* READ FROM UNIT                                                       DSPLIN
02802 C      IRD = 5                                                            DSPLIN
02803 C*
02804 C      READ(IRD,9040)(TITLE(I),I = 1,40)                                DSPLIN
02805 C      READ(IRD,9040)(XAXIS(I),I = 1,49)                                DSPLIN
02806 C      READ(IRD,9040)(YAXIS(I),I = 1,44)                                DSPLIN
02807 C      READ(IRD,*)ZXSIZE,ZYSIZE,ZXMIN,ZYMIN,ZXMAX,ZYMAX                 DSPLIN
02808 C      READ(IRD,*)ZAX,ZAY,ZINC,ZINT                                     DSPLIN
02809 C      READ(IRD,*)OFFX,OFFY,SCX,SCY                                     DSPLIN
02810 C*
02811 C      IF(SCX.EQ.0)SCX = 1.0                                             DSPLIN
02812 C      IF(SCY.EQ.0)SCY = 1.0                                             DSPLIN
02813 C      IF(ZINC.EQ.0)ZINC = 1.0                                           DSPLIN
02814 C      IF(ZINT.EQ.0)ZINT = 1.0                                           DSPLIN
02815 C      CALL AREA(ZXSIZE,ZYSIZE)                                          DSPLIN
02816 C      CALL SETPLT(ZXMIN,ZYMIN,ZXMAX,ZYMAX)                              DSPLIN
02817 C* CONSTRUCT RECTANGLE AROUND PHYSICAL PLOT SIZE                       DSPLIN
02818 C      ZX = ZXMAX - ZXMIN                                                DSPLIN
02819 C      ZY = ZYMAX - ZYMIN                                                DSPLIN
02820 C      ZXMIN = ZXMIN - ZX/1000                                           DSPLIN
02821 C      ZYMIN = ZYMIN - ZY/1000                                           DSPLIN
02822 C* SCALE                                                                 DSPLIN
02823 C      XSC = ZX/ZXSIZE                                                    DSPLIN
02824 C      YSC = ZY/ZYSIZE                                                    DSPLIN
02825 C      CALL RECT(ZXMIN,ZYMIN,-ZX,-ZY)                                    DSPLIN
02826 C* PRINTING OF TITLE ON PLOT                                           DSPLIN
02827 C      ZHT = ZX/44                                                        DSPLIN
02828 C      ZHTY = ZHT*(YSC/XSC)                                              DSPLIN
02829 C      ZXP = ZXMIN + 2.0*ZHT                                              DSPLIN
02830 C      ZYP = ZYMAX - 2.0*ZHTY                                            DSPLIN
02831 C      CALL CHRPRT(ZXP,ZYP,TITLE,0.0,-ZHTY)                              DSPLIN
02832 C* DRAWING THE AXES                                                     DSPLIN

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02881 C
02882 C CALLS - INTERV,FORM,DMULT
02883 C - TRAPS
02884 C
02885 C* PROGRAM BEGINS
02886 COMMON /DIM1/IOBSNO,IOA1,IOW1,IDTX,IDP,IOPV,IOLOBS,IOVAR,IOV
02887 COMMON /DIM2/IDKNOT,IDA2,IDTK,IDTK,IDX,IOVX,IOW2,IOV2,IOX0,
02888      2 IDCOF,IOVCOF
02889 REAL*8 X(2,1),VX(2,2),B(2,8),TK(IDTK,1),
02890      2 COF(IDCOF,8),VCOF(10VCOF,8,8),CO(8,1),VCO(8,8)
02891 INTEGER*4 KNO
02892 DATA ISWT/0/,B/16*0.000/
02893 ICODE = 1
02894 CALL INTERV(T,TK,KNO,J,IDTK,IC)
02895 IF(IC.EQ.0)GO TO 10
02896 DR = T - TK(J,1)
02897 CALL FORM(DR,B)
02898 C** EXTRACTING THE COEFFICIENTS AND COVARIANCES
02899 IF(ISWT.EQ.J)GO TO 30
02900 DO 20 IJ = 1,8
02901 CO(IJ,1) = COF(J,IJ)
02902 DO 20 IK = 1,8
02903      20 VCO(IJ,IK) = VCOF(J,IJ,IK)
02904 ISWT = J
02905 CALL TRAPS(0,0,10000,0,0)
02906      30 CALL DMULT(B,2,8,CO,8,1,X,2,8,8,1,2,1)
02907 DO 40 I = 1,2
02908     DO 40 L = 1,2
02909     VX(I,L) = 0.000
02910     DO 40 J = 1,8
02911     DO 40 K = 1,8
02912     40 VX(I,L) = VX(I,L) + B(I,K)*VCO(K,J)*B(L,J)
02913     X1 = X(1,1)
02914     X2 = X(2,1)
02915     VX1 = VX(1,1)
02916     VX2 = VX(2,2)
02917     VX12 = VX(1,2)
02918     RETURN
02919     10 WRITE(6,900)T
02920     ICODE = 0
02921     RETURN
02922     900 FORMAT(//,2X,'TIME ',D12.5,' AT WHICH POSITION IS REQUESTED ',
02923     2 /,' LIES OUTSIDE THE TIME DEFINED BY THE OUTER ',
02924     2 ' KNOTS',//)
02925 END
02926 SUBROUTINE PREPAR(KNO,NO,R,M,N, TX,TK,DTK,AOBS,ACON,
02927      2 A1,ADDA1,A2,ADDA2,
02928      2 XO,LCBS,W1,W2,IAPRI)

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02929      IMPLICIT REAL*8(A-H,O-Y),REAL*4(Z)
02930      C *****
02931      C *   VERSION      :   7 JUNE 1982
02932      C *   DESCRIPTION :   PREPARES MATRICES FOR INPUT INTO THE LS ROUTINE
02933      C *****
02934      C INPUT PARAMETERS
02935      C   KNO,NO,R,M,N - AS IN MAIN
02936      C   TX,TK,DTK,XO,LOBS
02937      C               - AS IN MAIN
02938      C   IAPRI          - INPUT CODE OF APRIORI SOLN VECTOR
02939      C
02940      C OUTPUT PARAMETERS
02941      C   A1,A2          - VARIABLE PROFILE BANDED DESIGN MATRICES( DIM BELOW)
02942      C   ADDA1,ADDA2   - ADDRESS SEQUENCE FOR A1 AND A2 MATRICES RESP.
02943      C   W1,W2         - MISCLOSURE VECTORS
02944      C
02945      C WORK ARRAYS
02946      C   AOBS,ACON - AS DIMENSIONED IN MAIN
02947      C
02948      C CALLS - DCLEAR,INTERV,CONSTR,APRORI,OBS
02949      C *****
02950      COMMON /DIM1/IOBSNO,IDA1,IDW1,IDX,IDV,IDLV,IDLQBS,ICVAR,ICV
02951      COMMON /DIM2/IDKNOT,IDA2,IDX,IDVX,IDW2,IDV2,IDX,
02952      @         IDCOF,IOVCOF
02953      C* ARRAYS
02954      REAL*8 A1(IDA1,7),A2(IDA2,11),TX(IDTX,1),TK(IDTK,1),DTK(IDCTK,1),
02955      @         ZO,AOBS(7,1),ACCN(11,1),
02956      @         XO(IDXO,1),LOBS(IDLOBS,1),W1(IDW1,1),W2(IDW2,1)
02957      C* OTHERS
02958      INTEGER ADDA1(IDA1),ADDA2(IDA2),KNO,NO,R,M,N,IAPRI
02959      C* FUNCTIONS
02960      IROW(I) = (I+1)/2
02961      ICOL(I) = (2-((I+1)/2 - (I/2)))
02962      C* PSEUDO MATRIX SIZES  A1(N,M) , A2(R,M) , P(N,N) , VAR(N-R,N)
02963      R = 2*KNO - 4
02964      M = 4*KNO
02965      N = 2*NO + 8
02966      C* CLEARING THE A MATRICES
02967      CALL DCLEAR(A1,IDA1,7)
02968      CALL DCLEAR(A2,IDA2,11)
02969      C* FORMULATION OF THE A1 MATRIX
02970      J = 1
02971      L = NO + 2
02972      DO 31 I1 = 3,L
02973      J = J + 1
02974      CALL INTERV(TX(J,1),TK,KNO,INT,IDTK,ICODE)
02975      IF(ICODE.EQ.0)WRITE(6,9000)J
02976      IF(ICODE.EQ.0)STOP

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03169      9000 FORMAT(/, ' ERROR : INPUT COVARIANCE SINGULAR - PROG STOPPED ',//)DSPLIN
03170      END DSPLIN
03171      SUBROUTINE READ(IEND,LINE,T,X,Y,SX,SY,SXY,ICODE1,ICODE2) DSPLIN
03172      IMPLICIT REAL*8(A-H,C-Z) DSPLIN
03173      REAL*8 T,X,Y,SX,SY,SXY DSPLIN
03174      C ***** DSPLIN
03175      C * VERSION : 12TH SEPT 1982 DSPLIN
03176      C * DESCRIPTION : READ IN DATA ACCORDING TO OPTION CODE * DSPLIN
03177      C ***** DSPLIN
03178      C INPUT PARAMETERS DSPLIN
03179      C ICODE1 - CHOICE OF THE DIFFERENT READS DSPLIN
03180      C 1 - NORMAL INPUT DSPLIN
03181      C 2 - NORMAL INPUT BUT WITH CORRELATION COEFFICIENT DSPLIN
03182      C 3 - LOREX DATA FORMAT WITH NO MODIFICATION TO VARIANCES DSPLIN
03183      C 4 - BEGINNING AND END KNOT SLOPE AND VARIANCE INTAKE DSPLIN
03184      C 5 - LOREX DATA FORMAT WITH MODIFICATION TO VARIANCES DSPLIN
03185      C 7 - LOREX DATA FORMAT WITH VELO AND DIR (CORRS APPLIED) DSPLIN
03186      C 9 - LOREX DATA FORMAT WITH VELO AND DIR (CORRS NOT APPLIED) DSPLIN
03187      C ICODE2 - INPUT ECHO REQUEST ; 1 - YES MODIF TC VAR PRINTED. DSPLIN
03188      C 0 - NO DSPLIN
03189      C IEND - TOTAL NUMBER OF LINES TO BE READ(END KNOT INPUT DETECTN) DSPLIN
03190      C LINE - CURRENT LINE CF INPUT DSPLIN
03191      C DSPLIN
03192      C OUTPUT PARAMETERS DSPLIN
03193      C T,X,Y - DATA POINT DEFINED BY COORDS X,Y, AT TIME T DSPLIN
03194      C SX,SY - STANDARD DEVIATIONS OF X,Y DSPLIN
03195      C SXY - COVARIANCE DSPLIN
03196      C DSPLIN
03197      C CALLS - UPSTD, ERRORS DSPLIN
03198      C - CABS DSPLIN
03199      C DSPLIN
03200      C PROGRAM BEGINS DSPLIN
03201      C* READ INPUT UNIT NUMBER - IRD DSPLIN
03202      IRD = 5 DSPLIN
03203      C* WRITE INPUT UNIT NUMBER - IWR DSPLIN
03204      IWR = 6 DSPLIN
03205      C* DSPLIN
03206      IF(ICODE1.NE.1)GO TO 10 DSPLIN
03207      C* NORMAL INPUT : COVARIANCE READ DSPLIN
03208      READ(IRD,*)T,X,Y,SX,SY,SXY DSPLIN
03209      IF(ICODE2.EQ.1)WRITE(IWR,110)T,X,Y,SX,SY,SXY DSPLIN
03210      RETURN DSPLIN
03211      10 IF(ICODE1.NE.2)GO TO 20 DSPLIN
03212      C* CORRELATION COEFFICIENT READ DSPLIN
03213      READ(IRD,*)T,X,Y,SX,SY,SXY DSPLIN
03214      IF(ICODE2.EQ.1)WRITE(IWR,110)T,X,Y,SX,SY,SXY DSPLIN
03215      SXY = (SXY/100.000)*SX*SY DSPLIN
03216      RETURN DSPLIN

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03217      20      IF(ICODE1.NE.3.AND.ICODE1.NE.5      DSPLIN
03218      @ .AND.ICODE1.NE.7.AND.ICODE1.NE.9)GO TO 30      DSPLIN
03219      C -----      DSPLIN
03220      C      INPUT VARIATION WITH A CORRELATION COEFFICIENT      DSPLIN
03221      C      NOTE THAT THE X,Y (EAST,NORTH) READ SEQUENCE HAS BEEN CHANGED      DSPLIN
03222      C      TO MATCH LOREX INPUT DATA FORMAT AND THAT THE VELOCITY AND THE      DSPLIN
03223      C      DIRECTION OF MOTION IS READ IN      DSPLIN
03224      C      VELO AND DIREC ARE REQUESTED ONLY FOR THE FIXES AND NOT END      DSPLIN
03225      C      KNOT INFORMATION.      DSPLIN
03226      C -----      DSPLIN
03227      C* END KNOT INFORMATION INTAKE      DSPLIN
03228      IF(LINE.NE.1.AND.LINE.NE.IEND)GO TO 23      DSPLIN
03229      READ(IRD,*)IDAY,IHRMIN,Y,X,SY,SX,SXY      DSPLIN
03230      IF(ICODE2.EQ.1)WRITE(IWR,120)IDAY,IHRMIN,Y,X,SY,SX,SXY      DSPLIN
03231      GO TO 24      DSPLIN
03232      C* DATA POINT ,VELO AND DIRECTION INTAKE      DSPLIN
03233      23      IF(ICODE1.EQ.3.OR.ICODE1.EQ.5)READ(IRD,*)IDAY,IHRMIN,Y,X,SY,SX,SXY      DSPLIN
03234      IF(ICODE1.EQ.7)READ(IRD,*)IDAY,IHRMIN,Y,X,SY,SX,SXY,VELO,DR      DSPLIN
03235      IF(ICODE1.EQ.9)READ(IRD,*)IDAY,IHRMIN,Y,X,SY,SX,SXY,VELO,DR      DSPLIN
03236      C* ECHO OUTPUT      DSPLIN
03237      IF(ICODE2.EQ.1.AND.ICODE1.EQ.7)      DSPLIN
03238      @      WRITE(IWR,120)IDAY,IHRMIN,Y,X,SY,SX,SXY,VELO,DR      DSPLIN
03239      IF(ICODE2.EQ.1.AND.(ICODE1.EQ.3.OR.ICODE1.EQ.5.OR.ICODE1.EQ.9))      DSPLIN
03240      @      WRITE(IWR,120)IDAY,IHRMIN,Y,X,SY,SX,SXY      DSPLIN
03241      C* CONVERSION OF CORRELATION TO COVARIANCE      DSPLIN
03242      24      IF(DABS(SXY).EQ.100.0)SXY = (SXY/DABS(SXY))*99.999D0      DSPLIN
03243      SXY = (SXY/100.0D0)*SX*SY      DSPLIN
03244      IHR = IHRMIN/100      DSPLIN
03245      XMIN = (IHRMIN - (IHRMIN/100)*100)      DSPLIN
03246      T = IDAY + (IHR/24.0D0) + (XMIN/1440.0D0)      DSPLIN
03247      IF(ICODE1.NE.5.AND.ICODE1.NE.7)RETURN      DSPLIN
03248      C* AVOID MODIFICATIONS ON THE FIRST AND LAST LINES      DSPLIN
03249      IF(LINE.EQ.1.OR.LINE.EQ.IEND)RETURN      DSPLIN
03250      C* STANDARD DEVIATION CORRECTION      DSPLIN
03251      CALL UPSTD(SX,SY,SXY,ICODE2)      DSPLIN
03252      C* CROSS TRACK CORRECTION      DSPLIN
03253      IF(ICODE1.NE.7)RETURN      DSPLIN
03254      DIR = DR*(3.141592654D0/180.0D0)      DSPLIN
03255      CALL ERRORS(X,Y,SX,SY,SXY,VELO,DIR,ICODE2)      DSPLIN
03256      RETURN      DSPLIN
03257      30      IF(ICODE1.NE.4)GO TO 500      DSPLIN
03258      C* SLOPE AND ITS CORRELATION INPUT      DSPLIN
03259      READ(IRD,*)Y,X,SY,SX,SXY      DSPLIN
03260      IF(ICODE2.EQ.1)WRITE(IWR,110)Y,X,SY,SX,SXY      DSPLIN
03261      SXY = (SXY/100.0D0)*SX*SY      DSPLIN
03262      RETURN      DSPLIN
03263      C*      DSPLIN
03264      C* FURTHER INPUT FORMATS TO BE HERE      DSPLIN

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03793           C           THE INPUT UPPER LEFT N BY N PORTION.
03794           C
03795           C           DET - THE NON-EXPONENT PORTION OF THE DETERMINANT OF THE
03796           C           INPUT N BY N (UPPER LEFT PORTION OF Q) MATRIX. SEE
03797           C           IDEXP BELOW.
03798           C
03799           C           IDEXP - THE EXPONENT (OF 10) PART OF THE DETERMINANT DESCRIBED
03800           C           UNDER DET ABOVE.  THUS THE DETERMINANT IS RETURNED IN
03801           C           TWO PARTS CORRESPONDING TO
03802           C           DETERMINANT = DET * 10 ** IDEXP .
03803           C           THIS IS DONE TO AVOID UNDER OR OVERFLOW IN THE
03804           C           COMPUTATION OF THE DETERMINANT.  TO PRINT THE DETERM-
03805           C           INANT THE USER SHOULD PRINT BOTH NUMBERS AS FOLLOWS:
03806           C           (FOR EXAMPLE)
03807           C           PRINT 10,DET,IDEXP
03808           C           10 FORMAT(' ','DETERMINANT= ',F7.4,'D',I4)
03809           C
03810           C
03811           C
03812           C
03813           C
03814           C           IMPLICIT REAL*8 (A-H,O-Z), INTEGER*4 (I-N)
03815           C           DIMENSION Q(MM,MM)
03816           C           DET=0.00
03817           C           DO 4 J=1,N
03818           C           DO 4 I=1,J
03819           C           IF(I.EQ.1) GO TO 2
03820           C           M=I-1
03821           C           SUM=0.000
03822           C           DO 1 K=1,M
03823           C           1 SUM=SUM+Q(K,I)*Q(K,J)
03824           C           Q(I,J)=Q(I,J)-SUM
03825           C           2 IF(I.EQ.J) GO TO 3
03826           C           Q(I,J)=Q(I,J)/Q(I,I)
03827           C           GO TO 4
03828           C           3 CONTINUE
03829           C           DET=DET+DLOG10(Q(I,I))
03830           C           Q(I,I)=DSCRT(Q(I,I))
03831           C           4 CONTINUE
03832           C           IDEXP=DET
03833           C           RPART=DET-IDEXP
03834           C           APART=DABS(RPART)
03835           C           IF(APART.LT.1.0-20) DET=1.00
03836           C           IF(APART.LT.1.0-20) GO TO 10
03837           C           DET=10**RPART
03838           C           10 CONTINUE
03839           C           DO 7 J=1,N
03840           C           DO 7 I=1,J

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R.R. STEEVES
SEPT., 1979


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03889 C
03890 C ADDITIONAL INFORMATION DSPLIN
03891 C XLEVEL - LARGEST VALUE OF INTERNAL COMPUTATIONAL ACCURACY ACCEPTABLE DSPLIN
03892 C BEFORE REJECTION OF COMPUTATIONS WITH ICODE = 2 DSPLIN
03893 C XLCON - LARGEST VALUE OF CONDITION NUMBER ACCEPTED DSPLIN
03894 C IF EXCEED, ICODE = 3 DSPLIN
03895 C 7 JULY - UPGRADE TO TAKE 204 SIZE MATRICES DSPLIN
03896 C DSPLIN
03897 C CALLS - COND.CHOLD.RESID.DMAG.BMULT1.SCMULT DSPLIN
03898 C ***** DSPLIN
03899 C DSPLIN
03900 REAL*8 A(IA,JA),P(IP,JP),W(IW,1),X(IX,1),VX(IVX,IVX), DSPLIN
03901 @ ATP(8,204),ATPW(8,1),DET,VTV,SO,V(IV,1),PV(204,1),ATPV(8,1) DSPLIN
03902 INTEGER PCODE DSPLIN
03903 EQUIVALENCE (ATPV(1),ATPW(1),PV(1)) DSPLIN
03904 DATA XLEVEL/1.0D-5/,XLCON/1.0D+8/ DSPLIN
03905 C* FUNCTION DSPLIN
03906 IROW(I) = (I+1)/2 DSPLIN
03907 ICOL(I) = (2 - (((I+1)/2) - (I/2))) DSPLIN
03908 C* NUMBER OF CODIAGONALS DSPLIN
03909 ICO = (JP-1)/2 DSPLIN
03910 C* ERROR CODE SET DSPLIN
03911 ICODE = 0 DSPLIN
03912 C* DIMENSION ALLOCATION DSPLIN
03913 IDATP = 8 DSPLIN
03914 JDATP = 56 DSPLIN
03915 IDATPV = 8 DSPLIN
03916 IDPV = 56 DSPLIN
03917 IDATPW = 8 DSPLIN
03918 C* FORN NORMALS DSPLIN
03919 DO 10 I = 1,M DSPLIN
03920 DO 10 J = 1,N DSPLIN
03921 ATP(I,J) = 0.000 DSPLIN
03922 IB = J - ICO DSPLIN
03923 IE = J + ICO DSPLIN
03924 IF(IB.LT.1)IB = 1 DSPLIN
03925 IF(IE.GT.N)IE = N DSPLIN
03926 DO 10 K = IB,IE DSPLIN
03927 JAC = J - K + ICO + 1 DSPLIN
03928 IJ = I - ICOL(K) + 1 DSPLIN
03929 IF(IJ.LT.1.OR.IJ.GT.JA)GO TO 10 DSPLIN
03930 IK = IROW(K) DSPLIN
03931 ATP(I,J) = ATP(I,J) + A(IK,IJ)*P(K,JAC) DSPLIN
03932 10 CONTINUE DSPLIN
03933 DO 20 I = 1,M DSPLIN
03934 DO 30 J = 1,M DSPLIN
03935 VX(I,J) = 0.000 DSPLIN
03936 IF(J.GT.I)GO TO 20 DSPLIN

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04033       RETURN
04034       END
04035       SUBROUTINE UPSTD(SX,SY,SXY,ICODE)
04036 C *****
04037 C * VERSION      : SEPT 1982
04038 C * DESCRIPTION : MINIMUM ALLOWABLE MINOR AXIS TO BE *
04039 C *              ENFORCED.
04040 C *****
04041 C INPUT PARAMETERS
04042 C  SX,SY,SXY - STD DEVIATIONS AND COVARIANCE
04043 C  ICODE   - PRINT CODES
04044 C
04045 C OUTPUT PARAMETERS
04046 C  SX,SY,SXY - SCALED STD DEVIATIONS AND COVARIANCE
04047 C
04048 C FURTHER INFORMATION
04049 C  MINB      - SET MINIMUM ALLOWABLE SEMI-MINOR AXIS OF THE ERROR
04050 C             ELLIPSES AND IF IT FALLS BELOW THIS
04051 C             SET FIGURE, THE SEMI-MINOR AXIS IS SCALED TO
04052 C             THIS VALUE WITH THE MAJOR AXIS BEING SCALED ACCORDINGLY.
04053 C  SETMIN    - MINIMUM VALUE ALLOWED OF THE SEMI MINOR AXIS. IF IT
04054 C             FALLS BELOW THIS NUMBER, THE AXIS IS REPLACED BY SETMIN.
04055 C
04056 C CALLS      - FLIPSE, ELLSIG
04057 C            *****
04058 C            REAL*8 SX,SY,SXY,MINB,SETMIN,SCB,A,B,DR,VX,VY
04059 C            DATA MINB/40.0D0/,SETMIN/1.0D0/
04060 C            VX = SX*SX
04061 C            VY = SY*SY
04062 C            CALL ELIPSE(VX,VY,SXY,A,B,1.0D0,DR)
04063 C            IF(ICODE.EQ.1)WRITE(6,9000)SY,SX,SXY,A,B
04064 C            IF(B.LT.SETMIN)B = SETMIN
04065 C            IF(B.EQ.SETMIN)CALL ELLSIG(A,B,DR,SX,SY,SXY,1)
04066 C            IF(B.GT.MINB)RETURN
04067 C            SCB = MINB/B
04068 C            B = MINB
04069 C            A = SCB*A
04070 C            SX = SCB*SX
04071 C            SY = SCB*SY
04072 C            SXY = SCB*SCB*SXY
04073 C            IF(ICODE.EQ.1)WRITE(6,9010)MINB,SY,SX,SXY,A,B,SCB
04074 C 9000    FORMAT(/,3X,'INPUT ERROR ELLIPSE (SN,SE,SEN,A AND B) : ',
04075 C            6(F9.1,2X),'. M')
04076 C 9010    FORMAT( 3X,'ACCEPTED (MIN: ',F5.1,')- MOD BY UPSTD : ',
04077 C            5(F9.1,2X),'. M' ( X ',F6.1,' )')
04078 C            RETURN
04079 C            END
04080 C            SUBROUTINE VARFAC(SO,DEGOF,NO,R,M,N,ALPHA,TX,P,V,PV,VTWV,DX1,DX2) OSPLIN

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04273      SVN = SCTIME*SVN/DCONV
04274      CVEN = SCTIME*SCTIME*CVEN/(DCONV*DCONV)
04275      WRITE(IWR,9030)II,TRU,SPEED,DR,VE,VN,SVE,SVN,CVEN
04276    10  CONTINUE
04277  9010  FORMAT(///,3X,'SMOOTHED VELOCITIES AT INPUT DATA TIMES',/)
04278  9020  FORMAT(//,10X,'PREDICTED VELOCITIES AT SPECIFIED TIMES',/10X,
04279      .19('=='),//,2X,'NO',6X,'TIME',9X,'SPEED(M/HR)',3X,'DIR(DEG)',7X,
04280      .'VELOCITIES(E,N):M/HR      SIGMA VELO(E,N)',9X,'COVARIANCE',
04281      .//)
04282  9030  FORMAT(2X,I4,2X,F10.4,10(F12.3,2X))
04283      RETURN
04284      END
04285      SUBROUTINE LS2(C,D,G,H,P,W1,W2,X,VX,V,R,M,N,IC,JC,JD,
04286      @      IG,JG,IH,JH,IP,JP,IW1,IW2,IX,IV,IER)
04287      IMPLICIT REAL*8(A-H,P-Z)
04288  C *****
04289  C * VERSION      : JANUARY 1982
04290  C * DESCRIPTION  : PERFORMS THE METHOD OF LEAST SQUARES USING THE
04291  C *               ELIMINATION OF CONSTRAINT EQUATIONS APPROACH .
04292  C *****
04293  C INPUT PARAMETERS
04294  C   R,M,N - LS PROBLEM SPECS ; R - NO OF CONSTRAINT ECNS
04295  C                                   M - NO OF UNKNOWNNS
04296  C                                   N - NO OF OBSERVATIONS
04297  C   C, D  - PARTITIONED MATRICES OF A1 DESIGN MATRIX - PRIMARY MODEL
04298  C   G, H  - PARTITIONED MATRICES OF A2 DESIGN MATRIX - SECONDARY MODEL
04299  C             DIMENSIONS      H - R X R
04300  C                               G - R X M
04301  C                               C - N X M
04302  C                               D - N X R
04303  C             DECLARED DIMENSIONS IS AS STATED BELOW
04304  C   W1,W2 - MISCLASURE VECTORS
04305  C   IC,JC,JD,IG,JG,IH,JH,IP,JP,IW1,IW2
04306  C             - DECLARED DIMENSIONS OF MATRICES( SEE BELOW)
04307  C
04308  C OUTPUT PARAMETERS
04309  C   X,VX  - LS ESTIMATES AND COVARIANCE
04310  C   V     - RESIDUALS
04311  C   IX,IV - DECLARED DIMENSIONS OF MATRICES X,VX AND V(SEE BELOW)
04312  C   IER   - ERROR CODE
04313  C
04314  C ADDITIONAL NOTES
04315  C   CURRENT ARRAY SETTINGS LIMIT THE SOLUTION TO ONLY 100 ESTIMATES
04316  C
04317  C CALLS - COND,DINV,CHOLD,DMULT,OPRINT,SCMULT,DMAG,PCOPY
04318  C *****
04319  C   REAL*8 C(IC,JC),D(ID,JD),G(IG,JG),H(IH,JH),
04320  C   @     P(IP,JP),W1(IW1,1),W2(IW2,1).

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04513	C *****		DSPLIN
04514	C * VERSION : JANUARY 1982		DSPLIN
04515	C * DESCRIPTION : PERFORMS THE PERMUTATION OF MATRICES X AND VX		DSPLIN
04516	C * (SOLUTION VECTOR AND ITS COVARIANCE) COMPUTED		DSPLIN
04517	C * VIA THE ELIMINATION OF CONSTRAINTS MODEL TO THAT		DSPLIN
04518	C * AS IF WERE COMPUTED VIA THE FUNCTIONAL CONSTRAINT		DSPLIN
04519	C * MODEL.		DSPLIN
04520	C *****		DSPLIN
04521	C INPUT PARAMETERS		DSPLIN
04522	C X,VX - SOLUTION VECTOR AND ITS COVARIANCE		DSPLIN
04523	C II - DECLARED DIMENSIONS OF V AND VX		DSPLIN
04524	C M - UPPER LEFT HAND CORNER CONTAINING THE MATRIX ELEMENTS		DSPLIN
04525	C		DSPLIN
04526	C OUTPUT PARAMETERS		DSPLIN
04527	C X,VX - PERMUTATED MATRICES X AND VX.		DSPLIN
04528	C		DSPLIN
04529	C ADDITIONAL NOTES		DSPLIN
04530	C THE PERMUTATION SEQUENCE IS FIXED BY THE PROGRAM.		DSPLIN
04531	C THE ALGORITHM WILL OPERATE ONLY ON AN EVEN ORDER SQUARE MATRIX.		DSPLIN
04532	C THIS IS NOT CHECKED ANYWHERE.		DSPLIN
04533	C		DSPLIN
04534	C*PROGRAM BEGINS		DSPLIN
04535	C START POINTERS		DSPLIN
04536	J = M/2-1		DSPLIN
04537	I = -1		DSPLIN
04538	IK = M - 3		DSPLIN
04539	DO 10 K = 1,IK,4		DSPLIN
04540	C* INCREMENT		DSPLIN
04541	I = I + 2		DSPLIN
04542	I2 = I + 1		DSPLIN
04543	J = J + 2		DSPLIN
04544	J2 = J + 1		DSPLIN
04545	K2 = K + 1		DSPLIN
04546	K3 = K + 2		DSPLIN
04547	K4 = K + 3		DSPLIN
04548	C* FEED		DSPLIN
04549	P(K,1) = I		DSPLIN
04550	P(K2,1) = I2		DSPLIN
04551	P(K3,1) = J		DSPLIN
04552	10 P(K4,1) = J2		DSPLIN
04553	C* SETS TRACK SEQUENCE ; MONITORS THE ACTUAL LOCATION OF THE ROW/COLUMN		DSPLIN
04554	DO 20 I = 1,M		DSPLIN
04555	20 TRACK(I) = I		DSPLIN
04556	C*		DSPLIN
04557	C* ROW EXCHANGES OF THE MATRIX		DSPLIN
04558	C*		DSPLIN
04559	DO 30 I = 1,M		DSPLIN
04560	IS = I		DSPLIN

VITA

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